FOUNDATION CALCULATIONS

65'x70' Metal Building
MVE #23-0706

REVIEWED FOR CODE COMPLIANCE 09/18/2023

CLAY HOCKEL C&B HOLDINGS Hayden, Colorado

Metal Building Supplied By:

METAL BUILDING OUTLET CORP. 7651 Shaffer Pkwy, Ste. A Littleton, CO 80127

JUL 31 2023

Foundation Design by:





Page: Job: MVE #23-0706 METAL BUILDING OUTLET CORP. **CLAY HOCKEL C&B HOLDINGS** Subject:

Date: 07/26/23 **BLC** By:

DESIGN CRITERIA:

REVIEWED CODE 80 psf COMPLIANCE 60 psf 09/18/2023 20 psf 1 psf

Code: 2018 IBC

Ground Snow Load

Roof Collateral Load

Roof Snow Load

Roof Live Load

SDS 0.409 Wind Speed 115 mph C Seismic Design Category Exposure = C Site Class D Importance Factor 1.0

Other Loads:

Soil Bearing	3500	psf (Per Geotech)
Minimum Bearing	1500	psf (Per Geotech)
Frost Depth	48	inches (Per Geotech
Passive Pressure	250	psf/ft (Assumed)
Coefficient of Friction	0.25	(Assumed)

Notes:

Reactions per METAL BUILDING OUTLET CORP. drawings.

The foundation has been designed, and the site soils should be prepared for the foundation. in accordance with the recommendations in the geotechnical investigation report by:

Erika K. Hill, P.E., P.G. of NWCC, Inc.

2580 Copper Ridge Drive, Steamboat Springs, CO 80487

Concrete and Reinforcement:

Concrete Strength

3000 P.S.I. for Foundations

3500 P.S.I. for Slabs

2500 P.S.I. Used for design, no special inspection required.

Rebar - ASTM A615 grade 60



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CLAY HOCKEL C&B HOLDINGS

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Sidewall Footings

(Lines 2 & 3 / Grids A & E)

 $P_{D+L} =$ 53.7 kips $F_H =$ 30.3 kips 9.3 Uplift = kips

Use 5.0 ft. x 5.0 ft. x 30 inch deep footing

REVIEWED FOR CODE

								
Horizontal Force Use rebar tension ties across the building to resist horizontal force at the column base.								
Top of Pier to Center of Ties =	18 in	Number of Ties =	4 ties					
Tensile Strength of Rebar =	24 ksi	Tie Size =	#6 rebar					
Area Required =	1.263 in^2	Use (4) #6	tension ties.					
Weights		Passive Soil Resistance						
Weight of Pier =	1.36 kips	Wall Length for Passive Res. =	1.5 ft					
Weight of Soil Above Footing =	3.58 kips	Ftg. Width for Passive Res. =	5 ft					
Weight of Spot Footing =	9.06 kips	Passive Earth Pressure =	200 psf/ft					
Weight of Continuous Wall =	0.00 kips	Passive Res. (Spot Footing) =	8.13 kips					
Weight of Continuous Ftg. =	0.00 kips	Passive Res. (Wall & Pier) =	0.30 kips					
g g	•	Passive Res. (Cont. Ftg.) =	0.00 kips					
Use Passive Res. to Resist Moment?	YES	Total Passive Resistance =	8.43 kips					
Check Soil Bearing		Allowable Bearing Pressure =	3500 psf					
Moment Arm =	1.5 ft	Top of Wall to Grade =	6 in					
P (total) =	53.70 kips	OS Conc. to CL A.R. =	16.25 in					
Overturning Moment =	45.45 kip*ft	Pier Width =	18 in					
OTM Eccentricity =	10.2 inches	Pier Depth (wall included) =	30 in					
Footing Offset =	3.25 inches	Pier Height =	30 in					
-	14.54 kip*ft	Wall Thickness =	8 in					
	7.72 kip*ft	Wall Height =	48 in					
Net Eccentricity =	5.2 inches	Footing Width =	16 in					
B/6 = 10 inches OK		Footing Depth =	8 in					
Pageing Programs of (mark)	2204 5 OV	Offset feet	na 2 25 inches					
Bearing Pressure, q (max.) =	3261 psf OK	Unset loot	ng 3.25 inches.					
Minimum Bearing Pressure = Uplift	1763 psf OK							
Weight of Footing and Pier =	10.42 kips	Wall Length used for Uplift =	23 ft					
Weight of Soil Above Footing =	3.58 kips	Cont. Ftg. Length for Uplift =	23.0 ft					
Weight of Cont. Wall & Footing =	10.63 kips	Cont. Fig. Length for Ophilt =	20.0 IL					
Total =	24.64 kips	Factor of Safety =	2.65 > 1.0 OK					

Check Footing Flexure (Reinforcing in Direction of Horizontal Force)

q (min.) =	1035	psf	Rebar d' =	3.5	in
OS Footing Edge from Wall =	1.417	ft	Rebar d =	26.5	in
q (at face of wall) =	2630	psf	Rebar fy =	60000	psi
Moment in Footing (Mu, ULT) =	20.74	k*ft	Concrete f'c =	2500	psi
As (req'd by calc.) =	0.174	in^2	ACI 7.12 As (min) =	3.240	in^2

Opposite Direction Reinforcing

Min. Steel Ratio = 0.0018 As per ACI 7.12

Use (6) #5 bars each way at top of footing and use (6) #5 bars each way at bottom of footing.

Check Footing Shear For Pier Design Nu = 86 kips Shear in Footing (Vu, ULT) = 29.27 kips **See pier calculation Mu = 73 kip*ft Required Thickness = 10.01 in OK on page 3. Vu = 48 kips



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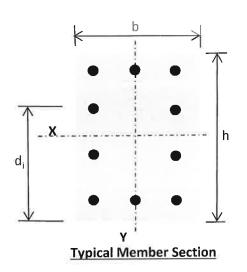
BLC

Concrete Column Analysis (ACI 318)

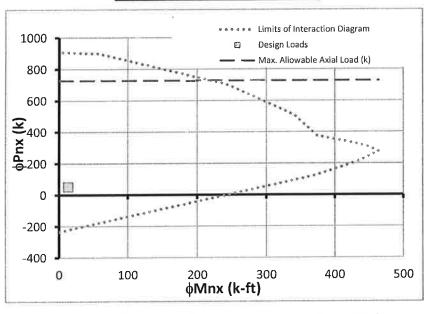
For X-Axis Flexure with Axial Compression or Tension Load Assuming "Short", Non-Slender Member with Symmetric Reinforcing

CODE COMPLIANCE 09/18/2023

<u>Input</u>			Column Geometry		
$f_c' =$	2500	psi	Bar Size =	5	Total # of Bars
$f_{\gamma} =$	60	ksi	# of Bars b Face	4	Tie Size =
d' =	2.375	in	# of Bars h Face	5	
b =	18	in			
h =	30	in	Placement of Reinf	orcem	ent Steel
φ =	0.65			\underline{d}_{i}	\underline{A}_{si}
Loadi	ng		Edge Layer (d₁)	27.63	1.24
P _{ux} =	51.6	kips	Interior Layer (d ₂)	21.31	0.62
$M_{ux} =$	13.2	kip-ft	Interior Layer (d ₃)	15.00	0.62
$V_{ux} =$	3.3	kips	Interior Layer (d ₄)	8.69	0.62
			Interior Layer (d ₅)	0.00	0.00
			Edge Layer (d ₆)	2.38	1.24



X-AXIS INTERACTION DIAGRAM



DESIGN LOADS FALL WITHIN THE LIMITS OF THE INTERACTION DIAGRAM, THEREFORE, USE (14) # VERTICAL BARS IN COLUMN.

 $V_u < \phi V_c/2$ Shear Design $\phi V_c = 39.076$ $\phi V_c/2 = 19.538$

If $V_u < \phi V_c/2$ then Vertical Spacing of ties shall not exceed the least of:

16 x (longitudal bar diameters) 10 in 48 x (tie bar diameter) 24 in 18 in Least dimension of column

If $V_{ij} > \phi V_c/2$ then vertical spacing of ties shall not exceed the least of:

 $A_v f_v / (0.75 v (f_c') b) = 35.556$ in s max = = 26.667 in $A_v f_v / (50b)$ s max = = 13.813 in $d/2 \le 24$ in s max =

INCHES ON CENTER WITH (3) IN THE TOP SIX INCHES OF PIER. TIES AT 8.00



7

inches OK

Job: MVE #23-0706 METAL BUILDING OUTLET CORP.

Footing Depth =

Factor of Safety =

CLAY HOCKEL C&B HOLDINGS

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By: **BLC**

Endwall Footings

Subject:

(Line 1 / Grids B, D, & E and Line 4 / Grids B, C, & E)

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in

2.04 > 1.0 OK

P _{D+L} -	25.3	Kips
F _H =	2.9	kips
Uplift =	5.9	kips

B/6 =

Total =

Use 3.5 ft. x 3.5 ft. x 12 inch deep footing

Check Soil Bearing				Allowable Bearing Pressure =	3500	psf
Moment Arm =		5	ft	Top of Wall to Grade =	6	in
P (total) =		25.30	kips	OS Conc. to CL A.R. =	4	in
Overturning Moment =		14.5	kip*ft	Pier Width =	12	in
OTM Eccentricity =		6.9	inches	Pier Depth (wall included) =	8	in
Footing Offset =		0	inches	Pier Height =	48	in
Offset Resisting Moment =	-	0.00	kip*ft	Wall Thickness =	8	in
Passive Resisting Moment =	S 7.	4.34	kip*ft	Wall Height =	48	in
Net Eccentricity =		4.8	inches	Footing Width =	16	in

Bearing Pressure, q (max.) =	3487 psf OK	Offset footi	ng 0 inches.
Minimum Bearing Pressure =	1783 psf OK		,
Sliding Resistance			
Coefficient of Friction =	0.25	Wall Length for Sliding =	4.0 ft
Weight of Pier =	0.39 kips	Wall Length for Passive Res. =	4.0 ft
Weight of Soil Above Footing =	3.24 kips	Ftg. Width for Sliding/Passive =	4.0 ft
Weight of Spot Footing =	1.78 kips	Passive Earth Pressure =	200 psf/ft
Weight of Continuous Wall =	1.16 kips	Passive Res. (Spot Footing) =	2.80 kips
Weight of Continuous Ftg. =	0.06 kips	Passive Res. (Wall & Pier) =	1.40 kips
Sliding Resistance from Footing & Pier =	0.54 kips	Passive Res. (Cont. Ftg.) =	0.26 kips
Sliding Resistance from Soil above Ftg. =	0.81 kips	Total Passive Resistance =	4.46 kips
Sliding Resistance from Vertical Load =	6.33 kips	Total Sliding Resistance =	7.98 kips
Sliding Resistance from Wall & Ftg. =	0.31 kips	Factor of Safety =	4.29 > 1.0 OK
<u>Uplift</u>			
Weight of Footing and Pier =	2.16 kips	Wall Length used for Uplift =	14.5 ft
Weight of Soil Above Footing =	3.24 kips	Cont. Ftg. Length for Uplift =	14.5 ft
Weight of Cont. Wall & Footing =	6.64 kips		

Check Footing Flexure (Reinforcing in Direction of Horizontal Force)

q (min.) =	644	psf	Rebar d' =	3.5	in	<u>Opti</u>	ons
OS Footing Edge from Wall =	1.417	ft	Rebar d =	8.5	in	5	#4 bars
q (at face of wall) =	2336	psf	Rebar fy =	60000	psi	3	#5 bars
Moment in Footing (Mu, ULT) =	15.55	k*ft	Concrete f'c =	2500	psi	3	#6 bars
As (reg'd by calc.) =	0.411	in^2	ACI 7.12 As (min) =	0.907	in^2		

12.04 kips

Opposite Direction Reinforcing	Opt	ions
	5	#4 bars

As per ACI 7.12	3 #6 bars_	and use (5) #4 bars in the opposite direction.
Min. Steel Ratio = 0.0018	3 #5 bars	Use (5) #4 bars in direction of horizontal force
	0	the state of the s

For Pier Design

Check Footing Shear

Shear in Footing (Vu, ULT) =	21.95 kip	os	Nu =	40	kips	**See pier calculation
Required Thickness =	10.47 in	OK	Mu =	19	kip*ft	on page 5.
			Vu =	5	kips	_



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CLAY HOCKEL C&B HOLDINGS

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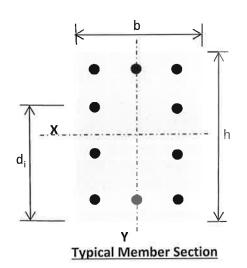
Concrete Column Analysis (ACI 318)

Subject:

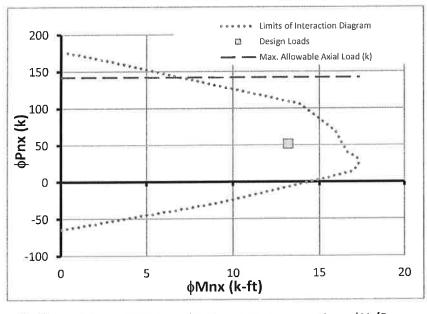
For X-Axis Flexure with Axial Compression or Tension Load Assuming "Short", Non-Slender Member with Symmetric Reinforcing

REVIEWED FOR CODE COMPLIANCE 09/18/2023

Input			Column Geometry		
f _c ' =	2500	psi	Bar Size =	4	Total # of Bars
$f_y =$	60	ksi	# of Bars b Face	3	Tie Size =
d' =	2	in	# of Bars h Face	2	
b =	12	in			
h =	8	in	Placement of Reinf	orcem	ent Steel
φ =	0.65			\underline{d}_{i}	\underline{A}_{st}
Loadir	og .		Edge Layer (d₁)	6.00	0.60
$P_{ux} =$	51.6	kips	Interior Layer (d ₂)	0.00	0.00
$M_{ux} =$	13.2	kip-ft	Interior Layer (d ₃)	0.00	0.00
$V_{ux} =$	3.3	kips	Interior Layer (d ₄)	0.00	0.00
			Interior Layer (d ₅)	0.00	0.00
			Edge Layer (d ₆)	2.00	0.60



X-AXIS INTERACTION DIAGRAM



DESIGN LOADS FALL WITHIN THE LIMITS
OF THE INTERACTION DIAGRAM,
THEREFORE, USE (6) # 4
VERTICAL BARS IN COLUMN.

Shear Design (

 $\phi V_c = 6.8513$

 $\phi V_c/2 = 3.4256$

 $V_u < \phi V_c/2$

If $V_u < \phi V_c/2$ then Vertical Spacing of ties shall not exceed the least of:

16 x (longitudal bar diameters) = 8 in
48 x (tie bar diameter) = 18 in
Least dimension of column = 8 in

If $V_u > \phi V_c/2$ then vertical spacing of ties shall not exceed the least of:

s max = $A_v f_v / (0.75v(f_c')b)$ = 29.333 in s max = $A_v f_v / (50b)$ = 22 in s max = $d/2 \le 24$ in = 3 in

USE # 3 TIES AT 8.00 INCHES ON CENTER WITH (3) IN THE TOP FIVE INCHES OF PIER.



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Corner Footings (Lines 1 & 4 / Grids A & E)

Subject:

FOR FOR CODE COMPLIANCE 09/18/2023

 $P_{D+L} = 9.3$ kips Uplift = 4.3 kips

Check Soil Bearing

Allowable Pressure = 3500 psf Minimum Pressure = 1500 psf

 $B \operatorname{req'd} = 1.63 \operatorname{ft}$

Use 2.5 ft² x 12 inch deep footing reinforced with (4) #4 bars each way.

q = 3355 psf OK $q_{min} = 1867$ psf OK

<u>Uplift</u>

Design uplift = 4.3 kips

Slab Thickness = 0 inches

Depth to top of Ftg. = 42 inches

(EW) OS Conc. to CL Footing = 4 inches

(SW) OS Conc. to CL Footing = 9.8 inches

(EW) Length of Wall for Uplift = 7.5 feet

(SW) Length of Wall for Uplift = 11.5 feet

Wall Thickness = 8 inches

Weight of Footing and Soil = 3.13 kips

Weight of Concrete Slab = 0.00 kips

Weight of Foundation Wall & Ftg. = 8.54 kips

Total = 11.67 kips

Factor of Safety = 2.71 > 1.0 OK



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CLAY HOCKEL C&B HOLDINGS

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Endwall Footings (Lines 2 & 3 / Grid D.1)

kips

Subject:

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$F_H = 2.1$ kips		12	Use 2.5 ft. x 2.5 ft. x 12 inch	deep	footing
Uplift = 0.0 kips					<i>y</i> 10/202
Check Soil Bearing			Allowable Bearing Pressure =	3500	psf
Moment Arm =	1	ft	Top of Wall to Grade =	6	in
P (total) =	14.8	kips	OS Conc. to CL A.R. =	4	in

Overturning Moment = 2.058 kip*ft Pier Width = 12 in OTM Eccentricity = 1.7 inches Pier Depth (wall included) = 8 in Footing Offset = 0 inches Pier Height = 48 in Offset Resisting Moment = 0.00 kip*ft Wall Thickness = 8 in Passive Resisting Moment = 0.00 kip*ft Wall Height = 48 in Net Eccentricity = Footing Width = 1.7 inches 16 in

Footing Depth = B/6 =5 inches OK 8 in

Bearing Pressure, q (max.) = 3159 OK psf Minimum Bearing Pressure = 3159 psf OK

Offset footing 0 inches.

Sliding Resistance					
Coefficient of Friction =	0.25		Wall Length for Sliding =	2.0	ft
Weight of Pier =	0.40	kips	Wall Length for Passive Res. =	2.0	ft
Weight of Soil Above Footing =	1.51	kips	Ftg. Width for Sliding/Passive =	2.0	ft

Weight of Pier =	0.40	kips	Wall Length for Passive Res. =	2.0	ft	
Weight of Soil Above Footing =	1.51	kips	Ftg. Width for Sliding/Passive =	2.0	ft	
Weight of Spot Footing =	0.94	kips	Passive Earth Pressure =	200	psf/ft	
Weight of Continuous Wall =	0.39	kips	Passive Res. (Spot Footing) =	2.00	kips	
Weight of Continuous Ftg. =	-0.07	kips	Passive Res. (Wall & Pier) =	0.70	kips	
Sliding Resistance from Footing & Pier =	0.33	kips	Passive Res. (Cont. Ftg.) =	-0.26	kips	
Sliding Resistance from Soil above Ftg. =	0.38	kips	Total Passive Resistance =	2.44	kips	
Sliding Resistance from Vertical Load =	0.16	kips	Total Sliding Resistance =	0.95	kips	
Sliding Resistance from Wall & Ftg. =	0.08	kips	Factor of Safety =	1.65	> 1.0 OK	

<u>Uplift</u>

 $P_{D+L} =$

0.6

piiit				
Weight of Footing and Pier =	1.34	kips	Wall Length used for Uplift =	23.33 ft
Weight of Soil Above Footing =	1.51	kips	Cont. Ftg. Length for Uplift =	23.33 ft
Weight of Cont. Wall & Footing =	11.32			
Total =	14.16	kips	Factor of Safety =	na

Check Footing Flexure (Reinforcing in Direction of Horizontal Force)

q (min.) =	1578	psf	Rebar d' =	3.5	in
OS Footing Edge from Wall =	0.917	ft	Rebar d =	8.5	in
q (at face of wall) =	2579	psf	Rebar fy =	60000	psi
Moment in Footing (Mu, ULT) =	4.58	k*ft	Concrete f'c =	2500	psi
As (req'd by calc.) =	0.120	in^2	ACI 7.12 As (min) =	0.648	in^2

Opposite Direction Reinforcing

Min. Steel Ratio = 0.0018 As per ACI 7.12

Use (4) #4 bars in direction of horizontal force and use (4) #4 bars in the opposite direction.

For Pier Design

Check Footing Shear

**See pier calculation Shear in Footing (Vu, ULT) = 9.99 Nu = 1 kips kips 7.94 in Required Thickness = Mu = 13 kip*ft OK on page 8. Vu = 3 kips



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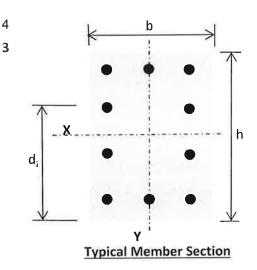
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Concrete Column Analysis (ACI 318)

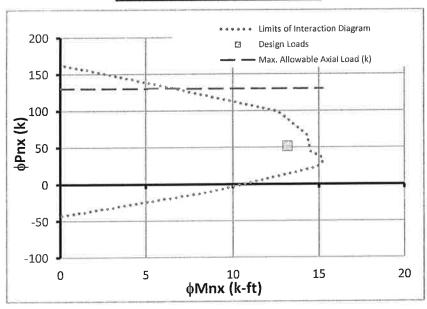
For X-Axis Flexure with Axial Compression or Tension Load Assuming "Short", Non-Slender Member with Symmetric Reinforcing

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Input			Column Geometry		
f _c ' =	2500	psi	Bar Size =	4	Total # of Bars
$f_{v} =$	60	ksi	# of Bars b Face	2	Tie Size =
d' =	2	in	# of Bars h Face	2	
b =	12	in			
h =	8	in	Placement of Reinf	orcem	ent Steel
φ =	0.65			\underline{d}_{i}	\underline{A}_{st}
Loadir	1g		Edge Layer (d₁)	6.00	0.40
$P_{ux} =$	51.6	kips	Interior Layer (d ₂)	0.00	0.00
$M_{ux} =$	13.2	kip-ft	Interior Layer (d ₃)	0.00	0.00
$V_{ux} =$	3.3	kips	Interior Layer (d ₄)	0.00	0.00
			Interior Layer (d ₅)	0.00	0.00
			Edge Layer (d ₆)	2.00	0.40



X-AXIS INTERACTION DIAGRAM



DESIGN LOADS FALL WITHIN THE LIMITS OF THE INTERACTION DIAGRAM, THEREFORE, USE (4) # **VERTICAL BARS IN COLUMN.**

 $V_u < \phi V_c/2$ $\phi V_c/2 = 3.4256$ **Shear Design** $\phi V_c = 6.8513$

If $V_{II} < \phi V_c/2$ then Vertical Spacing of ties

shall not exceed the least of: 16 x (longitudal bar diameters) in 48 x (tie bar diameter) 18 in Least dimension of column 8 in

If $V_{ij} > \phi V_c/2$ then vertical spacing of ties shall not exceed the least of:

 $A_v f_v / (0.75 v(f_c')b) =$ 29.333 in s max = $A_v f_v / (50b)$ 22 in s max = 3 $d/2 \le 24$ in in s max =

INCHES ON CENTER WITH (3) IN THE TOP FIVE INCHES OF PIER.

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CLAY HOCKEL C&B HOLDINGS

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By: BLC

Worst Case: Sidewall Anchors (Tension and Shear)

ANCHOR ROD GROUP CHECK (per ACI 318-14 Chapter 17, headed anchors)

FOR

Tensile Force on Anchors (N _U) =	14.88	kips
Shear Force on Anchors $(V_U) =$	48.48	kips
Seismic Design Category =	C	
Number of Anchors (n) =	6	
Number of Anchors in Tension (n) =	6	
Anchor Diameter $(d_a) = 1$ in $A_{SE} =$	0.606	in^2
Anchor Spacing Perpendicular to Load (s ₁) =	4	in
Anchor Spacing Parallel to Load $(s_2) =$	4	in
Spacing of outer Anchors $(s_0) =$	8	in
Embedment Depth (h _{EF}) =	22	in
Yield Strength of Anchors (Fy) =	36	ksi
Tensile Strength of Anchors (F _{uta}) =	58	ksi
Edge Distance in Load Direction (c _{a1}) =	12.25	in
Edge Distance Perpendicular to Load $(c_{a2}) =$	7	in
Concrete Strength $(f_C) =$	2500	psi
Axial Eccentricity (e' _N) =	0	in
Shear Eccentricity (e' _V) =	0	in

Steel Strength of Anchors in Tension (17.4.1.2)

$$N_{sa} = nA_{SE}F_{uta} = 210.89 \text{ kips}$$

 $\phi = 0.75 \quad \phi N_{sa} = 158.17 \text{ kips}$

Concrete Breakout Strength of Anchors in Tension (17.4.2)

$A_{Nc} = 540 \text{ in}^2 A_{Nco}$	$=9h_{ef}^{2}=$	4356	in^2
$\Psi_{\text{ec,N}} = 1/(1+2e'_{\text{N}}/3h_{\text{EF}}) \le 1.0$)	$\Psi_{ec,N} =$	1.000
$e_{a \text{ (min.)}} < 1.5 h_{EF}$?	YES	$\Psi_{ed,N} =$	0.764
Cracking at Service Loads?	YES	$\Psi_{c,N} =$	1.000
Headed anchors used, therefore		$\Psi_{cp,N} =$	1.000
$h_{EF} >= 11 \text{ in. } ?$	YES	$k_C =$	24

Anchor bolts are tied into the footings with rebar cages, so concrete breakout will be limited by the tensile strength of the rebar verticals in the cage.

Number of Verticals = 8 Size of rebar = #5Tensile strength of the reinforcement = 148.8 kips (ULT)

$$\phi = 0.75 \qquad \phi N_{CBG} = 111.60 \text{ kips}$$

Pullout Strength of Anchors in Tension (17.4.3)

Side-face Blowout of Anchors in Tension (17.4.4) SIDE-FACE BLOWOUT $h_{EF} > 2.5 c_{a1}$ NO $s_1 < 6c_{a1}$? YES NOT CONTROL YES $c_{a2} < 3c_{a1}$? R = 0.39 $N_{sb} = 160c_{a1}A_{BRG}^{0.5}\lambda_a f_C^{0.5}R$ 41.52 kips Therefore, $N_{\rm sbg} = (1 + s_0 / 6c_{\rm al}) N_{\rm sb} =$ $\phi = 0.75$ $\phi N_{sbg} =$

Steel Strength of Anchors in Shear (17.5.1)

Built-up grout pads used? NO
$$V_S = 0.6nA_{SE}F_{uta} = 126.53 \text{ kips}$$
 $\phi = 0.65 \text{ } \phi V_S = 82.25 \text{ kips}$

Concrete Breakout Strength of Anchors in Shear (17.5.2)

$$V_{cbg} = \frac{A_{Vc}}{A_{Vco}} \Psi_{ec,V} \Psi_{ed,V} \Psi_{c,V} \Psi_{h,V} V_b = 17.20$$
 kips
Concrete breakout in shear will be resisted by rebar ties at the

top of the footing, tensile capacity of the bars will control. # 4 bar 0.2 in^2 Tie Size = Bar Area =

Fy =Number of Ties at top = 108 kips Tensile Capacity of Ties = $V_{\rm cbg} = 108.00 \text{ kips}$ Therefore, $\phi V_{cbg} = 81.00 \text{ kips}$ $\Phi = 0.75$

Concrete Pryout Strength of Anchors in Shear (17.5.3)

Concrete pryout of anchors in shear will only occur where anchors are relatively stiff and short.

$$\frac{h_{EF}}{d_0} = 22 > 6$$

THEREFORE, CONCRETE PRYOUT WILL NOT CONTROL SHEAR DESIGN OF ANCHORS.

ANCHOR ROD GROUP CAPACITY

SDC = C, D, E, & F REDUCE CONCRETE ALLOW. TENSION BY 0.75

ALLOW. TENSION $(\Phi N_N) =$ 73.27 kips > 14.9 kipsOK ALLOW. SHEAR $(\Phi V_N) =$ **81.00** kips > 48.5 kips OK

CHECK SHEAR/TENSION INTERACTION

$$\begin{array}{ll} N_{UA} > 0.2 \Phi N_N ~? & YES \\ V_{UA} > 0.2 \Phi V_N ~? & YES \\ \hline \frac{N_{UA}}{\Phi N_N} + \frac{V_{UA}}{\Phi V_N} = & 0.80 < 1.20 ~\underline{OK} \\ \end{array}$$

Job: MVE #23-0706 METAL BUILDING OUTLET CORP.
Subject: CLAY HOCKEL C&B HOLDINGS

 $\Phi = 0.75$

Page: 10
Date: 07/31/23
By: BLC

By:

Worst Case: Endwall Anchors (Tension and Shear)(Wind Controls)

ANCHOR ROD GROUP CHECK (per ACI 318-14 Chapter 17, headed anchors)

COMPLIANC

REVIEWED

FOR

Tensile Force on Anchors $(N_U) =$	9.44	kips
Shear Force on Anchors (V_U) =	4.64	kips
Seismic Design Category =	C	
Number of Anchors (n) =	4	
Number of Anchors in Tension (n) =	4	
Anchor Diameter $(d_a) = 0.625$ in $A_{SE} =$	0.226	in^2
Anchor Spacing Perpendicular to Load (s_1) =	4	in
Anchor Spacing Parallel to Load $(s_2) =$	3	in
Spacing of outer Anchors $(s_0) =$	3	in
Embedment Depth $(h_{EF}) =$	12	in
Yield Strength of Anchors (Fy) =	36	ksi
Tensile Strength of Anchors (F _{uta}) =	58	ksi
Edge Distance in Load Direction (cal) =	2.5	in
Edge Distance Perpendicular to Load $(c_{a2}) =$	12	in
Concrete Strength (f' _C) =	2500	psi
Axial Eccentricity (e' _N) =	0	in
Shear Eccentricity (e' _V) =	0	in

Steel Strength of Anchors in Tension (17.4.1.2)

$$N_{sa}$$
 = $nA_{SE}F_{uta}$ = 52.43 kips
 ϕ = 0.75 ϕN_{sa} = 39.32 kips

Concrete Breakout Strength of Anchors in Tension (17.4.2)

$A_{Nc} = 96 \text{ in}^2 A_N$	$_{\text{leo}} = 9h_{\text{ef}}^2 =$	1296	in^2
$\Psi_{ec,N} = 1/(1+2e'_{N}/3h_{EF}) <=$	1.0	$\Psi_{ec,N} =$	1.000
$c_{a \text{ (min.)}} < 1.5 h_{EF}$?	YES	$\Psi_{ed,N} \; = \;$	0.742
Cracking at Service Loads?	YES	$\Psi_{c,N} =$	1.000
Headed anchors used, therefo	re	$\Psi_{cp,N} =$	1.000
$h_{\rm FF} > = 11 \text{ in. } ?$	YES	$k_C =$	24

$$\begin{array}{llll} N_b &=& k_C \lambda_a \; f_C^{~0.5} h_{EF}^{~~5/3} &=& 50.32 \quad kips \\ N_{ebg} &=& \frac{A_{Nc}}{A_{Nco}} & \Psi_{ec,N} \Psi_{ed,N} \Psi_{cp,N} N_b &=& 2.76 \quad kips \end{array}$$

Anchor bolts are tied into the footings with rebar cages, so concrete breakout will be limited by the tensile strength of the rebar verticals in the cage.

Number of Verticals = 6 Size of rebar = # 4

Tensile strength of the reinforcement = 72 kips (ULT)

$$\phi = 0.75 \qquad \phi N_{CBG} = 54.00 \text{ kips}$$

Pullout Strength of Anchors in Tension (17.4.3)

$$\begin{array}{lll} A_{BRG} = & 0.454 & in^2 \\ N_P = & 8A_{BRG} f_C & = & 9.08 & kips \\ Cracking at Service Loads? & YES & \Psi_{c,P} & = & 1 \\ N_{PN} \left(group\right) = & n\Psi_{c,P} N_P = & 36.32 & kips \\ \varphi & = & 0.7 & \varphi N_{PN} \left(group\right) = & 25.42 & kips \end{array}$$

Side-face Blowout of Anchors in Tension (

 $\phi N_{sba} =$

Steel Strength of Anchors in Shear (17.5.1)

Built-up grout pads used? NO $V_S = 0.60 A_{SE} F_{uta} = 31.46 \text{ kips}$ $\phi = 0.65 \phi V_S = 20.45 \text{ kips}$

Concrete Breakout Strength of Anchors in Shear (17.5.2)

Concrete breakout in shear will be resisted by rebar ties at the top of the footing, tensile capacity of the bars will control.

Tie Size = # 3 bar Bar Area = 0.11 in^2 Number of Ties at top = 3 Fy = 60 ksi

Tensile Capacity of Ties = 39.6 kips

Therefore, $V_{cbg} = 39.60 \text{ kips}$ $\Phi = 0.75 \Phi V_{cbg} = 29.70 \text{ kips}$

Concrete Pryout Strength of Anchors in Shear (17.5.3)

Concrete pryout of anchors in shear will only occur where anchors are relatively stiff and short.

$$\frac{h_{EF}}{d_0} = 19.2 > 6$$

THEREFORE, CONCRETE PRYOUT WILL NOT CONTROL SHEAR DESIGN OF ANCHORS.

ANCHOR ROD GROUP CAPACITY

ALLOW. TENSION $(\Phi N_N) = 12.13$ kips > 9.44 kips \underline{OK} ALLOW. SHEAR $(\Phi V_N) = 20.45$ kips > 4.64 kips \underline{OK}

CHECK SHEAR/TENSION INTERACTION

 $\begin{array}{ll} N_{UA} > 0.2 \Phi N_N ~? & YES \\ V_{UA} > 0.2 \Phi V_N ~? & YES \\ \hline \frac{N_{UA}}{\Phi N_N} ~+ \frac{V_{UA}}{\Phi V_N} = ~1.01 ~< ~1.20 ~\underline{OK} \end{array}$



Project Title: Engineer:

Clay Hockel C&B Holdings BLC

23-0706

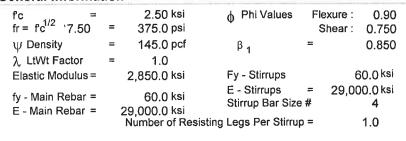
Project ID: 65'x70' Metal Building Project Descr:

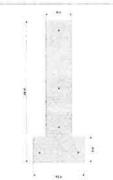
Concrete Beam LIC#: KW-06014791, Build:20.23.07.20 MOUNTAIN VIEW ENGINEERING, INC. **DESCRIPTION:** Grade Beam **CODE REFERENCES** 09/18/2023

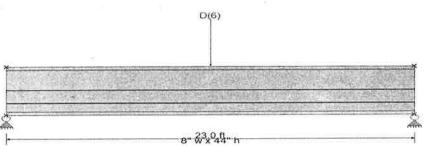
Calculations per ACI 318-14, IBC 2018, CBC 2019, ASCE 7-16

Load Combination Set: IBC 2018

General Information







Cross Section & Reinforcing Details

Inverted Tee Section, Stem Width = 8.0 in, Total Height = 44.0 in, Top Flange Width = 16.0 in, Flange Thickness = 8.0 in Span #1 Reinforcing....

2-#4 at 3.0 in from Bottom, from 0.0 to 23.0 ft in this span 1-#4 at 11.0 in from Bottom, from 0.0 to 23.0 ft in this span 1-#4 at 3.0 in from Top, from 0.0 to 23.0 ft in this span 1-#4 at 21.0 in from Top, from 0.0 to 23.0 ft in this span

Beam self weight calculated and added to loads

Point Load: D = 6.0 k @ 11.50 ft

Design OK **DESIGN SUMMARY** 0.742:1Maximum Bending Stress Ratio = Section used for this span **Typical Section** Mu: Applied 86.991 k-ft Mn * Phi : Allowable 117.297 k-ft 11.521 ft Location of maximum on span Span # where maximum occurs Span #1 **Maximum Deflection** 0 <360.0 Ratio = Max Downward Transient Deflection 0.000 in Ratio = 0 <360.0 0.000 in Max Upward Transient Deflection Span: 1: D Only Ratio = 11159 >=240.0 Max Downward Total Deflection 0.025 in Ratio = 0 <240.0 Span: 1 : D Only Max Upward Total Deflection 0.000 in Support notation: Far left is #1 **Vertical Reactions** Support 1 Support 2

Load Combination 7.817 7.817 Max Upward from all Load Conditions 4.690 4.690 Max Upward from Load Combinations 7.817 Max Upward from Load Cases 7.817 7.817 7.817 D Only 4.690 4.690 +0.60D

Shear Stirrup Requirements

Entire Beam Span Length: Vu < Phi*Vc / 2, Req'd Vs = Not Reqd per 9.6.3.1, Stirrups are not required.



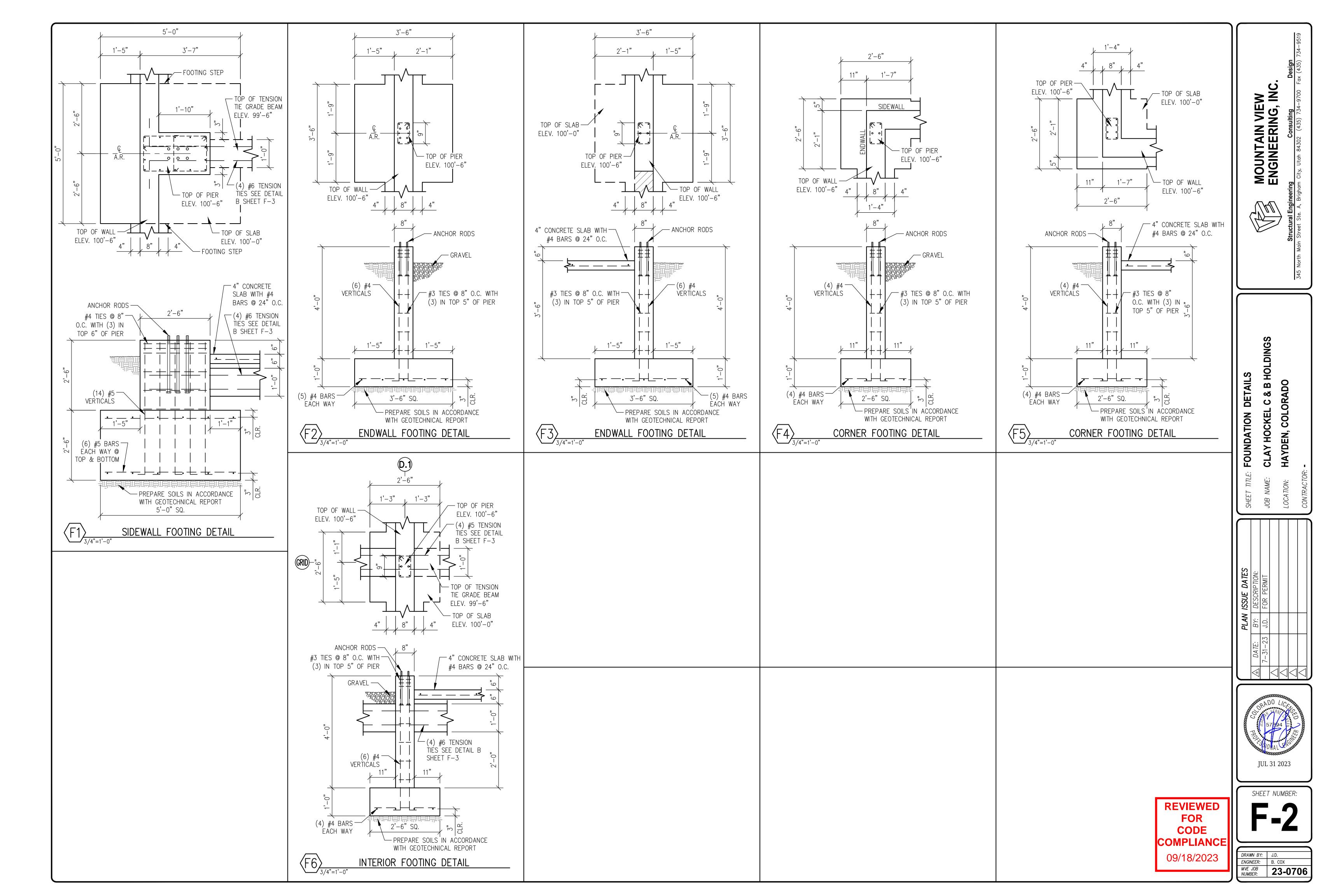
Project Title: Clay Hockel C&B Holdings
Engineer: BLC
Project ID: 23-0706
Project Descr: 65'x70' Metal Building

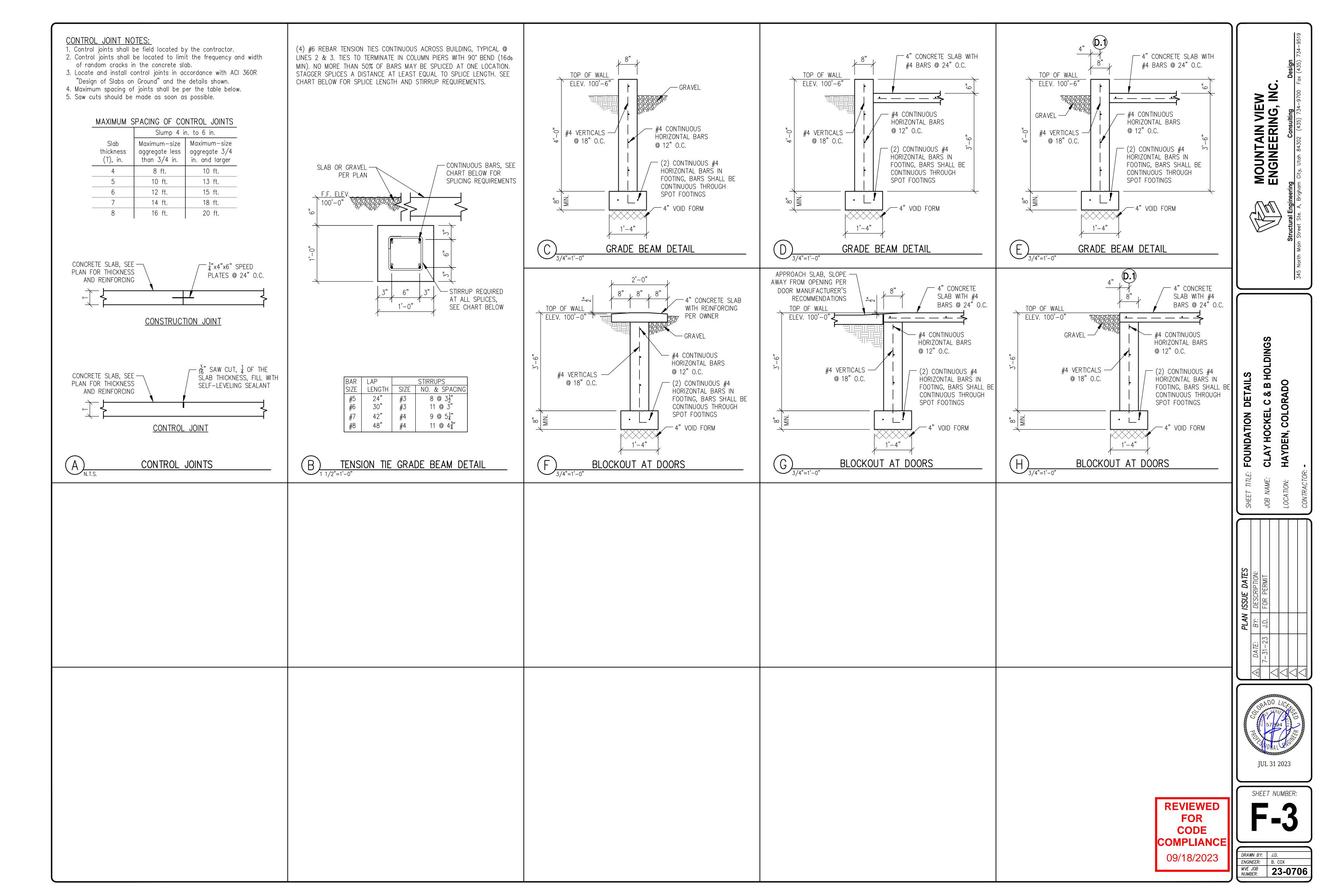
Concrete Beam LIC#: KW-06014791, Build:20.23.07.20 DESCRIPTION: Grade Beam Maximum Forces & Stresses for Lo		VIEW ENGINEERIN	G, INC.		X*=*/,=;155	REVIEWED RCALC INC 1983-2023 FOR CODE COMPLIANCE
Load Combination	au Combinatio	Location (ft)	Bending S	tress Results	(k-ft)	
Segment	Span #	along Beam	Mu : Max	Phi*Mnx	Stress	09/18/2023 Ratio
MAXimum BENDING Envelope Span # 1 +1.40D	1	23.000	86.99	117.30		74
Span # 1 +1.20D	1	23.000	86.99	117.30	0	.74
Span # 1 +0.90D	1	23.000	74.56	117.30	0	64
Span # 1	1	23.000	55.92	117.30	0.	48

Overall Maximum Deflecti	ions	
--------------------------	------	--

Load Combination	Span	Max. "-" Defl (in) .oc	ation in Span (ft Load Combination	Vlax. "+" Defl (in;ocation in Span (ft
D Only	1	0.0247	11.500	0.0000 0.000

FOUNDATION NOTES 1. Design Information and Loads 1. #6 and smaller — 49 bar diameters 2. #7 and larger — 76 bar diameters A. Foundation design in accordance with 2018 International Building b. f'c = 4000 p.s.i. or greater Code using the reactions provided by the metal building MOUNTAIN VIEW ENGINEERING, INC 1. #6 and smaller — 38 bar diameters manufacturer for the following design criteria. 70'-0" 2. #7 and larger — 60 bar diameters B. Ground Snow Load 80 psf c. Increase lap splice lengths by 50% where epoxy coated bars Roof Snow Load 60 psf are used. 23'-4" 23'-4" 23'-4" iii. Stagger splices in walls so that no two adjacent bars are spliced in the same location, unless shown otherwise. $2'-0\frac{1}{2}"$ $8'-8\frac{1}{2}"$ 12'-7" iv. Make all bars continuous around corners or provide corner bars of equal size and spacing. v. Where 12 inches or less of fresh concrete is placed below horizontal reinforcing lap splice length may be reduced by 30%. LOCATE 2. Earthwork $\langle F4 \rangle$ vi. Vertical bars in walls, grade beams, and piers to terminate in A. The foundation has been designed and the site soils should be footings with ACI standard hooks (12 bar diameters) to within (A)prepared for the foundation, in accordance with the 4" of the bottom of the footing unless noted otherwise. FIELD OCATE recommendations in the geotechnical investigation report by: vii. Horizontal wall reinforcing shall terminate at the ends of walls Erika K. Hill, P.E. of NWCC, Inc. with a 90 degree hook plus a 6 bar diameter extension, unless 2580 Copper Ridge Drive, Steamboat Springs, CO 80487 shown otherwise. - TOP OF FOOTING Phone: (970) 879–7888 Job Number: 22–12817 viii. Horizontal wall reinforcing shall be continuous through B. Foundation Design Values ELEV. 98'-6" (TYP. — TOP OF PIER ELEV. construction and control joints. i. Allowable Soil Bearing Pressure - 3500 psf AT ALL F1 FOOTINGS) ix. Splices in horizontal reinforcement shall be staggered. Splices in 100'-6" (TYP.) ii. Minimum Soil Bearing Pressure — 1500 psf two curtains (where used) shall not occur in the same location. iii. Coefficient of Friction — 0.25 (Assumed) x. Use chairs or other support devices as required for proper iiii. Passive Earth Pressure — 250 psf/ft of depth (Assumed) GRAVEL F.F. ELEV. 100'-0" C. The site soils shall be prepared for the foundation in accordance xi. Rebar hairpins shall be centered in slabs and shall be wire tied with the geotechnical report referenced above. The contractor shall TOP OF FOOTING ELEV. to the slab reinforcing (if any). Rebar hairpins shall be verify that soil under footings is suitable to support footings. 96'-6" (TYP. U.N.O.) continuous through walls and piers; lap splices in hairpins may (f B)-D. It is the responsibility of the contractor to ensure that the depth only occur in the floor slab unless noted otherwise. of the bottom of the foundation is far enough below the adjacent C. Control joints in slabs on grade are recommended to control grade to ensure adequate frost protection. cracking. See plans for control joint spacing and details. D. Slabs and grade beams shall not have joints in a horizontal plane. 3. Concrete and Reinforcement All reinforcement shall be continuous through all construction TOP OF TENSION A. Material Standards TIE GRADE BEAM i. Concrete E. Floor slab thickness and reinforcing shown in these drawings are ELEV. 99'-6" a. Footings: Exposure Classes FO, SO, WO, CO adequate to support typical uniform loads only. Mountain View f'c = 3000 p.s.i., max. w/cm ratio = 0.55 -BLOCKOUT AT ALL Engineering has not designed the slab for any specific concentrated b. Exterior Walls: Exposure Classes F1, S0, W0, C1 DOORS SEE DETAIL F forces such as those from vehicles, storage racks, or heavy —(4) #6 TENSION TIES @ f'c = 3500 p.s.i., max. w/cm ratio = 0.55SHEET F-3 (TYP. U.N.O.) equipment (unless noted otherwise). c. Interior Walls: Exposure Classes FO, SO, WO, CO LINES 2 & 3 SEE DETAIL F. Welding of rebar is not allowed unless specifically indicated in the f'c = 3000 p.s.i., max. w/cm ratio = N.A. B SHEET F-3 (TYP.) drawings. All embedments, reinforcing, and dowels shall be securely $\mathbf{\omega}$ d. Interior Slabs: Exposure Classes FO, SO, WO, CO tied to framework or to adjacent reinforcing prior to placement of FOUNDATION PLAN f'c = 3500 p.s.i., max. w/cm ratio = 0.55 the concrete. Tack welding of rebar joints in grade beams, walls, CLAY HOCKEL C e. Air content for Exposures F1-F3 must meet the or cages is not allowed. Where welding of rebar is shown in the requirements of Table 19.3.3.1 of ACI 318-14. Air-entraining drawings, all rebar to be welded shall be ASTM A706 Grade 60. (c)admixtures shall conform to ASTM C260 f. Use Type II cement for Exposure Class SO. For Exposure 4. Special Inspections Classes S1, S2 and S3 use Type II or Type V as required in A. Concrete Table 19.3.2.1 of ACI 318-14. Cement shall conform to ASTM TOP OF WALL ELEV. i. Spot Footings - Not required (IBC 1705.3 Exception 1) BLOCKOUT AT ii. Continuous Ftgs. — Not required (IBC 1705.3 Exception 2.3) q. Calcium Chloride admixture shall not be used in Exposures 100'-6" (TYP.) C AR CAR DOOR SEE DETAIL iii. Slabs - Not required (IBC 1705.3 Exception 3) 4 *****, OF S2 and S3 H SHEET F-3 h. Normal weight aggregates — ASTM C33 iv. Grade Beams — Not required (IBC 1705.3 Exception 4) ii. Reinforcing v. Walls - Not required (IBC 1705.3 Exception 4) (D.) a. Rebar - ASTM A615 Grade 60 (Fy = 60 ksi) vi. Anchor rods/bolts - Required (IBC Table 1705.3) Special b. Welded wire - ASTM A1064 inspection may be waived subject to the approval of the c. Epoxy/Adhesive - Simpson SET-XP (ICC-ES ESR-2508), building official. 3'-11" (E)FIELD LOCATE Hilti RE-500V3 (ICC-ES ELC-3814), or Dewalt Pure110+ B. Steel Reinforcement BLOCKOUT AT — (ICC-ES ESR-3298) unless noted otherwise in the drawings. i. Placement - Third party special inspection of reinforcing DOOR SEE DETAIL placement need only be performed where specifically required by iii. Anchor Rods/Bolts G SHEET F-3 a. All anchor rods shall be cast—in—place headed anchor rods. ii. Welding — Special inspection of rebar welding is required (if any Use of post-installed (epoxy, adhesive, expansion, screw, 4" CONCRETE SLAB WITH #4 is used). etc.) anchors is not allowed without written permission from BARS @ 24" O.C. ON SOILS MVE or unless specifically noted in the drawings. PERPARED IN ACCORDANCE b. Steel column anchor rods/bolts — ASTM F1554 Grade 36 5. Miscellaneous - BLOCKOUT AT TO GEOTECHNICAL REPORT DOOR SEE DETAIL with ASTM A563 heavy hex nuts and hardened washers A. The contractor shall notify engineer of any variations in F.F. ELEV. 100'-0" G SHEET F-3 (unless noted otherwise) — BLOCKOUT AT c. Wood framing anchors — ASTM A307 with A36 plate washers B. The engineer is not responsible for any deviations from these plans DOOR SEE DETAIL _ _ | | _ unless such changes are authorized in writing by the engineer. d. Headed stud anchors (HSA) — ASTM A108 G SHEET F-3 e. Deformed bar anchors (DBA) — ASTM A496 f. Screw Anchors for jambs as indicated in the typical anchor rod schedule - Simpson Titen HD (ICC-ES ESR-2713), Hilti $\langle F5 \rangle$ Kwik HUS-TZ (ICC-ES ESR-3027), or Dewalt Screwbolt+ (ICC-ES ESR-2526) g. Use of hooked anchor rods/bolts is limited under the ACI TYPICAL ANCHOR ROD DIMENSIONS FIELD LOCATE 3'-11" and the IBC. Headed anchor rods/bolts must be used where DIA. EMBED NOTE: VERIFY ALL DOOR SIZES indicated in the details. AND LOCATIONS WITH METAL 10" h. The symbols \mathcal{Q} A.R./ \mathcal{Q} A.B. as shown in the drawings FOUNDATION PLAN CONCRETE NOTE: COORDINATE THIS DRAWING WITH F1 INDICATES APPLICABLE FOOTING DETAIL. BUILDING OUTLET CORP. PRIOR TO indicate the center line of the anchor rod/bolt pattern, not 12" THE METAL BUILDING OUTLET SCALE: 3/16"=1'-0" CONSTRUCTION. BLOCKOUT AT CORP. ANCHOR BOLT PLAN. the center line of any individual anchor rod/bolt. 14" ALL DOORS SEE DETAILS F, G, B. Detail reinforcing to comply with ACI 315 "Manual of Standard AND H SHEET F-3. 18" Practice for Detailing Reinforcing Concrete Structures" and the 22" Concrete Reinforcing Steel Institute (CRSI) recommendations. OPTION A: 24" i. Minimum clear concrete cover for reinforcement shall be as - OPTION B: THREADED ROD HEADED BOLT TACK follows unless noted otherwise: WITH HEAVY HEX NUT a. Concrete cast directly against and permanently exposed to *AT OPENING JAMBS, $\frac{1}{2}$ "øx4" OR $\frac{5}{8}$ "øx4" SCREW ANCHORS MAY BE USED JUL 31 2023 IN LIEU OF CAST-IN-PLACE ANCHORS. OPENING JAMB ANCHORS ARE b. Concrete exposed to weather or earth: NOT SHOWN ON THIS DRAWING, SEE METAL BUILDING ANCHOR PLAN. 1. #5 bars or smaller $-1\frac{1}{2}$ " CONTROL JOINTS, FIELD 2. #6 bars or larger - 2" LOCATE, SEE DETAIL A SHEET NUMBER: c. Concrete not exposed to weather or in contact with the ON SHEET F-3 AND ground $-\frac{3}{4}$ " NOTE 3C THIS SHEET **REVIEWED** d. Slabs on grade — as shown in details, $\frac{3}{4}$ min. from top of **FOR** slabs not exposed to weather CODE ii. Lap Splice Lengths with $1\frac{1}{2}$ minimum clear cover a. f'c = 2500-3500 p.s.i. COMPLIANCE DRAWN BY: J.D. ENGINEER: B. COX 09/18/2023 MVE JOB NUMBER: **23-0706**





ERECTION NOTES

- 1. All bracing shown and provided by the Metal Building Provider (MBP) for this building is required and shall be installed by the erector as a permanent part of the structure ("Code of Standard Practice for Steel Buildings" in the ANSI/AISC 303-16; Section 7.10).
- 2. Temporary supports, such as guys, braces, falsework, cribbing or other elements required for the erection operation shall be determined and furnished by the erector ("Code of Standard Practice for Steel Buildings and Bridges" in the ANSI/AISC 303-16; Section 7.10.3).
- 3. Normal erection operations include the correction of minor misfits by moderate amounts of reaming, grinding, welding or cutting, and the drawing of elements into line through use of drift pins. Errors which require major changes in the member configuration are to be reported immediately to the Metal Building Provider by the customer to enable whoever is responsible either to correct the error or to approve the most efficient and economic method of correction to be used by others ("Code of Standard Practice for Steel Buildings and Bridges "in the ANSI/AISC 303-16; Section 7.14).
- 4. Erection tolerances are set forth in the "Code of Standard Practice for Steel Buildings and Bridges" in the ANSI/AISC 303-16; Section 7.13 note that individual members are considered plump, level and aligned if the deviation does not exceed 1:500. Variations in finished overall dimensions of structure steel framing are deemed within the limits of good practice when they do not exceed the cumulative effect of rolling, fabricating, and erection tolerances.
- When crane support systems are part of the metal building system erection tolerances Section 6.8, Erection Tolerances, 2018 MBMA Metal Building Systems manual shall apply. To achieve the required tolerances grouting of the columns and shimming of the runway beams may be required. The customer shall provide grout if required. The contractor erecting the runway beams is responsible for shimming, plumbing, and leveling of the runway system. When aligning the runway beams the alignment shall be with respect to the beam webs so that the center of the gligned rail is over the runway web.
- 5. As a general rule field welding is not used to assemble a metal building system. In cases where the drawings indicate field welding and in cases where approved corrections are to be made by field welding the following requirements shall be met;
- welders must be qualified by an independent testing agency, with suitable documentation to AWS D1.1 Structural Welding Code -Steel or AWS D1.3 Structural Welding Code — Sheet as applicable, for the processes, positions, and materials involved.
- All welds must be made in conformance to a documented and approved Welding Procedure Specification (WPS). All joints which are not pregualified must be supported by a certified Procedure Qualification Record (PQR) by an independent testing agency. 6. All documentation and records shall be the responsibility of the customer.
- 7. Any claims or shortages by buyer must be made to the Metal Building Provider within seven (7) working days after delivery, or such claims will be considered to have been waived by the customer and disallowed. All claims should be directed to the Metal Building Provider's Customer Service Department.
- 8. Claims for correction of alleged misfits will be disallowed unless the Metal Building Provider shall have received prior notice thereof and allowed reasonable inspection of such misfits. Ordinary inaccuracies of shop work shall not be construed as misfits. No part of the building may be returned or charges assessed for alleged misfits without prior approval from the Metal Building Provider.
- 9. Neither the Metal Building Provider nor the customer will cut, drill or otherwise after their work, or the work of other trades to accommodate other trades unless such work is clearly specified in the contract documents. Whenever such work is specified the customer is responsible for furnishing complete information as to materials, size, location, and number of alterations prior to preparation of shop drawings ("Code of Standard Practice for Steel Buildings and Bridges" in the ANSI/AISC 303-16, Section 7.15). 10. The Metal Building Provider Field Modifications Policy:
- 10.1. The Metal Building Provider will only be responsible for the field-modified parts designed and approved by the Metal Building Provider's Customer Service Department.
- 10.2. Any field modifications designed by third parties may not be approved by the Metal Building Provider and may limit the Metal Building Provider's warranty and liability.
- The Metal Building Provider makes no warranty and hereby disclaims any responsibility with respect to the design, engineering, or construction of any field-modified parts performed by third parties.
- WARNING SOME PANÉLS AND TRIM PARTS ARE FURNISHED WITH A PROTECTIVE PEEL-OFF FILM. PARTS PROVIDED WITH THIS FILM CANNOT BE EXPOSED TO SUNLIGHT WITHOUT FIRST REMOVING THE FILM. THIS FILM MUST BE REMOVED PRIOR TO INSTALLATION, FILM MUST ALSO BE REMOVED FROM ALL NON EXPOSED PARTS WITHIN SIX MONTHS FROM FILM APPLICATION OR IRREPARABLE DAMAGE WILL OCCUR TO THE SURFACE CLAIMS WILL NOT BE ACCEPTED FOR THIS ISSUE.

RESPONSIBILITIES

- 1. The Metal Building Provider Customer, hereafter referred to as the "customer," obtains and pays for all building permits, licenses, public assessments, paving or utility pro rata, utility connections, occupancy fees and other fees required by any governmental authority or utility in connection with the work provided for in the Contract Documents. The customer provides at his expense all plans and specifications required to obtain a building permit. it is the customer's responsibility to ensure that all plans and specifications comply with the applicable requirements of any governing building authorities.
- 2. The customer is responsible for identifying all applicable building codes, zoning codes, or other regulations applicable to the Construction Project, including the Metal Building system.
- 3. It is the responsibility of the customer to interpret all aspects of the End User's specifications and incorporate the appropriate specifications, design criteria, and design loads into the Order Documents submitted to the Metal Building Provider.
- 4. It is the responsibility of the Metal Building Provider to furnish the metal building system to meet the specifications including the design criteria and design loads incorporated by the Contractor into the Order Documents. The Metal Building Provider is not responsible for making an independent determination of any local codes or any other requirements not part of the Order Document.
- 5. The Metal Building Provider's standard specifications apply unless stipulated otherwise in the Contract Documents. The Metal Building Provider design, fabrication, quality criteria, standards, practice, methods and tolerances shall govern the work any other interpretations to the contrary not with standing, it is understood by both parties that the customer is responsible for clarifications of inclusions or exclusions from the Architectural plans.
- 6. In case of discrepancies between the Metal Building Provider's structural steel plans and plans for other trades, the Metal Building Provider's shall govern ("Code of Standard Practice for Steel Buildings and Bridges" in the AISC 303-16; Section 3.3).
- 7. The customer is responsible for overall project coordination. All interface, compatibility and design considerations concerning any materials not furnished by the Metal Building Provider and the Metal Building Provider's steel system are to be considered and coordinated by the customer. Specific design criteria concerning this interface between materials must be furnished by the customer before release for fabrication or the Metal Building Provider's assumptions will govern.
- 8. Foundations, anchor rods, and anchor rod embedment are designed, furnished, and set by the customer in accordance with an approved drawing. Dimensional accuracy shall satisfy the requirements of Section 7.5 1 of "Code of Standard Practice for Steel Buildings and Bridges" in the AISC 303-16.
- 9. All other embedded items or connection materials between the structural steel and the work of other trades are located and set by the customer in accordance with approved location on erection drawings. Accuracy of these items must satisfy the erection tolerance
- 10. The Metal Building Provider does not investigate the influence of the metal building system on existing buildings or structures. The End Customer assures that such buildings and structures are adequate to resist snow drifts, wind loads, or other conditions as a result of the presence of the metal building system.

GENERAL SPECIFICATIONS

- 1. Wall and liner panels are an integral part of the structural system. Unauthorized removal of panels or cutting panels for framed openings not shown is prohibited.
- Oil-canning, a perceived waviness inherent to light gauge metal, may exist. This condition does not affect the structural integrity or the finish of the panel, and therefor is not a cause for rejection.
- The Metal Building Provider's red-oxide and gray-oxide primer are designed for short term field protection from exposure to ordinary atmospheric conditions. Primed steel which is stored in the field pending erection should be kept free of the ground, and so positioned as to minimize water-holding pockets, dust, mud, and other contamination of the primer film. Repairs of damage to primed surfaces and/or removal of foreign material due to transportation (e.g. road salt, de—icing chemicals and other substances encountered during transportation that may accelerate deterioration of the primer or corrosion of the underlying steel), improper field storage, or site conditions are not the responsibility of the Metal Building Provider. (MBMA, 2018 MBSM, Section 4.2.4)
- 4. All bolts are 1/2" x 1-1/4" A307 unless noted. Refer to the erection drawings for specific framing connections and the cross-section(s) for main frame connections.
- 5. Unless noted otherwise on the frame cross section(s), all bolted joints with ASTM F3125 Grade A325 bolts are specified as snug-tightened joints in accordance with the specification for Structural Joints Using High-Strength Bolts, June 11, 2020. Installation Inspection requirements for Snug-Tight Bolts (Specification for Structural joints, Section 9.1) is suggested.
- 6. Unless noted otherwise, all bolted connections are designed as bearing type connections with bolt threads not excluded from the
- 7. Any type of suspended or load inducing system(s) is prohibited if zero collateral and zero sprinkler loads are designated on the contract. This would include lights, duct work, piping, and insulation types other than 3" standard duty fiberglass blanket

BUILDING DESIGN CODES Building Code: Hot-rolled version:	<u>IBC 18</u> AISC 360-16
Cold-formed version:	AISI S100-16
GENERAL LOADS Dead Load:	3.10 psf
Roof Collateral Load: Sprinkler Load: Roof Live Load:	1.00 psf (Misc.) 0.00 psf 20.00 psf
Tributary Live Load Reduction: Rainfall Intensity:	NO 4.00 in/hr (5-minute duration 5-year recurrence)
WIND LOAD Wind Load (3—sec gust) Vult: Vasd:	115_ mph 89_mph
Vusu. V service:	77 mph
Exposure Factor: Wind Condition:	C Enclosed
Internal Pressure Coefficient : Edge Zone Width:	+/- 0.18 6.50 Ft
SNOW LOAD Ground Snow Load :	80.00 pof
Roof Snow Load :	80.00 psf 60.00 psf
Importance Factor:	1.00
Exposure Factor: Thermal Factor:	<u>1.00</u> 1.00
Slope Factor:	1.00
Main Frames Horizontal: H/60 Main Frames Vertical: L/180 Bearing Frame Rafter: L/180 Endwall Columns: L/120 Wind Frame Horizontal : H/60	Roof Panels: L/60 Purlins: L/180 Wall Panels: L/60 Girts: L/90
For components, claddings and MWFRS, defle 10 year serviceability wind pressures.	ections involving wind are based on
SEISMIC LOAD	II. Marraral
Risk Category: Seismic Importance Factor :	II <u>– Normal</u> 1.0000
Structural Response Acceleration (Ss): Structural Response Acceleration(S1): Site Class:	0.4190 0.0862 D
Design Spectral Response (Sds):	0.4092
Design Spectral Response (Sd1): Seismic Design Category:	0.1376 C
Framing Direction: Structural Syst:	Lateral Longitudinal 'Structural Steel Systems Not Specif Detailed for Seismic Resistance'
Response Modification Factor(s) :	3.03.0
Deflection Amplification: Sesimic Response Coefficient(s) (Cs):	$\frac{3.0}{0.1365} \qquad \frac{3.0}{0.1365}$
Design Base Shear V :	
Analysis Procedure:	Equivalent Lateral Force
ROOF PANEL	
	26 Color: SMP Royal Blue

FOR APPROVAL:

FOR CONSTRUCTION PERMIT:

Final drawings for construction

Profile: Reverse Rolled Super Span X Gauge: 26 Color: SMP Steel Gray

Profile: Super Span X Gauge: <u>26</u> Color: <u>SMP Steel Gray</u>

PRIMARY FRAMING

Built-Up & Hot-Rolled: Gray Oxide Primer

SECONDARY FRAMING

These drawings, being for approval, are by definition not final and are

proper interpretation of the project documents. Only drawings issued "F

for conceptual representation only. Their purpose is to confirm the

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Erector Installation" can be considered complete.

Purlins, Eave Struts: Pre-Galvanized Girts, Light Gage Columns: Pre-Galvanized Light Gage Jambs & Headers: Pre-Galvanized Base Angle Finish: Pre-Galvanized

Hot-Dip Galvanizing conforms to the ASTM A123 specification. Pre-Galvanized members conform to the ASTM A653, Grade 50, Coating G-90 specification.

APPROVAL SPECIFICATIONS

- 1. Approval of the Metal Building Provider drawings and/or calculations indicate that the Metal Building Provider has correctly interpreted the contact requirements. This approval constitutes the customer acceptance of the Metal Building Provider design, concepts. assumptions, and loadings.
- 2. Failure to respond to clouded areas and areas to verify may result in additional costs and/or schedule delays for which the Metal Building Provider will not be responsible.
- 3. Anv changes made after the Metal Building Provider's customer has signed and returned the Metal Building Provider drawings and/or calculations and the project is released for fabrication shall be billed to the Metal Building Provider customer including material, engineering, and other costs. An additional fee may be charged if the project must be moved in the fabrication and/or the shipping
- 4. It is the responsibility of the customer to field verify all existing conditions prior to fabrication.
- 5. It is imperative that any changes to these drawings:
- 5.1. Be made in contrasting ink.
- 5.2. Be legible and unambiguous.
- 5.3. Have all instances of changes clearly indicated.
- 6. A dated signature, in the designated areas, is required on all pages. The signature must be from the person authorized on the contract or a person authorized, in writing, by the Metal Building Provider customer.
- 7. The Metal Building Provider reserves the right to resubmit drawings with extensive or complex changes required to avoid misfabrication. This may impact the delivery schedule.
- 8. Any changes noted on the drawings not in conformance with the terms and requirements of the contract between the Metal Building Provider and its customer are not binding on the Metal Building Provider unless subsequently acknowledged and agreed to in writing by change order or separate documentation.
- 9. Waiving the approval process by designating the order "For Production" supercedes notes 1,2,5,6, and 8 in this section, and constitutes the customer acceptance of the Metal Building Provider's design, concepts, assumptions, and loadings.

DRAWING SCHEDULE

DWG NO.	ISSUE	DATE	DESCRIPTION
C1	0	08.02.23	COVER SHEET
F1	1	07.20.23	ANCHOR BOLT PLAN
F2	1	07.20.23	ANCHOR BOLT DETAILS
F3	1	07.20.23	ANCHOR BOLT REACTIONS
F4	1	07.20.23	ANCHOR BOLT REACTIONS
P1	0	08.02.23	RIGID FRAME ELEVATION
E1	0	08.02.23	ROOF FRAMING PLAN
E2	0	08.02.23	ROOF SHEETING PLAN
E3	0	08.02.23	ENDWALL FRAME & SHEETING ELEVATION
E4	0	08.02.23	ENDWALL FRAME & SHEETING ELEVATION
E5	0	08.02.23	SIDEWALL FRAME & SHEETING ELEVATION
E6	0	08.02.23	SIDEWALL FRAME & SHEETING ELEVATION
E7	0	08.02.23	PARTITION FRAME & SHEETING ELEVATION
E8	0	08.02.23	BUILDING SECTIONS
E9	0	08.02.23	BUILDING SECTIONS
D1	0	08.02.23	STANDARD DETAILS PAGE
D2	0	08.02.23	STANDARD DETAILS PAGE
D3	0	08.02.23	STANDARD DETAILS PAGE
D4	0	08.02.23	STANDARD DETAILS PAGE

TRIM COLOR:		
Shadow Rake:	SMP Royal Blue	GAUGE: <u>26</u>
Shadow Eave:	SMP Royal Blue	GAUGE: 26
CORNER:	SMP Royal Blue	GAUGE: 26
ACCESSORY:	SMP Royal Blue	GAUGE: 26
SOFFIT TRIM:	SMP Royal Blue	GAUGE: <u>26</u>
PARTITION TRIM:	SMP Royal Blue	GAUGE: <u>26</u>
BASE Trim:	SMP Royal Blue	GAUGE: <u>26</u>

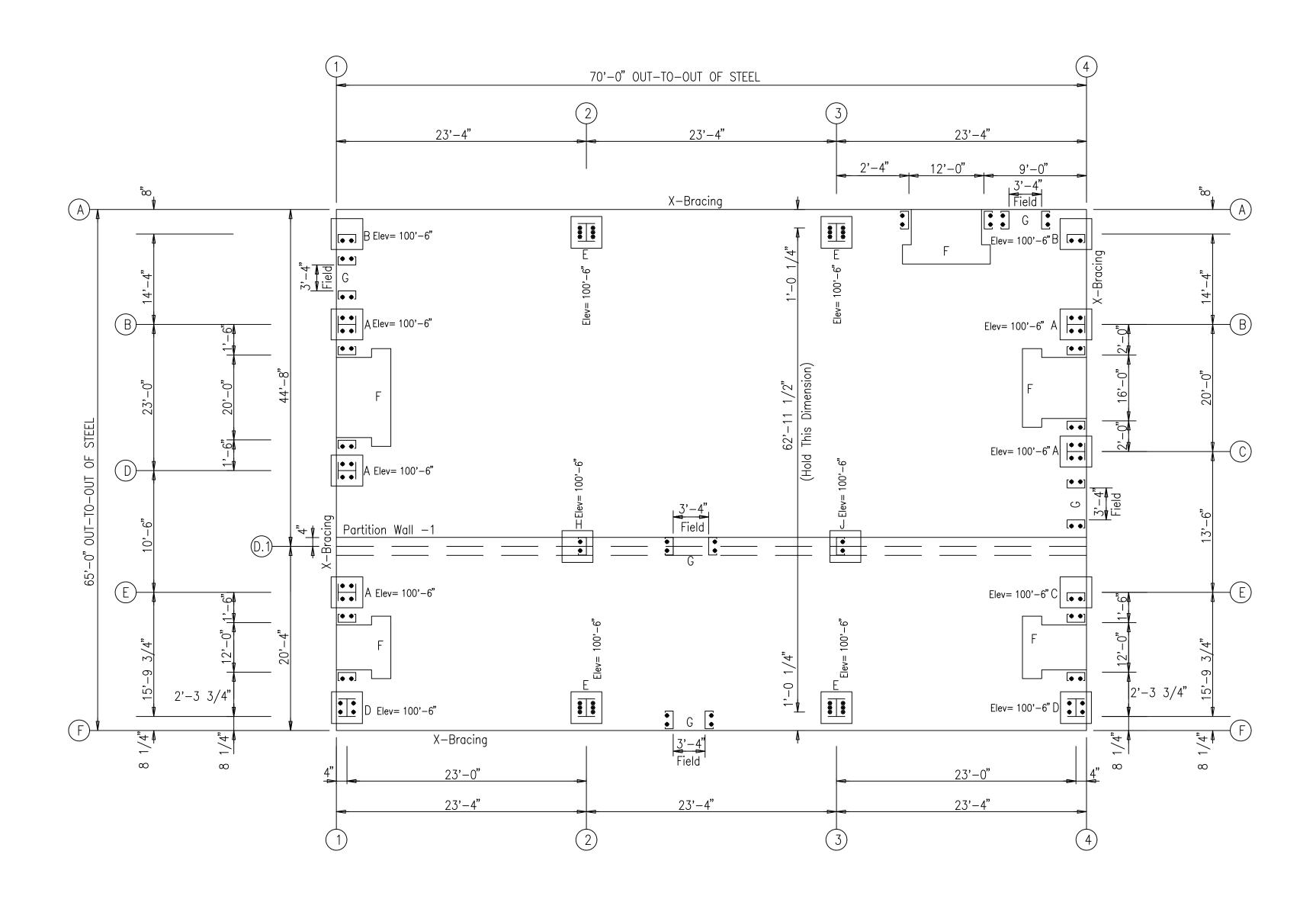
The Engineer whose seal and signature appear on these documents represents Whirlwind Steel Buildings, Inc., and is not the Engineer of Record for the overall project. The Engineer's responsibility is limited to material designed and manufactured by Whirlwind Steel Buildings, Ir and excludes part such as doors, windows, foundation design, and erection of the building.

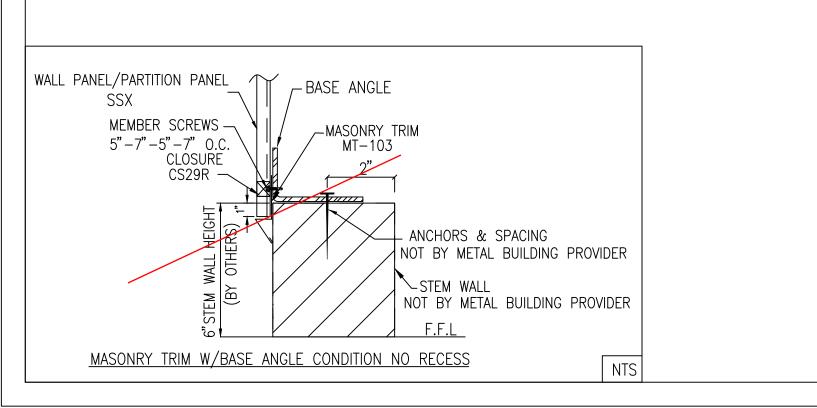
FOR CODE COMPLIANCE 09/18/2023

REVIEWED

SHEET DESCRIPTION: DATE DESCRIPTION 65'-0" x 70'-0" x 18'-0"/14'-3" 06.19.23 FOR CONSTRUCTION PERMIT PND PNC CUSTOMER: THUNDERSTRUCK / C&B HOLDINGS HAYDEN, CO 81639 P2 07.20.23 REV.FOR CONSTRUCTION PERMIT PND PNC METALBUILDING PROJECT REFERENCE: 08.02.23 FOR ERECTOR INSTALLATION PND PNC THUNDERSTRUCK / C&B HOLDINGS 7651 SHAFFER PARKWAY LITTLETON, CO 8012 HAYDEN, CO 81639 LIOR NO: 08.02.23 KMO 11217-32005 PNC C1









NOTE: All Base Plates @ 100'-0" (U.N.)

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These drawings, being for approval, are by definition not final and are for conceptual representation only. Their purpose is to confirm the ISSUE DATE DESCRIPTION 65'-0" x 70'-0" x 18'-0"/14'-3"

CUSTOMER LOCATION: ANCHOR BOLT PLAN 0 06.19.23 FOR ERECTOR INSTALLATION PND PNC CUSTOMER: 06.19.23 FOR ERECTOR INSTALLATION PND PNC THUNDERSTRI
PROJECT REFERENCE:
PROJECT REFERENCE: THUNDERSTRUCK / C&B HOLDINGS HAYDEN, CO 81639 proper interpretation of the project documents. Only drawings issued "For METALBUILDING
OUTLET CORP.
7651 SHAFFER PARKWAY LITTLETON, CO 80127 Proper interpretation of the project documents. Only drawings issued in Erector Installation" can be considered complete.

FOR CONSTRUCTION PERMIT:

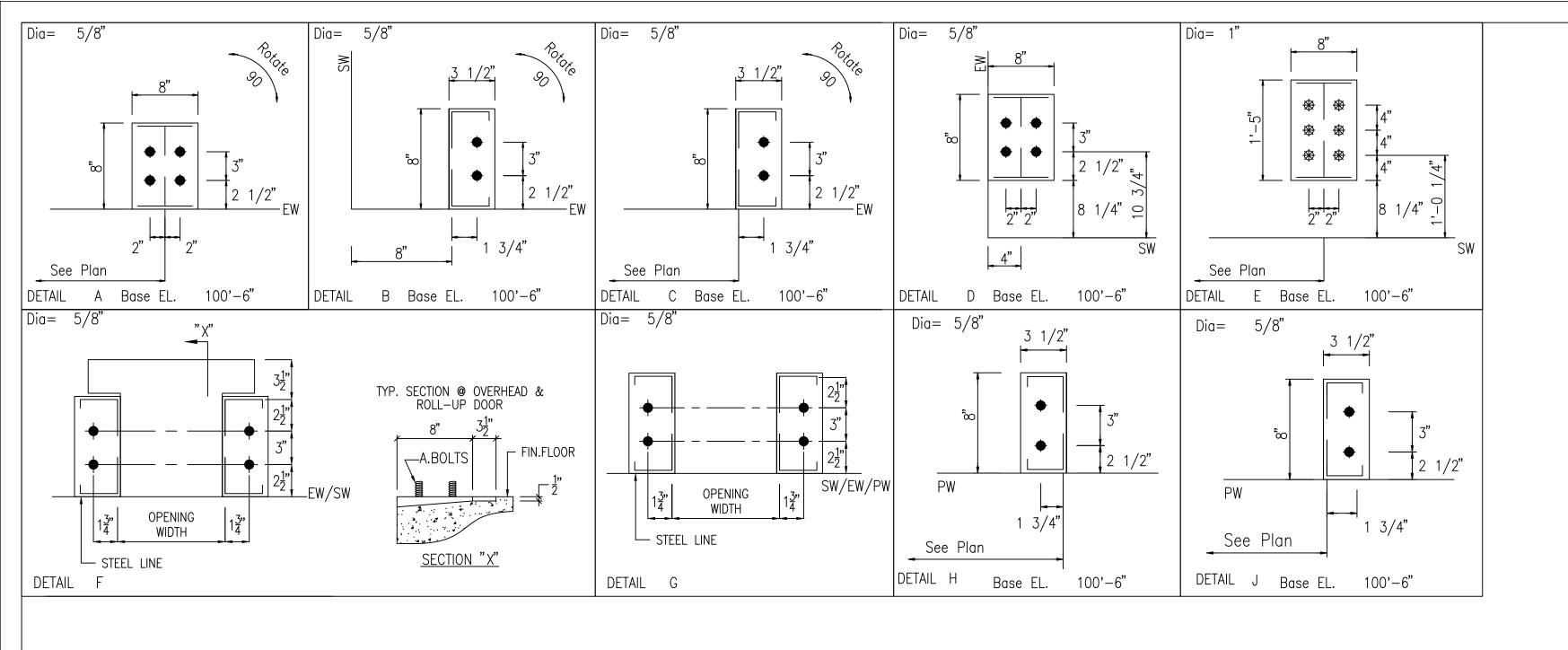
These drawings, being for permit, are by definition not final. Only drawings issued "For Erector Installation" can be considered complete.

FOR ERECTOR INSTALLATION:

Final drawings for construction. THUNDERSTRUCK / C&B HOLDINGS JOBSITE LOCATION:

REVIEWED FOR CODE COMPLIANCE 09/18/2023

JOBSITE COUNTY:



The Engineer whose seal and signature appear on these documents represents Whirlwind Steel Buildings, Inc., and is not the Engineer of Record for the overall project. The Engineer's responsibility is limited to material designed and manufactured by Whirlwind Steel Buildings, Inc., and excludes part such as doors, windows, foundation design, and erection of the building.

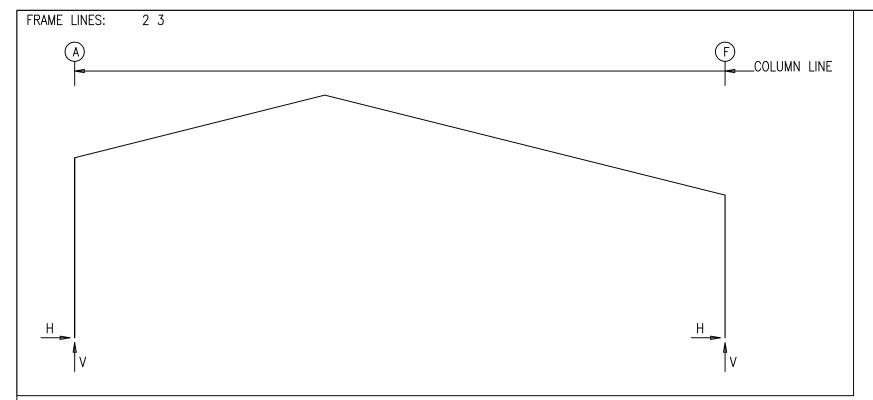
FOR APPROVAL:
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FOR CONSTRUCTION PERMIT:
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FOR ERECTOR INSTALLATION:
Final drawings for construction.

METALBUILDING
7651 SHAFFER PARKWAY LITTLETON, CO 80127

CODE COMPLIANCE 09/18/2023

REVIEWED

FOR



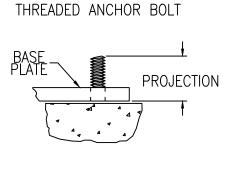
RIGID	FRAME:		MAXIMUM	REACTION	S, ANCH	IOR BOLTS	, & BASE	PLATE	S				
Frm Line	Col Line	Load Id	——— Coli Hmax H	umn_React V Vmax	tions(k Load Id) Hmin H	V Vmin	Bol Qty	t(in) Dia	Base Width	e_Plate(in) Length	Thick	Elev. (in)
2*	Α	1	30.3	53.7	2 4	-5.7 -1.1	-8.5 -9.2	6	1.000	8.000	17.00	0.500	6.0
2*	F	3 7	5.6 -28.3	-8.9 53.6	1 5	-30.3 1.6	53.1 -9.3	6	1.000	8.000	17.00	0.500	6.0
2*	Frame lir	nes:	2 3										

RIGI	D FRAN	ΛE:	BASI	C COLUM	n reacti	ONS (k)							
Frame Line 2* 2*	Column Line A F	 Horiz 2.1 -2.1	-Dead Vert 4.4 4.2		nteral— Vert 0.8 0.8	 Horiz 9.2 -9.2	-Live Vert 16.2 16.0	 Horiz 27.7 -27.7	-Snow Vert 48.5 48.1	-—-Wind Horiz -11.7 3.4	Left1- Vert -18.6 -12.8	−Wind_ Horiz −4.7 11.5	Right1- Vert -14.0 -19.1
Frame Line 2* 2*	Column Line A F	Wind Horiz -9.4 1.1	d_Left2- Vert -11.5 -5.7	−Wind_ Horiz −2.7 9.5	Right2- Vert -7.0 -12.0	Wind Horiz -4.0 5.4	_Long1- Vert -19.7 -15.8	Wind Horiz -6.7 4.8	LLong2- Vert -19.0 -19.6	-Seism Horiz -1.8 -2.5	ic_Left Vert -0.9 0.9	Seismic Horiz 1.8 2.5	_Right Vert 0.9 -0.9
Frame Line 2* 2*	Column Line A F	-Seism Horiz 0.0 0.0	vert Vert -4.7 -3.5	-MIN_S Horiz 9.2 -9.2	NOW Vert 16.1 16.0	F1UNB_ Horiz 20.0 –20.0	SL_L- Vert 48.0 22.6	F1UNB_ Horiz 25.7 –25.7	SL_R- Vert 31.3 48.6				
2*	Frame lin	nes:	2 3										

GENERAL NOTES

- 1. All anchor bolts (by others) to have nuts and flat washers.
- 2. All anchor bolts are designed to full S.A.E. diameters with cut threads. No substitutions are allowed.
- 3. The Metal Building Provider is not responsible for the design, materials and workmanship of the foundation. Anchor bolt plans prepared by the Metal Building Provider are intended to show only location, diameter, and projection of anchor bolts required to attach the Metal Building System to the foundation. The Metal Building Provider is responsible for providing to the Builder the loads imposed by the Metal Building System on the foundation. It is the responsibility of the End Customer to ensure that adequate provisions are made for specifying bolt embedment, bearing angles, tie rods, and/or other associated items embedded in the concrete foundation, as well as foundation design for the loads imposed by the Metal Building System, other imposed loads, and the bearing capacity of the soil and other conditions of the building site. This is typically the responsibility of the Design Professional or Engineer of Record, which is another reason that their involvement in the Construction Project from the outset is highly recommended. (2012 MBMA Metal Building Systems Manual, Section 3.2.2)

 4. The projection is based from the bottom of the base plate. Adiustments
- 4. The projection is based from the bottom of the base plate. Adjustments must be made for grout and/or leveling plates.



NOTE: PROJECTION BASED FROM BOTTOM OF BASE PLATE. ADJUSTMENTS SHOULD BE MADE FOR GROUT AND/OR LEVELING PLATES.

FNDW		COLU	MNI		BASIC CC	LLIMANI	DEACTIC	NIC (L)									
Frm Line 1 1 1 1	Col Line A B D E	Dead Vert 0.5 1.5 1.3 0.9	Collo Vert 0.1 0.3 0.3 0.2 0.1	t	Live Vert 2.0 6.1 5.1 3.4 2.7	Sno Ver 5.9 18.2 15.4 10.3	ow t 9 2 4 3	Wind_Le Horz 0.0 0.0 -2.8 0.0 -10.88	eft1 Vert -3.6 -8.6 -10.2 1.9 -3.0	Ho 0 0 0 1	ind_Rig orz .0 .0 .0 .9	Vert -2.9 -5.0 -2.9 -10.0	Wind_Le Horz 0.0 0.0 -2.5 0.0 -10.88	vert -2.5 -6.2 -7.8 3.3 -1.9	Wind_F Horz 0.0 0.0 0.0 2.0 2.12	Right2 Vert -1.7 -2.8 -1.0 -8.0 -3.0	
Frm Line 1 1 1 1	Col Line A B D E F	Wind_F Horz 0.0 -4.4 -3.8 -2.6 -6.4	Press Vert 0.0 0.0 0.0 0.0 -3.2	H C 4 4	Wind_Suct lorz Vert 0.0 0.0 4.9 0.0 4.2 0.0 2.9 0.0 0.0 3.2	; l	Wind_Lo Horz 0.0 0.0 0.0 0.0 0.6 0.0	ng1 Vert -3.1 -7.7 -2.7 -4.8 -2.2	Wind_L Horz 0.0 0.0 -2.4 0.0 0.0		ert .7 5.4 .0 .6	Seis_Le Horz 0.0 0.0 -2.8 0.0 0.0	eft Vert 0.1 -0.2 -5.5 5.6 -0.1	Seis_Ri Horz 0.0 0.0 0.0 2.8 0.0	ight Vert -0.1 0.2 4.8 -4.9 0.1	Seis_ Horz 0.0 0.1 0.1 0.0 -7.0	Long Vert 0.0 0.0 0.0 0.0 -3.5
Frm Line 1 1 1 1	Col Line A B D E F	-MIN_ Horz 0.0 0.0 0.0 0.0	SNOW Vert 2.0 6.1 5.1 3.4 2.7	H C C	11UNB_SL_L- lorz Verb 0.0 6.8 0.0 23.5 0.0 7.4 0.0 1.9 0.0 2.5	: 	E1UNB_ Horz 0.0 0.0 0.0 0.0 0.0	SL_R- Vert 0.8 9.7 19.5 9.3 8.4									
Frm Line 4 4 4 4	Col Line F E C B A	Dead Vert 0.7 1.0 1.2 1.4 0.5	Collo Vert 0.1 0.2 0.2 0.3 0.1	t	Live Vert 2.6 4.3 4.8 5.5	Sno Ver 7.8 12.8 14.3 16.5	t 3 3 5	Wind_Le Horz -1.83 0.0 0.0 -1.9 0.0	eft1 Vert -4.2 -7.5 -5.8 -7.6 0.1	Ho 2 0 0 0	ind_Rig orz .12 .0 .0 .0 .8	Vert	Wind_Le Horz -1.83 0.0 0.0 -2.0 0.0	rft2 Vert -3.0 -5.1 -4.3 -5.7	Wind_F Horz 2.12 0.0 0.0 0.0 2.5	Right2 Vert -1.8 -2.5 -2.2 -2.2 -6.2	Wind Press Horz 0.0 -2.9 -4.0 -4.1 0.0
Frm Line 4 4 4 4	Col Line F E C B A	Wind Suct Horz 0.0 3.2 4.4 4.5	Wind Horz 0.0 0.0 0.0 0.0 2.4		Vert H -3.5 (-7.9 (-5.4 (-1.4 -	/ind_Lo lorz).0).0).0).0).6).0	ng2 Vert -2.2 -4.3 -3.5 -8.3 -2.2	Seis Horz 0.0 0.0 0.0 -2.8 0.0	S_Left Vert 0.1 0.3 -0.4 -4.5 4.5		Seis_I Horz 0.0 0.0 0.0 0.0 2.8	Right Vert -0.1 -0.3 0.4 3.8 -3.8	Seis Long Horz 0.0 0.0 0.1 0.1 0.0	Ho 0 0 0 0	.0 2 .0 4 .0 4	/ ert 2.6 4.3 4.8 5.5 2.1	
Frm Line 4 4 4 4	Col Line F E C B A	E2UNB Horz 0.0 0.0 0.0 0.0	Vert 8.2 12.6 18.1 7.6 1.4	H C C	2UNB_SL_R- lorz Verb 0.0 2.4 0.0 3.0 0.0 7.1 0.0 22.6 0.0 7.0												
ENDV	VALL	COLU	MN:		MAXIMUM	REACTIO	DNS, AN	NCHOR BC)LTS, & E	BASE	PLATE	ES .					
Frn Line			Load Hn Id H	nax	olumn_React V Vmax	ons(k Load Id) Hmin H	V Vmi	 n Qt	Bolt(i	n) Dia		se_Plate(Lengtl		Ele k (ir		
1		\		0.0	— ——— −1.8 7.4	2	0.0		.8	2 (0.625		8.000	0.25	50 6	.0	
1	Е	3	9	2.9 0.0	-4.3 25.3	10 9	-2. ²	7 –3 9 –4		4 (0.625	8.000	8.000	0.37	75 6	.0	
1)		2.5 3.0	-5.9 21.0	12 11	-2.5 2.5	3 –5	5.9	4 (0.625	8.000	8.000	0.37	75 6	.0	
1	E		1	1.7 0.0	-5.5 11.3	10 14	-1.0 1.7	7 –5	5.5		0.625	8.000				.0	
1	F		13	0.0	-2.1 9.3	6 12	-4.9 -3.9	9 –3	5.7		0.625	8.000				.0	
4	F		15	0.0 0.0	-2.1 9.0	2	0.0				0.625	8.000				.0	
4	E		1	1.9 0.0	-4.1 14.0 -2.8	10 16	-1.3 1.9	9 –4	l.1		0.625	3.500				.0	
4	C		15	2.6 0.0 2.7	-2.8 19.5 -4.2	10 9	-2.6 2.6	-2	2.8		0.625	8.000				.0	
4	E		17	2.7 0.0	-4.2 24.2 -4.3	12 11 3	-2.5 2.7	7 –4	1.2		0.625	8.000 3.500				.0	
4	٨									o 1	0 605	7 500	9 000	0.25	50	6	6.0

-4.3

BUILDING BRACING REACTIONS ± Reactions(k) Panel_Shear (lb/ft) Line Horz Vert Horz Vert Wind Seis Line __EW 5.0 D,E 2.8 2.8 4.9 3.2 3.8 F_SW 1,2 6.5 7.0 3.5 R_EW B,A 3,2 2.8 2.8 3.8 7.2 4.8 7.1 4.7 B_SW Reactions for seismic represent shear force, Eh

ANCHOR BOLT SUMMARY (GRADE 36) Type Qty Locate 5/8" 5/8" 1" F1554 2.50 Jamb 2.50 3.50 2.50 2.50 F1554 Endwall ₩ 24 Frame F1554 5/8" F1554 Partition Column 5/8" F1554 Partition Jamb

Partition column reactions Dead Load Wind Press Wind Suct Horz. Frame Column Horz. -3.433.43 0.64 -3.433.43 0.64

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FOR APPROVAL:
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4

17

0.0

0.0

-4.3

7.7

3

0.0

Freetor Installation of the project accuments. The considered complete.

FOR CONSTRUCTION PERMIT:

These drawings, being for permit, are by definition not final. Only drawings issued "For Erector Installation" can be considered complete. FOR ERECTOR INSTALLATION:
Final drawings for construction



							•				•		•
	ISSUE	DATE	DESCRIPTION	BY	СНК	SHEET DESCR		BOLT REACTIONS		E	BLDG SIZE:	70'-0" x 18'-0'	'/14' 3"
	0	06.19.23	FOR ERECTOR INSTALLATION	PND	PNC	CUSTOMER:	ANCHOR	DOLI NEACTIONS				IER LOCATION:	/ 14 -3
	1	07.20.23	REV.FOR ERECTOR INSTALLATION	PND	PNC		JNDERSTRUCK	C / C&B HOLDIN	NGS		HAYD	EN, CO 81639	
G						PROJECT REF	ERENCE:						
						THI	UNDERSTRUCK	C&B HOLDING	NGS				
DRP. 80127						JOBSITE LOCA	ATION:					JOBSITE COUNTY:	
						i	HAYDEN, CO	81639				ROUTT	
						DWN:	CHK:	DATE:	ENG:		JOB NO:	DWG NO:	ISSUE:
						PND	PNC	07.20.23	1	KMO	11217-32005	F3	1

2 0.625 3.500 8.000 0.250 6.0

REVIEWED FOR CODE COMPLIANCE 09/18/2023

14 13 14

13

Zone	Width (ft)	Length (ft)	Pressure(psf Member) Panel	Suction(psf Member) Panel
1 2 3 4 5 6 7 8 9 10 11 12 13	6.50 6.50 14.83 4.44 6.50 30.29 2.06 2.06 6.50	4.50 4.50 2.00 2.00 2.00 2.00 2.00 61.00 6.50	16.00 16.00 16.00 16.00 16.00 16.00 16.00 16.00 16.00 24.65 24.65 24.70	18.56 18.56 18.56 18.56 18.56 18.56 18.56 18.56 16.00 16.00 30.61 30.61 30.60	-17.64 -34.22 -34.22 -51.33 -82.38 -91.90 -103.2 -82.38 -38.92 -43.59 -27.25 -29.16 -27.20	-56.56 -82.58 -82.58 -97.85 -91.06 -106.3 -122.2 -91.06 -64.86 -106.4 -33.21 -40.85 -33.20
14	6.50		24.70 (+) wind tow	30.60 vards surf	-29.10 face	-40.84

(+)	wind	towar	ds su	rface
(-)	wind	away	from	surfac

Components & Cladding

	10	9	10
12	6		[€
	5 2	1	2
	7 4	3	4 7
	7 4	3	4 7
12	8 2 6 10	9	2 8

14

12	
11	
12	

14

NOTES FOR REACTIONS

- All loading conditions are examined and only maximum/minimum H or V and the corresponding H or V are reported.
- 2. Positive reactions are as shown in the sketch. Foundation loads are in opposite directions.
- 3. Bracing reactions are in the plane of the brace with the H pointing away from the braced bay. The vertical reaction is downward.
- 4. Building reactions are based on the following building data:

Width (ft)
Length (ft)
Eave Height (ft)
Roof Slope (rise/12)
Dead Load (psf)
Collateral Load (psf) = 65.0 = 70.0 = 18.0/14.3 = 3.0/3.0 = 3.1 = 1.0 = 20.0 Live Load (psf ") Snow Load`'(psf = 60.0 Wind Speed (mph ') = 115.0Wind Code = IBC 18 Exposure = C Closure = Enclosed Importance Wind = 1.00 Importance Seismic = 1.00 Seismic Zone = C Seismic Coeff (Fa*Ss) = 0.61

5. Loading conditions are:

- Dead+Collateral+Snow+Slide_Snow
- 0.6Dead+0.6Wind_Left1

- 0.6Dead+0.6Wind_Right1 0.6Dead+0.6Wind_Long1L 0.6Dead+0.6Wind_Long2L
- 0.54Dead+0.7Seismic_LongL Dead+Collateral+F1UNB_SL_R
- Dead+Collateral+E1UNB_SL_L
 0.6Dead+0.6Wind_Left1+0.6Wind_Suction
- 10 0.6Dead+0.6Wind_Pressure+0.6Wind_Long1L 11 0.6Dead+0.6Wind_Suction+0.6Wind_Long2L 12 0.6Dead+0.6Wind_Pressure+0.6Wind_Long2L
- 13 Dead+Collateral+E1UNB_SL_R
 14 0.6Dead+0.6Wind_Right1+0.6Wind_Suction
 15 Dead+Collateral+E2UNB_SL_L
- 16 0.6Dead+0.6Wind_Suction+0.6Wind_Long1L 17 Dead+Collateral+E2UNB_SL_R

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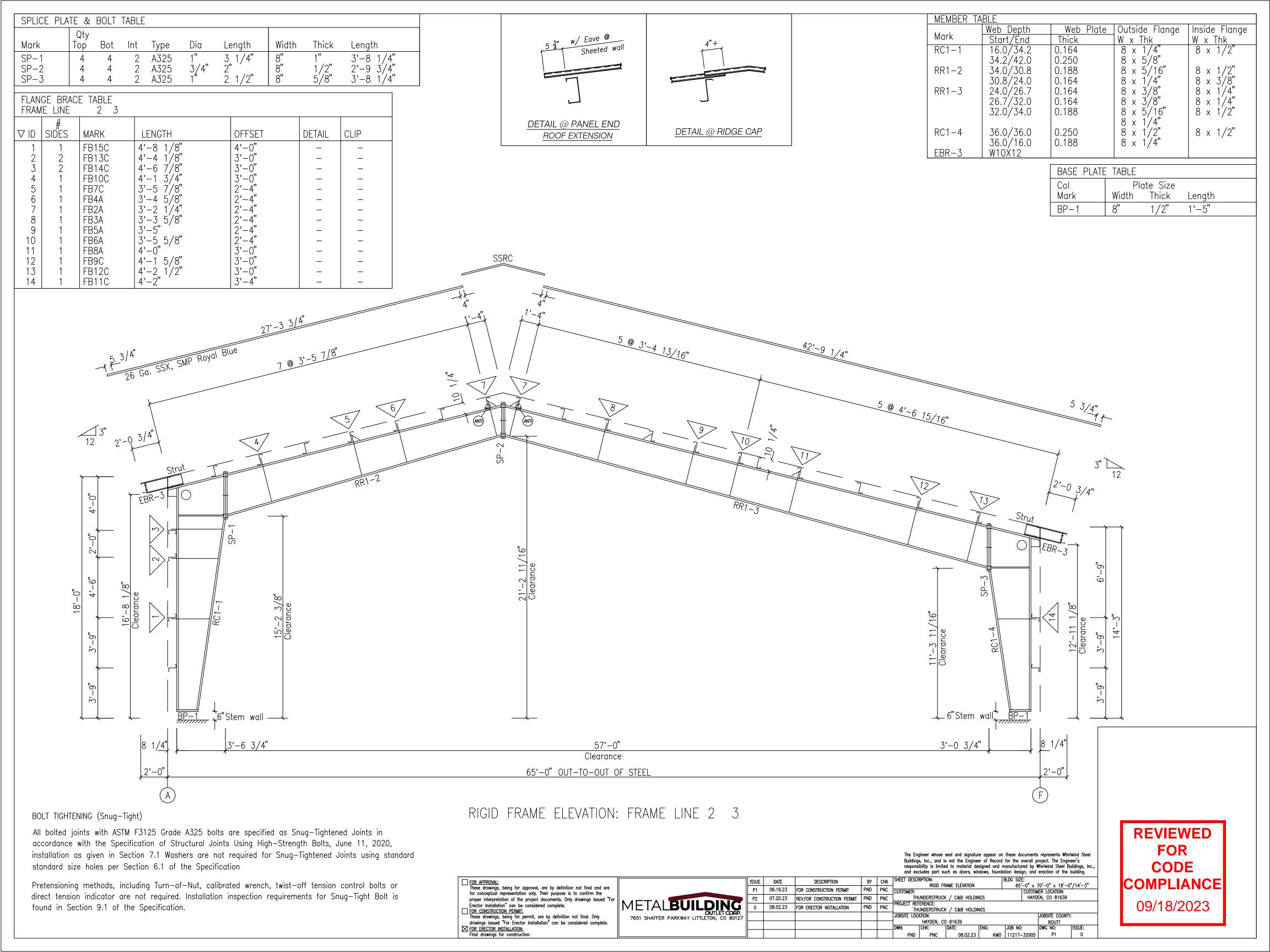
FOR CONSTRUCTION PERMIT:
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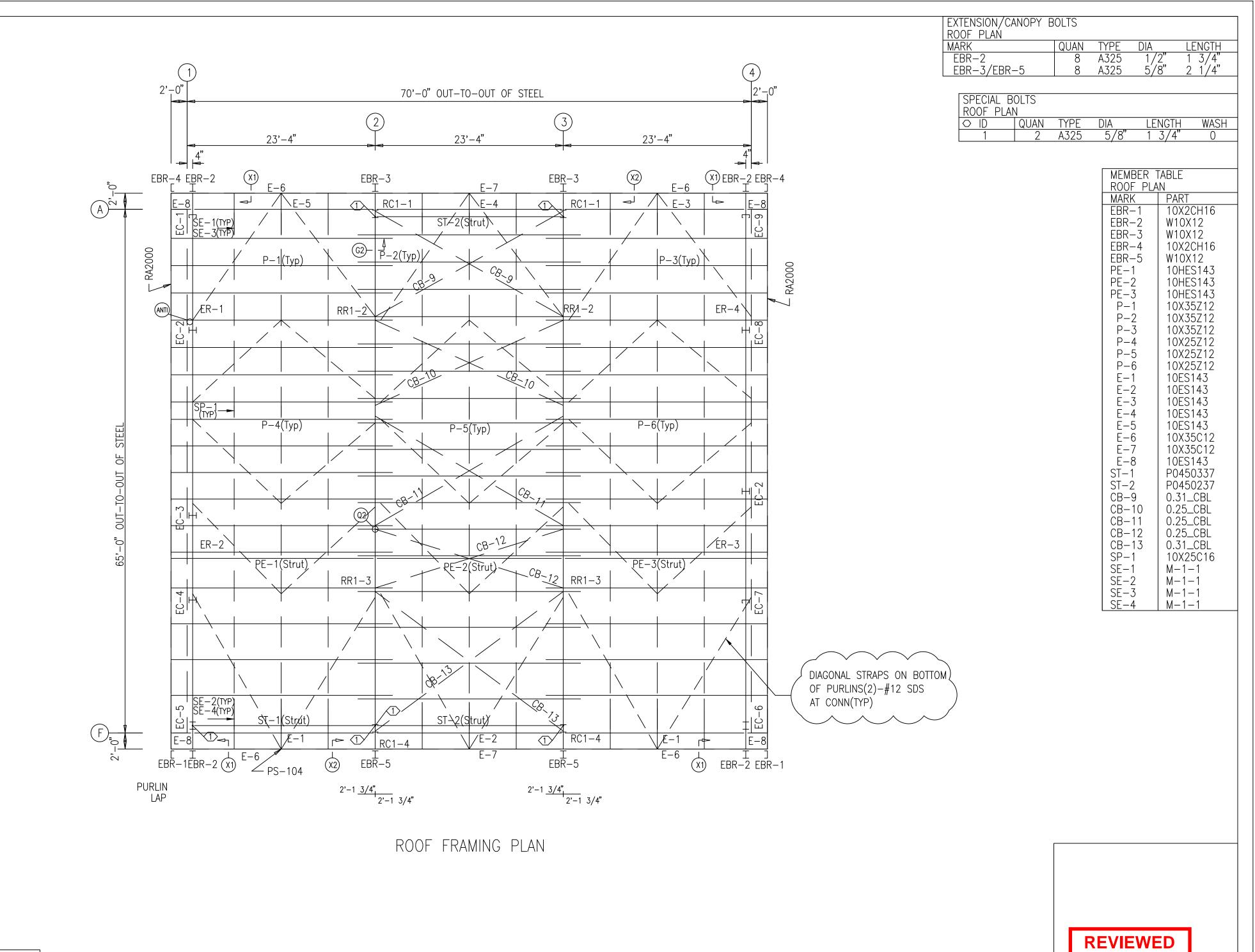
FOR ERECTOR INSTALLATION:
Final drawings for construction.

METALBUILDING
OUTLET CORP
7651 SHAFFER PARKWAY LITTLETON, CO 8012

	ISSUE	DATE	DESCRIPTION	BY	СНК	SHEET DESCH	RIPTION: ANCHOR	BLDG SIZE: 65'-0" x	70'-0" x 18'-0'	"/14'-3"			
	0	06.19.23	FOR ERECTOR INSTALLATION	PND	PNC	CUSTOMER:	7			ISTOMER LOCATION:			
	1	07.20.23	REV.FOR ERECTOR INSTALLATION	PND	PNC		THUNDERSTRUCK / C&B HOLDINGS HAYDEN, CO 81639						
P.						PROJECT REF	erence: Understruck						
						JOBSITE LOC			JOBSITE COUNTY:				
						1	HAYDEN, CO		ROUTT				
						DWN:	CHK:	DATE:	ENG:	JOB NO:	DWG NO:	ISSUE:	
						PND	PNC	07.20.23	KMO	11217-32005	F4	1	

REVIEWED FOR CODE COMPLIANCE 09/18/2023





UL580, CLASS 90 CONST. NUMBER 167

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BY CHK SHEET DESCRIPTION: I BLDG SIZE: | ISSUE | DATE | DESCRIPTION | BY CHK | STILL! DESCRIPTION | PND | PNC | CUSTOMER: 65'-0" x 70'-0" x 18'-0"/14'-3"

CUSTOMER LOCATION: ROOF FRAMING PLAN P2 07.20.23 REV.FOR CONSTRUCTION PERMIT PND PNC THUNDERSTRU
0 08.02.23 FOR ERECTOR INSTALLATION PND PNC THUNDERSTRU
THUNDERSTRU THUNDERSTRUCK / C&B HOLDINGS HAYDEN, CO 81639 THUNDERSTRUCK / C&B HOLDINGS JOBSITE LOCATION:

FOR CODE COMPLIANCE 09/18/2023

FOR APPROVAL:
These drawings, being for approval, are by definition not final and are for conceptual representation only. Their purpose is to confirm the proper interpretation of the project documents. Only drawings issued "For Proper interpretation of the project accuments. Only drawings issued in Erector Installation" can be considered complete.

FOR CONSTRUCTION PERMIT:

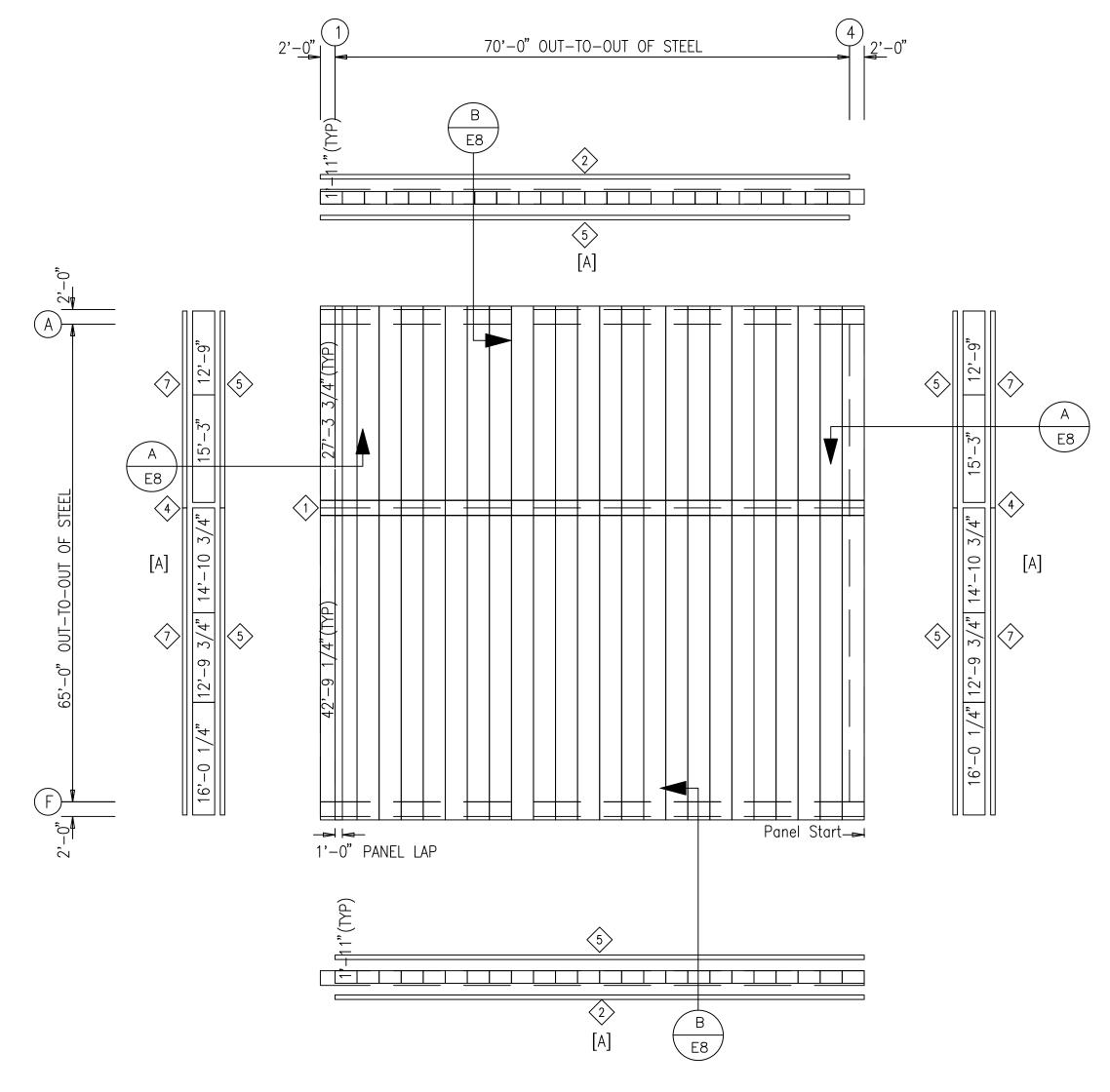
These drawings, being for permit, are by definition not final. Only drawings issued "For Erector Installation" can be considered complete.

FOR ERECTOR INSTALLATION:

Final drawings for construction.

.	METAL BUILDING
	7651 SHAFFER PARKWAY LITTLETON, CO 80127

ROOF	SHEETING	TRIM TABLE
$\Diamond ID$	PART	LENGTH
1	SSRC30	3'-0"
2	SF-12	15'-3"
4	CF-110	10'-3"
5	CF-116	15'-3"
7	SF-11	15'-3"
	◇ID 1 2 4	1 SSRC30 2 SF-12 4 CF-110 5 CF-116



ROOF SHEETING PLAN

PANELS: 26 Ga. SSX - SMP Royal Blue

[A] SOFFIT PANELS: 26 Ga. Reverse Rolled SSX — SMP Steel Gray

DESCRIPTION

08.02.23 FOR ERECTOR INSTALLATION

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BY CHK SHEET DESCRIPTION: BLDG SIZE:
65'-0" x 70'-0" x 18'-0"/14'-3"

CUSTOMER LOCATION:
HAYDEN, CO 81639 ROOF SHEETING PLAN PND PNC CUSTOMER: THUNDERSTRUCK / C&B HOLDINGS

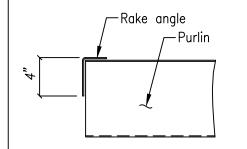
PROJECT REFERENCE: P2 07.20.23 REV.FOR CONSTRUCTION PERMIT PND PNC PND PNC | PROJECT REFERENCE: | THUNDERSTRUCK / C&B HOLDINGS | JOBSITE COUNTY: | JOBSITE LOCATION: | ROUTT | PND | PNC | D8.02.23 | KMO | 11217-32005 | E2 | 0

FOR CODE COMPLIANCE 09/18/2023

REVIEWED

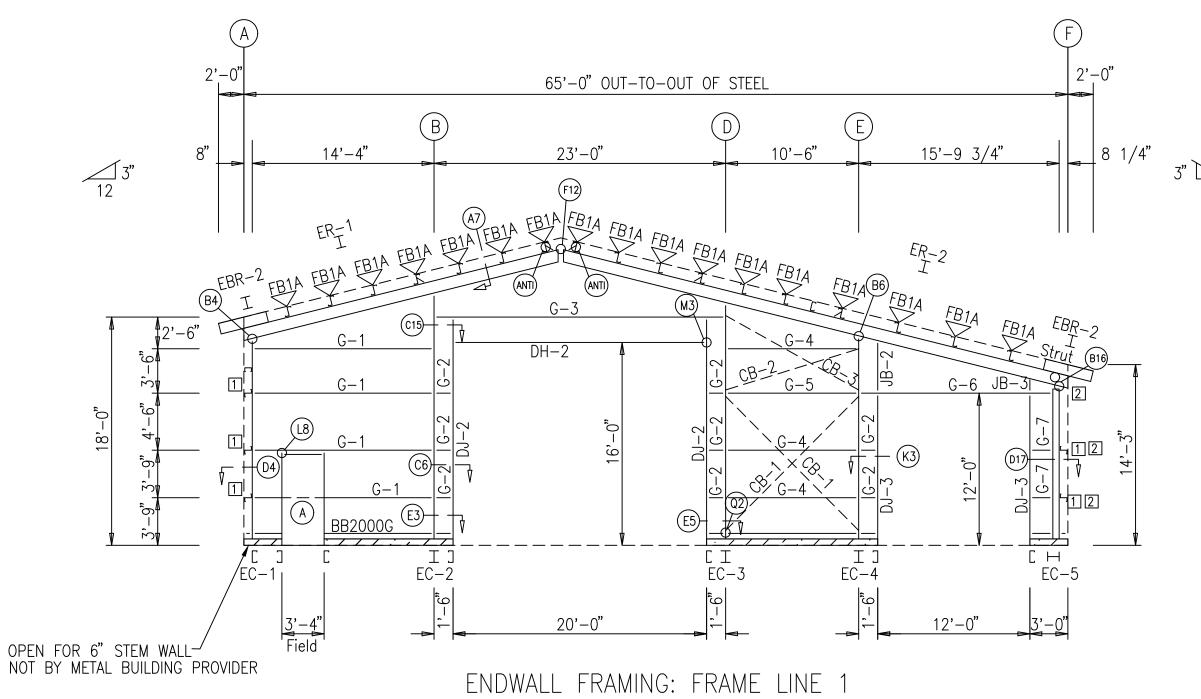
| FOR APPROVAL:
These drawings, being for approval, are by definition not final and are for conceptual representation only. Their purpose is to confirm the proper interpretation of the project documents. Only drawings issued "For Erector Installation" can be considered complete.
| FOR CONSTRUCTION PERMIT:
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| FOR ERECTOR INSTALLATION:
Final drawings for construction.

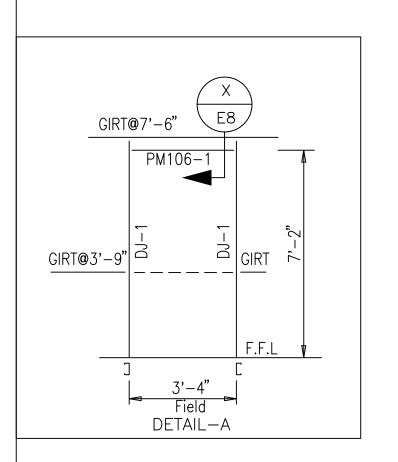
ISSUE DATE P1 06.19.23 FOR CONSTRUCTION PERMIT METALBUILDING OUTLET CORP. 7651 SHAFFER PARKWAY LITTLETON, CO 80127

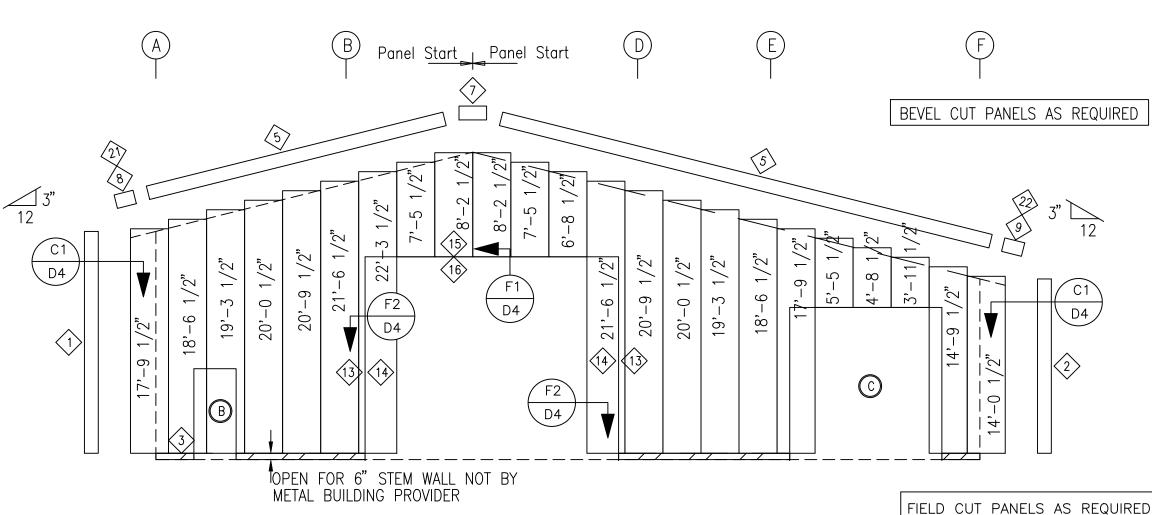


<u>Detail at Rake Angle</u>

TRIM TABLE — THIS WALL ONLY FRAME LINE —1						
♦ID	LENGTH					
1 2 3 5 7 8 9 10 12 13 14 15 16 17 18 19 20 21 22	CT-102 CT-102 MT-103 RT-101 SPB SPCB-3L SPCB-3R JT-101 MT-116B JT-101 MT-116B HT-101 MT-116B HT-101 SF-3L SF-3R	18'-4" 14'-7" 20'-3" 15'-3" 7'-6" 3'-8" 16'-4" 15'-10" 20'-3" 20'-3" 12'-4" 11'-10" 12'-4" 12'-4"				







BOLT TABLE FRAME LINE 1 LOCATION ER-1/ER-2 EC-1/ER-1 Int_Column/Raf EC-5/ER-2 LENGTH QUAN 5/8" 5/8" 5/8" 5/8" 5/8" A325 A325 A325 A325 A325 A325 1 1/2" 1 1/2" 2" 1 1/2" JB-2 & JB-3/ER-2

FLA	NGE BRACE TA	ABLE
FRA	AME LINE 1	
$\triangle ID$	MARK	LENGTH
1	FB1A	2'-6 3/4"

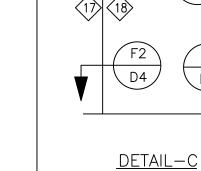
	NECTION PLATES
FRAM	E LINE 1
	MARK/PART
1	SC-5
2	Z-1

PAR1

MEMBER TABLE

FRAME LINE 1

IVIAINN	LANI
EBR-2	W10X12
EC-1	8M35C14
EC-2	W8X10
EC-3	W8X10
EC-4	W8X10
EC-5	W8X10
ER-1	W12X14
ER-2	W12X14
DJ-1	8M25C14
DJ-2	8M35C12
DJ-3	8M35C14
JB-2	8M35C14
JB-3	8M35C14
PM106-1	PM106
DH-2	8M25C14
G-1	8X25Z16
G-2	8X25Z16
G-3	8X25Z12
G-4	8X25Z16
Ğ-5	8X25Z12
G-6	8X25C14
G-7	8X25Z16
CB-1	0.50_CBL
CB-2	0.38_CBL
CB-3	0.38_CBL
	0.00_00L



D4

<u>DETAIL-B</u>

GENERAL SHEETING & TRIM NOTES

- Refer to erection drawings for rake angle locations.
 Roof member screws are at 12" o.c. Eave end lap and peak screws are as shown.
- 3. Wall member screws are at 6" o.c. at the base member and 12" o.c. at all remaining members.

 4. Roof stitch screws are located at each member with two between members (20" max. spacing).
- 5. Wall stitch screws are located at each member with one between members (20" max. spacing). 6. Skylight stitch screws are at 6" o.c.
- 7. Start endwall panels at centerline of bldg. unless noted. 8. Gutter, rake, & eave trim lap 2". All other trims lap 1".
- 9. Field cut or lap panels as required to fit.

- 10. Field cut panels as required to the.

 11. Pop rivet gutter counterflashing to wall panel on 3'-0 centers and caulk all laps.

 12. Gutter support strap spacing: Super Span 3'-0, Super Seam 4'-0, Weather Lok-16 2'-8".

 13. Corner and/or peak boxes are not furnished with special rake or gutter profiles. Field miter as req'd.

 14. Downspout straps are located 6" from base and at every girt location.
- 15. Hot-rolled or built-up members must be pre-drilled before attaching members screws. 16. Metal shavings must be swept from the roof each day to avoid surface rusting.
- 17. Windows and louvers must be installed before sheeting the walls.
- 18. For clarity, tape sealant, closures, etc. may not be shown. Refer to the standing seam erection manual or standard pull out for screw-down type roof for additional installation instructions.

GENERAL FRAMING NOTES

ENDWALL SHEETING & TRIM: FRAME LINE 1

PANELS: 26 Ga. SSX — SMP Steel Gray

FOR ERECTOR INSTALLATION:
Final drawings for construction

- 1. Angles are marked by their length in feet and inches. 2. Field cut or lap angles as required to fit.
- 3. Flange braces are marked by their length in decimal inches.
- 4. Outside flange of girt turns down unless noted.
- 5. Endwall girts and eave struts do not lap.6. Field cut and self—tap girts at walk doors.
- 7. Field slot girts for brace rods or cables.
- 8. Field locate windows and walk doors. 9. Field weld all splices at 14 gauge valley gutters.
- 9. Field weld all splices at 14 gauge valley gatters.

 10. Field bolt AK400 base clip to endwall columns:

 (2) 5/8" x 1-1/2" A325 bolts if (1) AK400 req'd

 (2) 5/8" x 1-3/4" A325 bolts if (2) AK400 req'd
- 11. Locate top of roof framed openings flush with the pan of the roof panel.
- 12. Some field drilling at framed openings may be required. Field drill 9/16" diameter holes. 13. For clarity, tape sealant, closures, etc. may not be shown. Refer to the standing seam erection
- manual or standard pull out for screw-down type roof for additional installation instructions. 14. Sub-jambs for overhead doors, if required, is not furnished by Metal Building Provider

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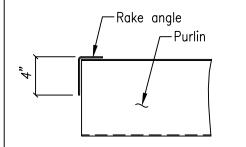
	ISSUE	DATE	DESCRIPTION	BY	СНК	SHEE
	P1	06.19.23	FOR CONSTRUCTION PERMIT	PND	PNC	CUSTO
	P2	07.20.23	REV.FOR CONSTRUCTION PERMIT	PND	PNC	DD0 11
DING	0	08.02.23	FOR ERECTOR INSTALLATION	PND	PNC	PROJE
OUTLET CORP. ETON, CO 80127						JOBSI
						DWN

	responsi	ibility is limite	d to material de ch as doors, wir	signed and m	anufa	ctured by W	/hirlwind Steel Bu	ıildings, Inc.,
CHK	SHEET DESCR			1 -	SLDG S			
	ENI	DWALL FRAME	& SHEETING ELE	VATION	(65'-0" x 7	'0'-0" x 18'-0	"/14'–3"
PNC	CUSTOMER:			•		CUSTOM	ER LOCATION:	
PNC	THUNDERSTRUCK / C&B HOLDINGS HAYDEN, CO 81639							
PNC	PROJECT REF		C&B HOLDIN	NGS		•		
	JOBSITE LOCA	ATION:					JOBSITE COUNTY	:
	HAYDEN, CO 81639 ROUTT							
	DWN:	CHK:	DATE:	ENG:	JOB	NO:	DWG NO:	ISSUE:

The Engineer whose seal and signature appear on these documents represents Whirlwind Steel

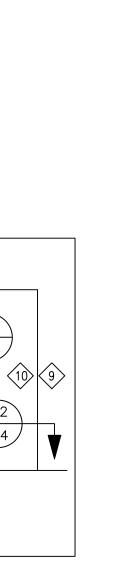
08.02.23 KMO 11217-32005

REVIEWED FOR CODE COMPLIANCE 09/18/2023



Detail at Rake Angle

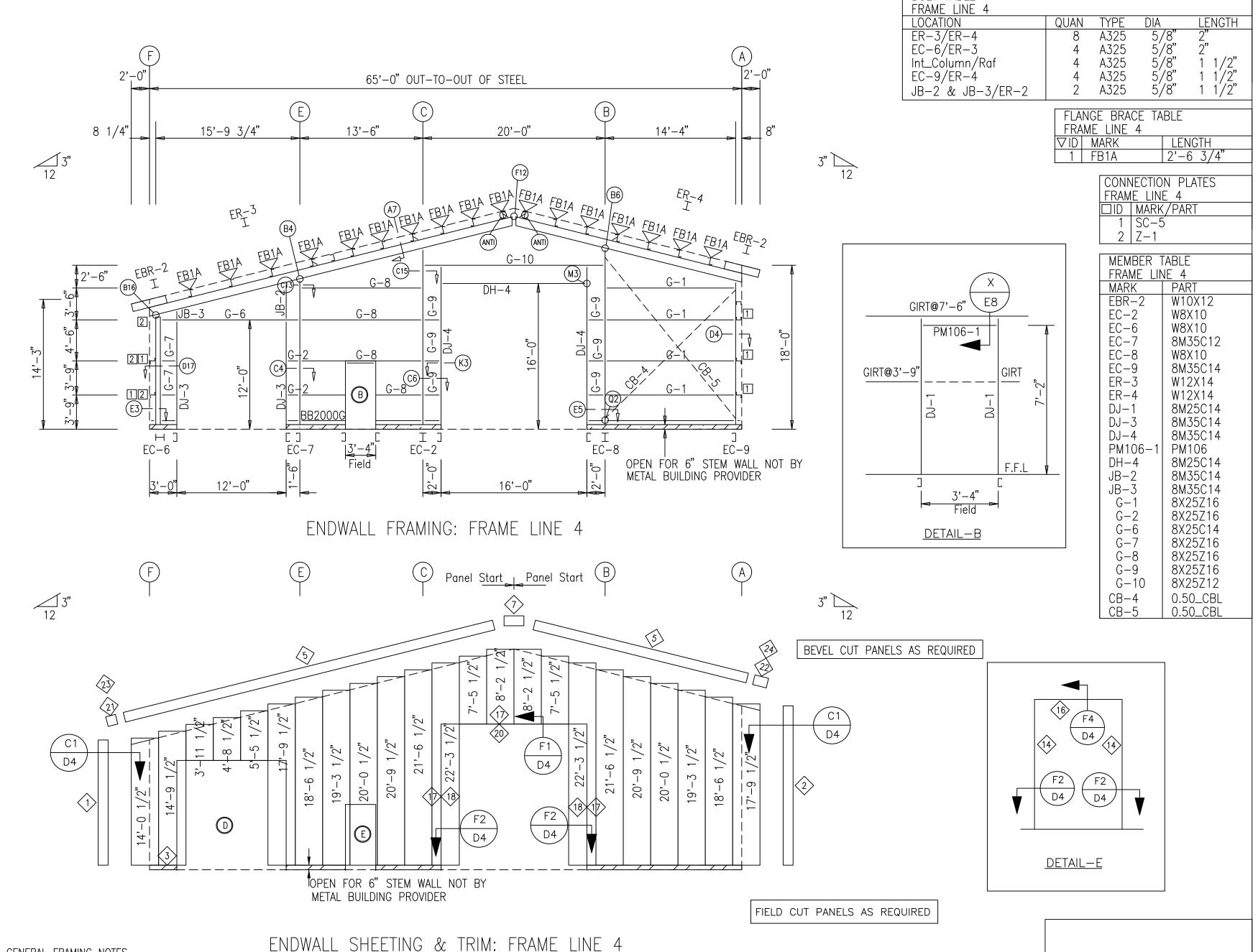
	TABLE – THIS LINE – 4	WALL ONLY
♦ID	PART	LENGTH
1 2 3 5 7 9 10 11 12 14 16 17 18 20 21 22 23 24	CT-102 CT-102 MT-103 RT-101 SPB MT-116B JT-101 MT-116B HT-101 JT-101 HT-101 SPCB-3L SPCB-3R SF-3L SF-3R	14'-7" 18'-4" 20'-3" 15'-3" 12'-4" 11'-10" 12'-4" 7'-6" 3'-8" 16'-4" 15'-10" 16'-4"



D4 /

D4 /

<u>DETAIL-D</u>



GENERAL SHEETING & TRIM NOTES

- Refer to erection drawings for rake angle locations.
 Roof member screws are at 12" o.c. Eave end lap and peak screws are as shown.
- 3. Wall member screws are at 6" o.c. at the base member and 12" o.c. at all remaining members. 4. Roof stitch screws are located at each member with two between members (20" max. spacing).
- 5. Wall stitch screws are located at each member with one between members (20" max. spacing). 6. Skylight stitch screws are at 6" o.c.
- 7. Start endwall panels at centerline of bldg. unless noted.
- 8. Gutter, rake, & eave trim lap 2". All other trims lap 1".
- 9. Field cut or lap panels as required to fit. 10. Field cut panels for all openings.
- 11. Pop rivet gutter counterflashing to wall panel on 3'-0 centers and caulk all laps.
- 12. Gutter support strap spacing: Super Span 3'-0, Super Seam 4'-0, Weather Lok-16 2'-8".

 13. Corner and/or peak boxes are not furnished with special rake or gutter profiles. Field miter as req'd.
- 14. Downspout straps are located 6" from base and at every girt location.
- 15. Hot-rolled or built-up members must be pre-drilled before attaching members screws. 16. Metal shavings must be swept from the roof each day to avoid surface rusting.
- 17. Windows and louvers must be installed before sheeting the walls.
- 18. For clarity, tape sealant, closures, etc. may not be shown. Refer to the standing seam erection manual or standard pull out for screw-down type roof for additional installation instructions.

GENERAL FRAMING NOTES

- 1. Angles are marked by their length in feet and inches.
- 2. Field cut or lap angles as required to fit. 3. Flange braces are marked by their length in decimal inches.
- 4. Outside flange of girt turns down unless noted. 5. Endwall girts and eave struts do not lap.
- 6. Field cut and self-tap girts at walk doors. 7. Field slot girts for brace rods or cables.
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- 12. Some field drilling at framed openings may be required. Field drill 9/16" diameter holes.
- 13. For clarity, tape sealant, closures, etc. may not be shown. Refer to the standing seam erection manual or standard pull out for screw-down type roof for additional installation instructions. 14. Sub-jambs for overhead doors, if required, is not furnished by Metal Building Provider

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METALBUILDING 7651 SHAFFER PARKWAY LITTLETON, CO 8012

PANELS: 26 Ga. SSX - SMP Steel Gray

DATE DESCRIPTION P1 06.19.23 PND PNC CUSTOMER: FOR CONSTRUCTION PERMIT REV.FOR CONSTRUCTION PERMIT PND PNC 07.20.23 PROJECT REFERENCE: PND PNC 08.02.23 FOR ERECTOR INSTALLATION JOBSITE LOCATION:

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BOLT TABLE

BY CHK SHEET DESCRIPTION: BLDG SIZE: ENDWALL FRAME & SHEETING ELEVATION 65'-0" x 70'-0" x 18'-0"/14'-3" CUSTOMER LOCATION: THUNDERSTRUCK / C&B HOLDINGS

JOB NO:

ROUTT DWG NO:

E4

THUNDERSTRUCK / C&B HOLDINGS

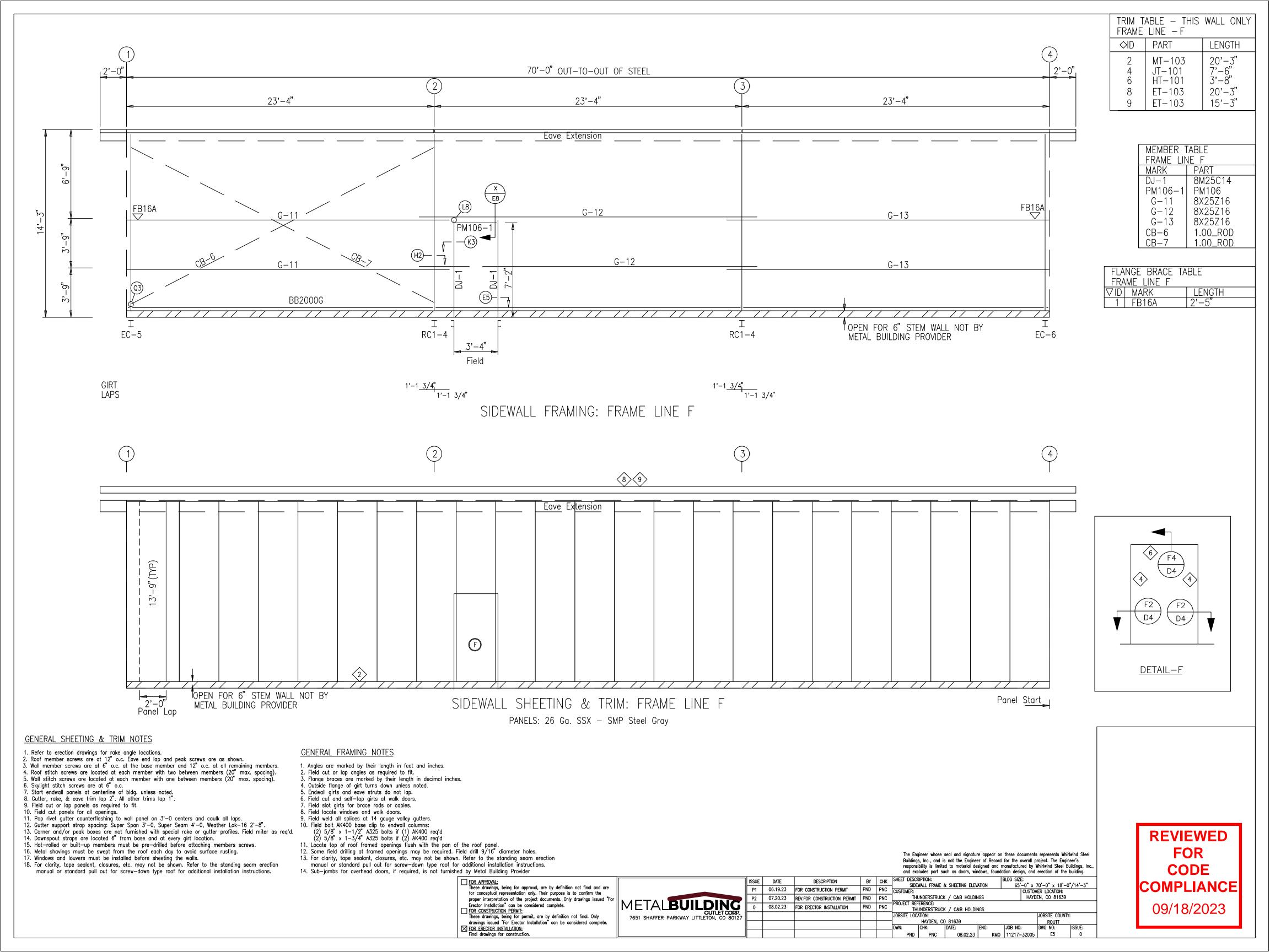
PND PNC 08.02.23 KMO 11217-32005

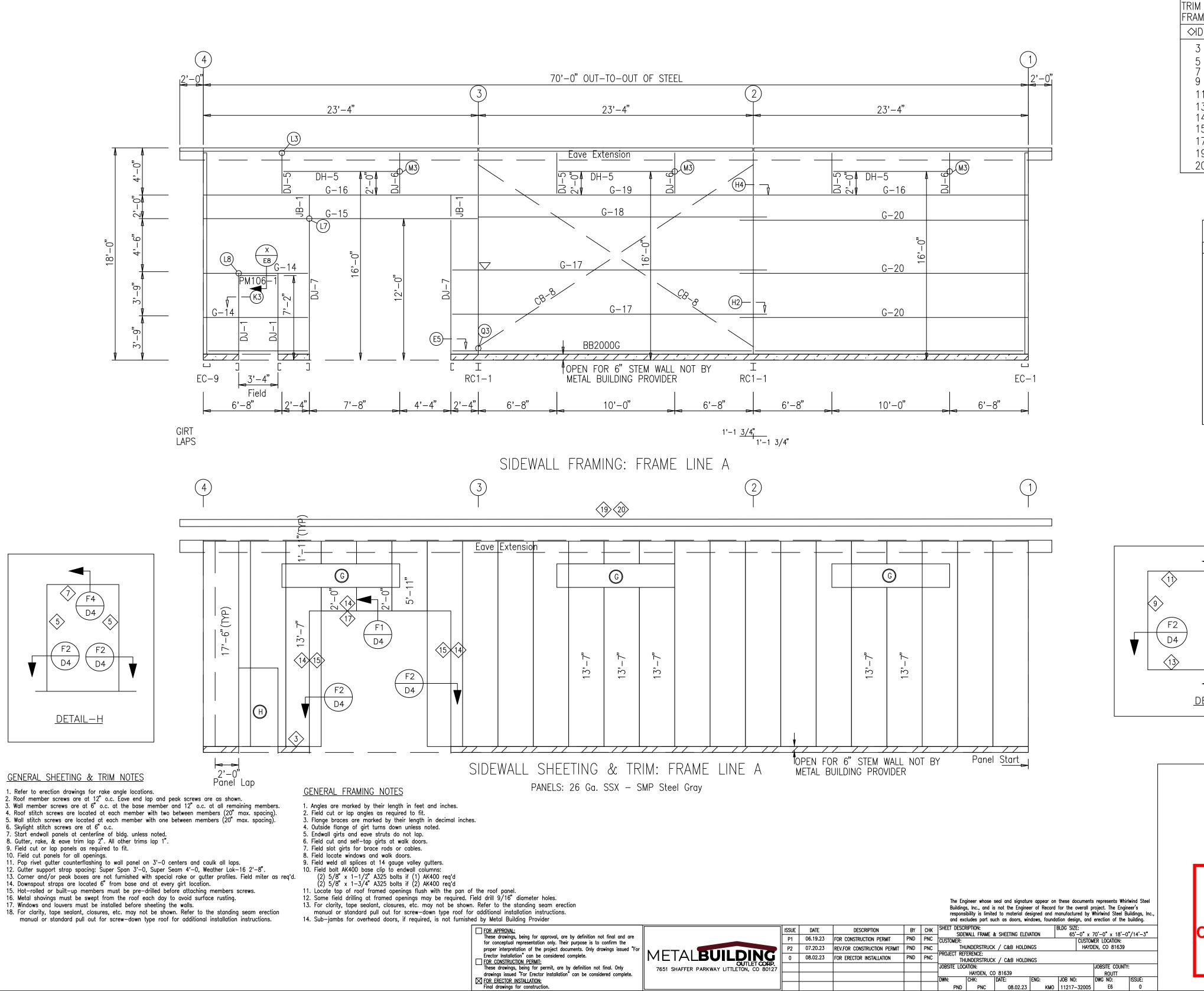
HAYDEN, CO 81639

09/18/2023

FOR CODE COMPLIANCE

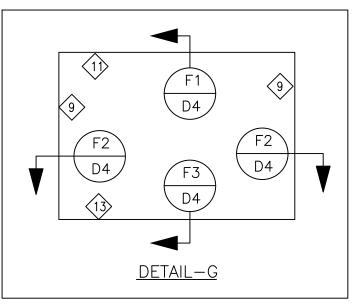
REVIEWED





TRIM TABLE - THIS WALL ONLY FRAME LINE -A PART LENGTH \Diamond ID 20'-3" MT - 103JT-101 HT-101 JT-101 10'-4" HT-101 13 MT-114 14 MT-116B 15 JT-101 10'-4" 12'-4" 17 HT-101 12'-4" 19 ET-103 20 ET-103 20'-3" 15'-3"

MEMBER T	ABLE
FRAME LIN	NE A
MARK	PART
DJ-1	8M25C14
DJ-5	8M25C14
DJ-6	8M25C14
DJ-7	8M35C14
JB-1	8M35C14
PM106-1	PM106
DH-5	8M25C14
G-14	8X25Z16
G-15	8X25C12
G-16	8X25C14
G-17	8X25Z16
G-18	8X25Z16
G-19	8X25C14
G-20	8X25Z16
CB-8	1.00_ROD



REVIEWED
FOR
CODE
COMPLIANCE

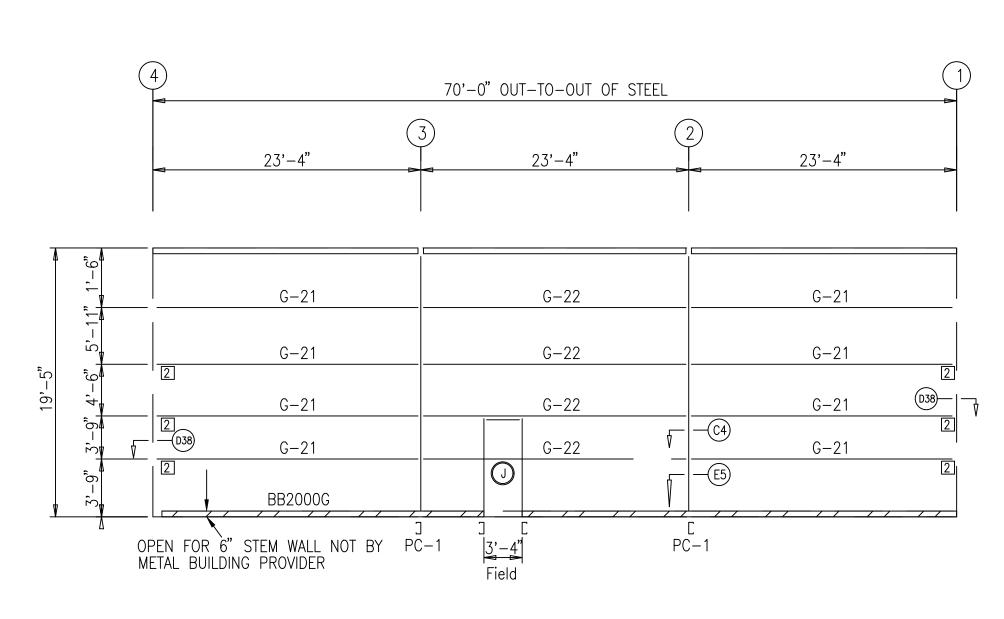
09/18/2023

BOLT TABLE PARTITION 1				
LOCATION	QUAN	TYPE	DIA	LENGTH
PC-1/RAFTER	2	A325	5/8"	1 1/2"

MEMBER 1	ABLE
PARTITION	1
MARK	PART
PC-1	8M35C12
DJ-1	8M25C14
PM106-1	PM106
G-21	8X25Z16
G-22	8X25Z16

TRIM PARTIT		IS WALL ONLY
♦ID	PART	LENGTH
2	JT-101	7'-6"
4	HT-101	3'-8 "
5	MT-103	20'-3"
6	SF-10	20'-3".
7	MT-106C	15'-3".
8	MT-106C	20'-3"

CONN	IECTION PLATES
PART	ITION 1
	MARK/PART
2	AK244



GIRT@7'-6" (E8)

PM106-1

3'-4" Field DETAIL-J

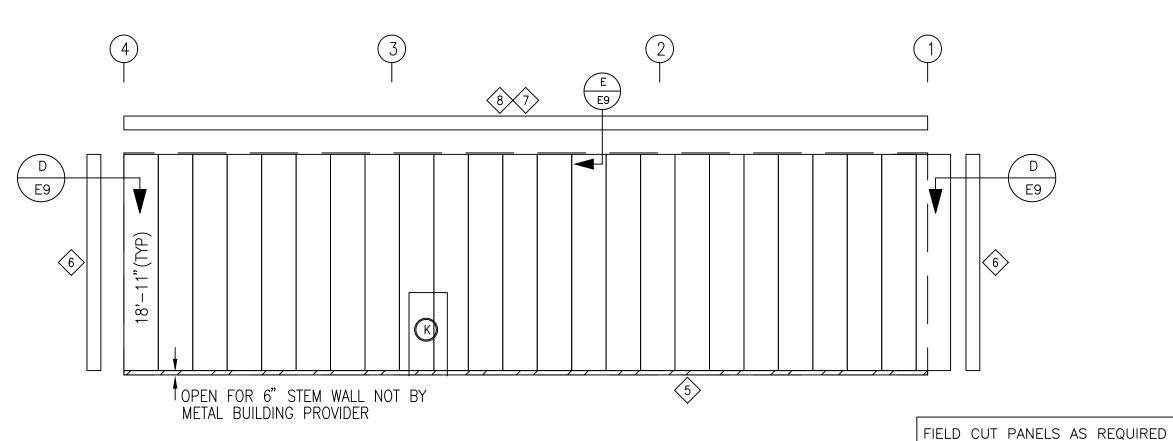
GIRT@3'-9"

GIRT

F.F.L

<u>DETAIL-K</u>

PARTITION 1 FRAMING



PARTITION 1 FRONT SHEETING & TRIMS PANELS: 26 Ga. SSX - SMP Steel Gray

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	and exc	cludes part su	ıch as doors, wir	idows, found	ation desi	gn, and	erection of t	he building.
CHK	SHEET DESCR		E:	70' 0" 10	, 0, 1, 1, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2, 2,			
PNC	CUSTOMER:	ARIIION FRAN	IE & SHEETING E	LEVATION	65'-0" x 70'-0" x 18'-0"/14'-3" CUSTOMER LOCATION:			
PNC			C / C&B HOLDIN		HAYDEN, CO 81639			
PNC	PROJECT REFERENCE: THUNDERSTRUCK / C&B HOLDINGS							
	JOBSITE LOCATION:						JOBSITE COU	INTY:
	HAYDEN, CO 81639 ROUTT							
	DWN:	CHK:	DATE:	ENG:	JOB NO:	:	DWG NO:	ISSUE:
	PND	PNC	08.02.23	кмо	11217-	-32005	E7	0

| FOR APPROVAL:

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| FOR ERECTOR INSTALLATION:
| Final drawings for construction.

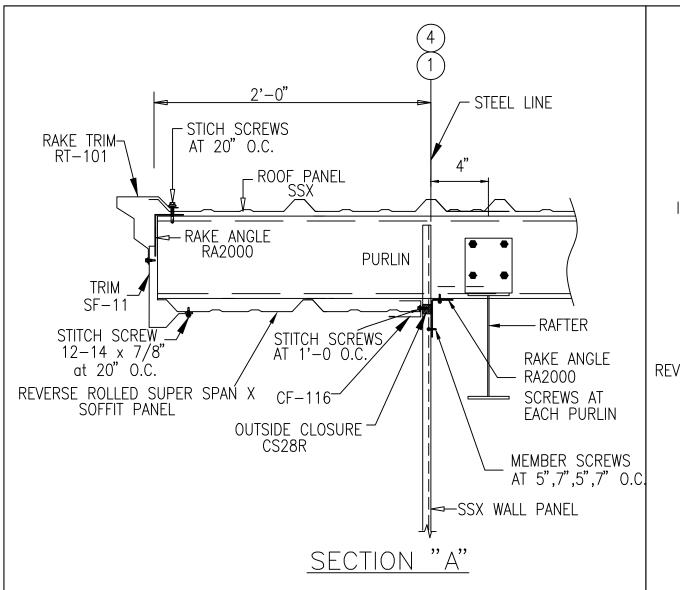
METALBUILDING OUTLET CORP. 7651 SHAFFER PARKWAY LITTLETON, CO 80127

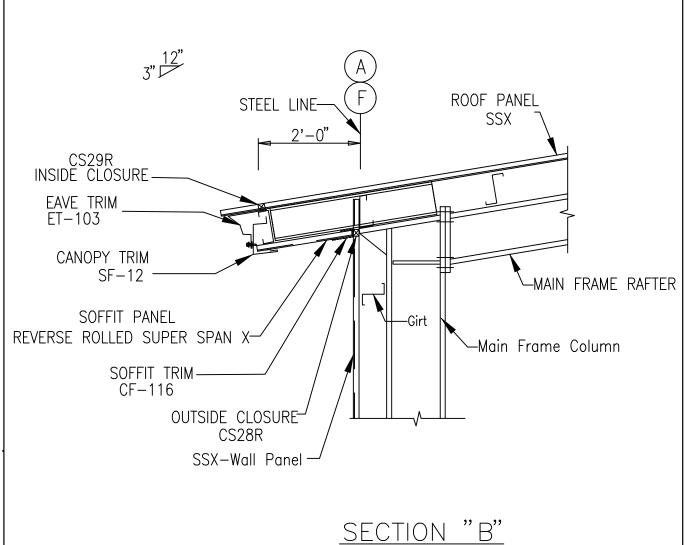
CODE COMPLIANCE 09/18/2023

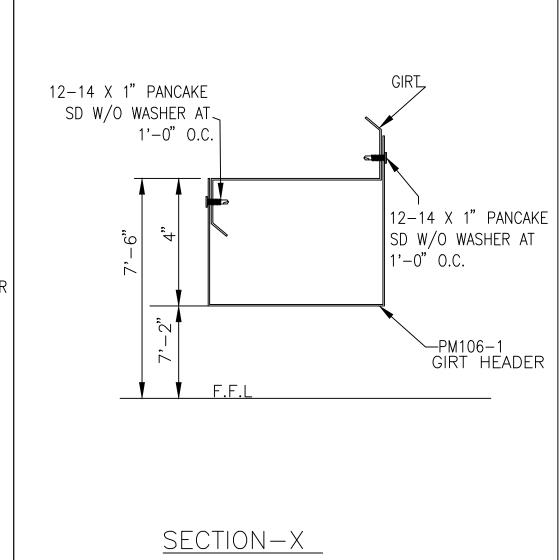
REVIEWED

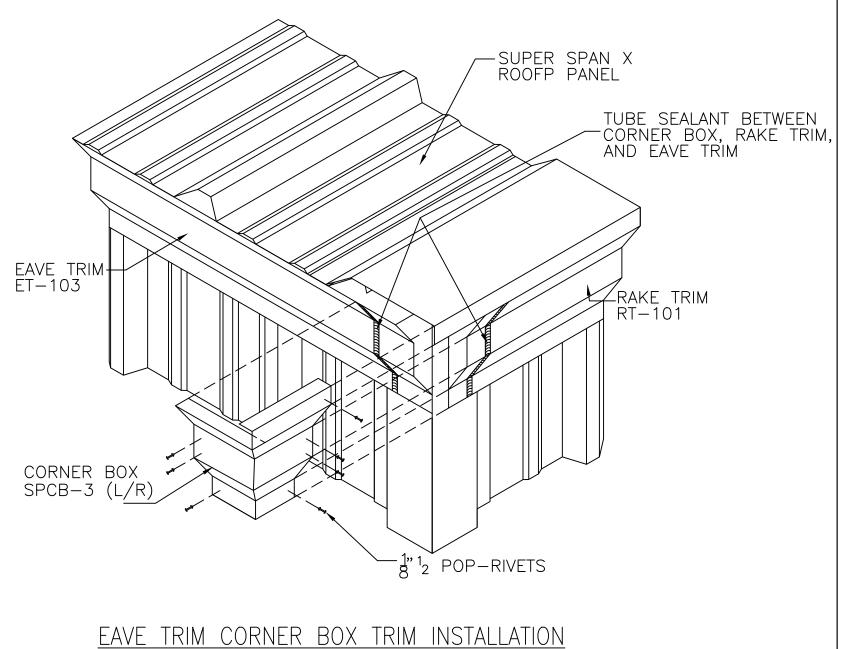
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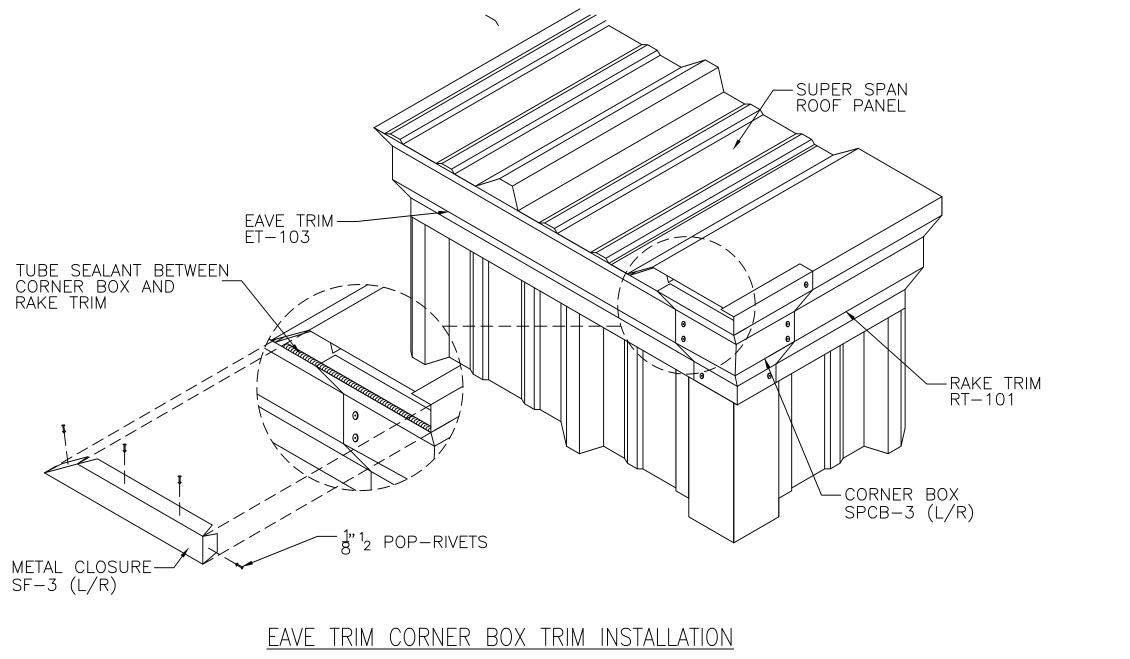
ISSUE DATE DESCRIPTION
P1 06.19.23 FOR CONSTRUCTION PERMIT PND P2 07.20.23 REV.FOR CONSTRUCTION PERMIT PND 0 08.02.23 FOR ERECTOR INSTALLATION











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FOR ERECTOR INSTALLATION:
Final drawings for construction.

METALBULDING
OUTLET CORP.
7651 SHAFFER PARKWAY LITTLETON, CO 80127

and excludes part such as doors, windows, foundation design, and erection of the building.

SHEET DESCRIPTION:

BUILDING SECTIONS

CUSTOMER:

THUNDERSTRUCK / C&B HOLDINGS

THUNDERSTRUCK / C&B HOLDINGS

PROJECT REFERENCE:

THUNDERSTRUCK / C&B HOLDINGS

JOBSITE LOCATION:

HAYDEN, CO 81639

DWN:

CHK:

DATE:

ENG:

JOB NO:

DWG NO:

ISSUE:

PND

PND

PNC

O8.02.23

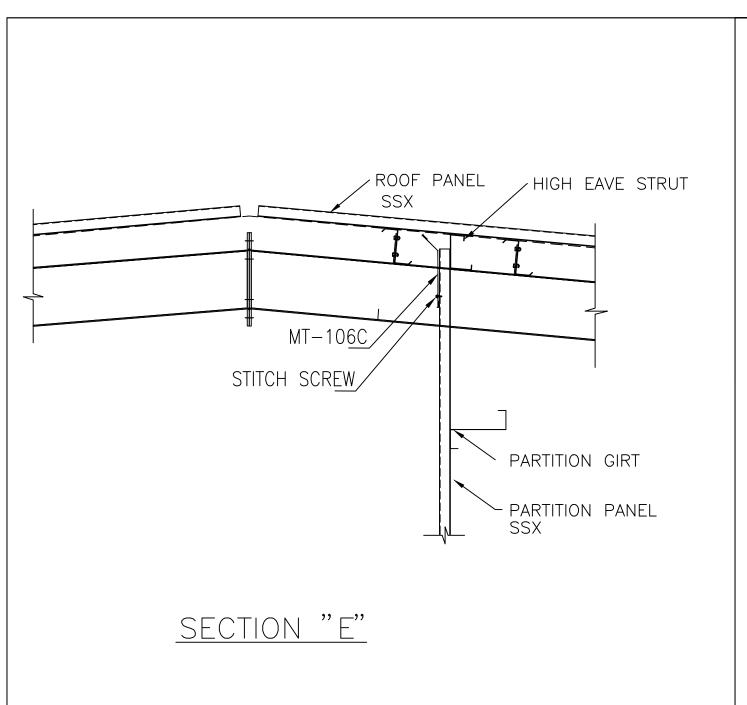
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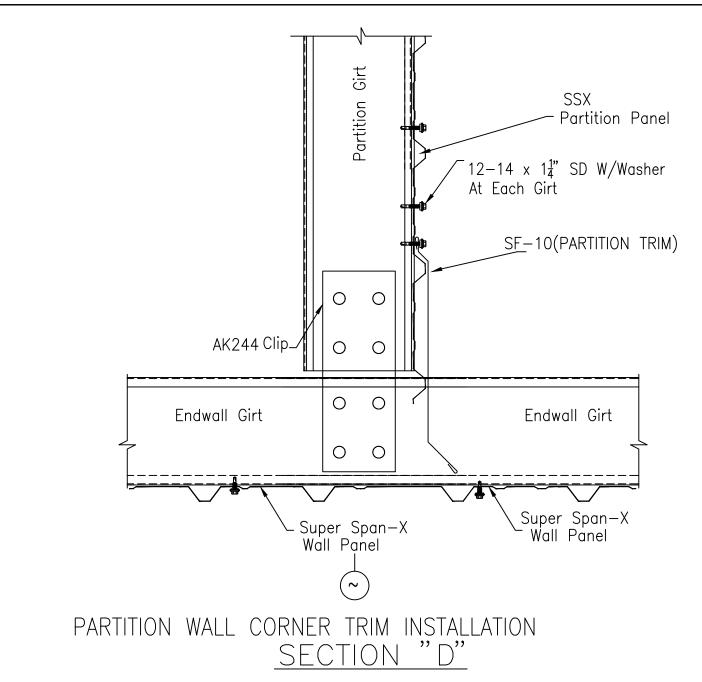
11217—32005

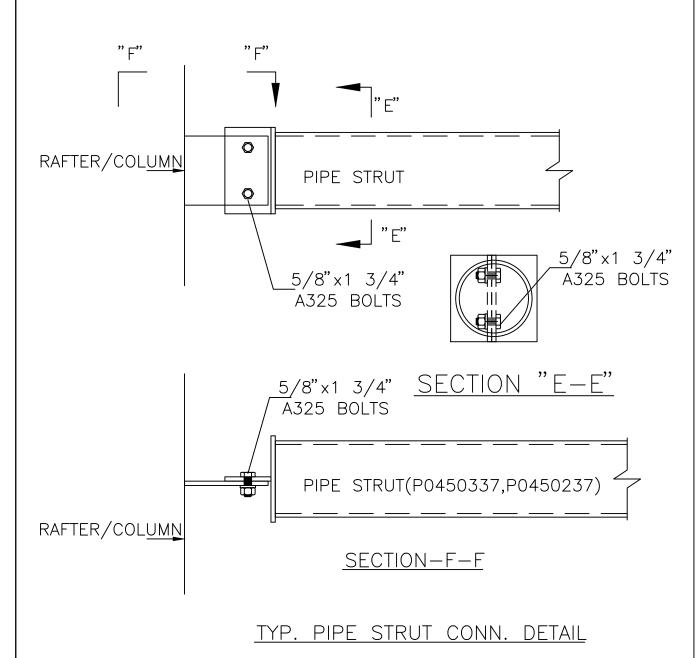
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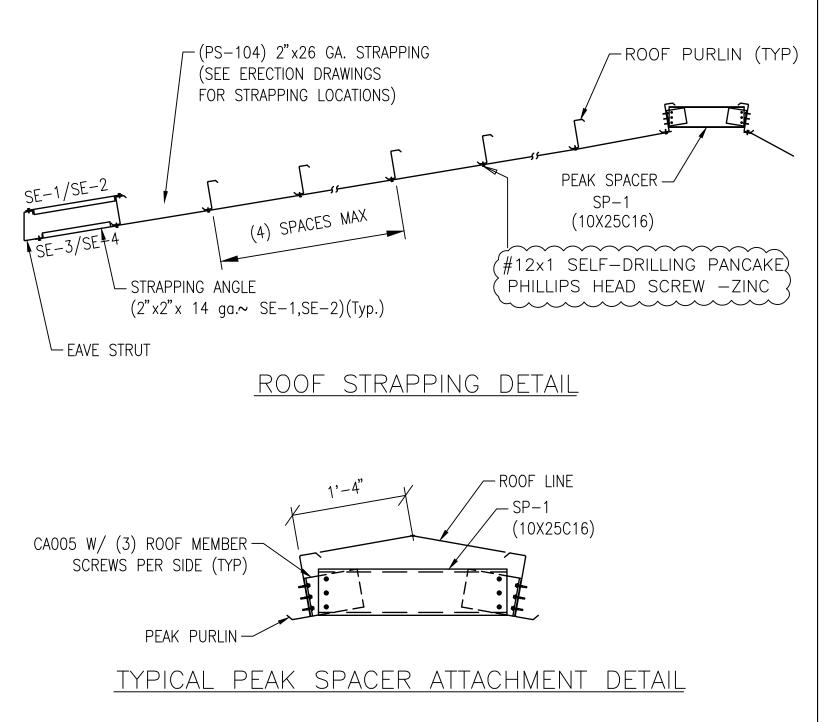
REVIEWED FOR CODE COMPLIANCE 09/18/2023

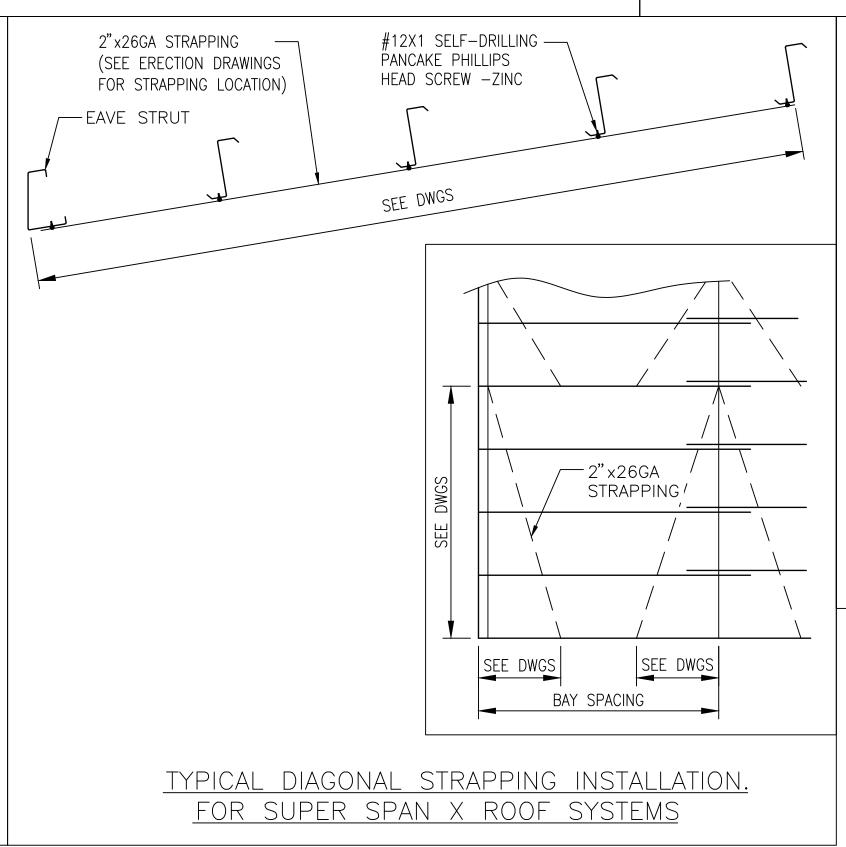


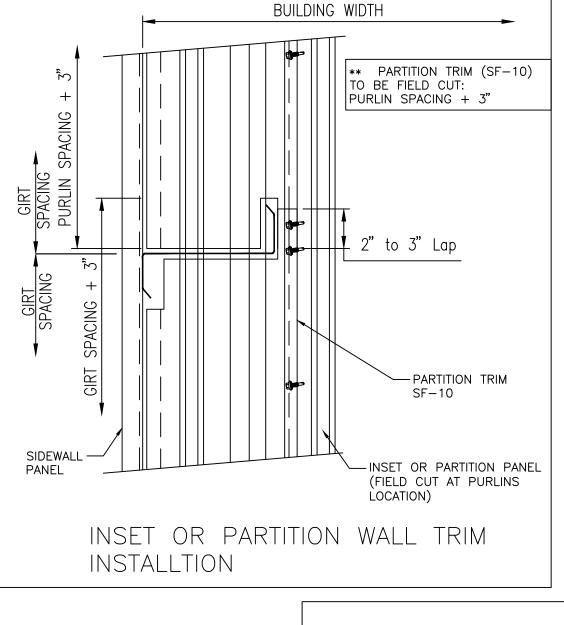




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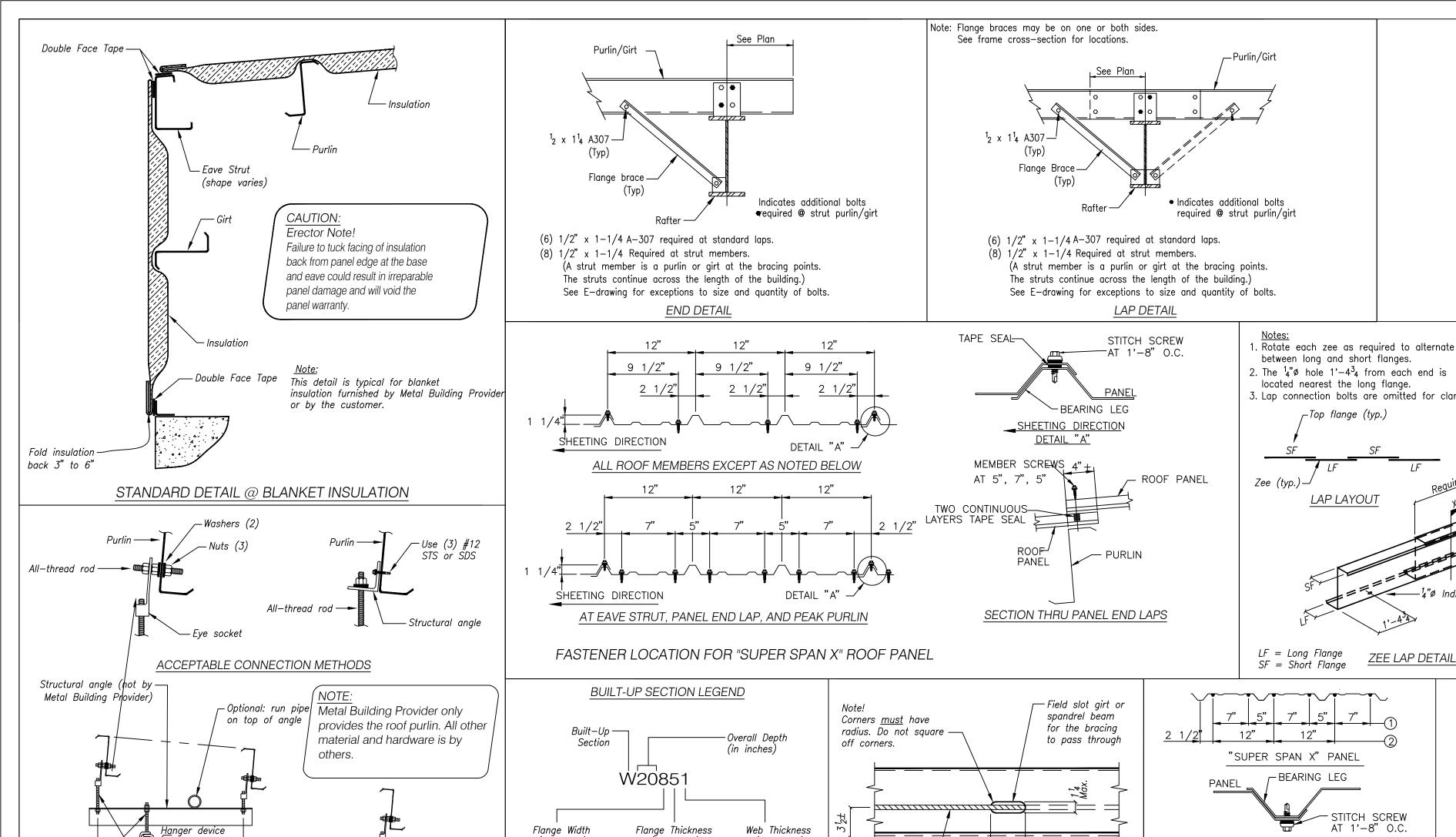
FOR ERECTOR INSTALLATION:
Final drawings for construction

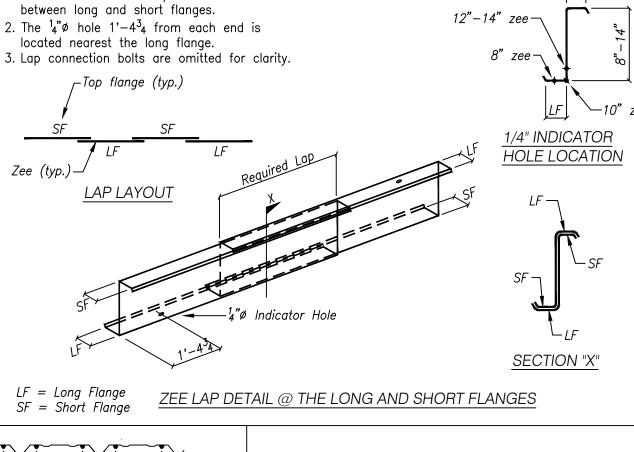
METALBUILDING
OUTLET CORP.
7651 SHAFFER PARKWAY LITTLETON, CO 80127

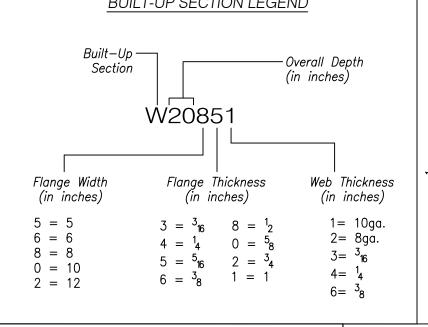
ISSUE DATE DESCRIPTION BY CHK P1 06.19.23 FOR CONSTRUCTION PERMIT P2 07.20.23 REV.FOR CONSTRUCTION PERMIT PND PNC PND PNC 08.02.23 FOR ERECTOR INSTALLATION

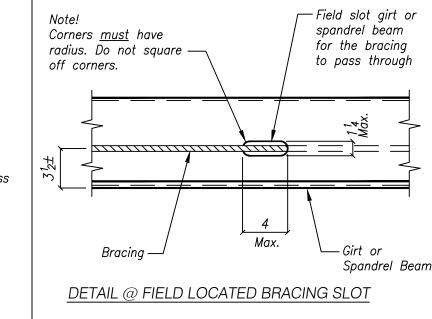
REVIEWED FOR CODE COMPLIANCE 09/18/2023

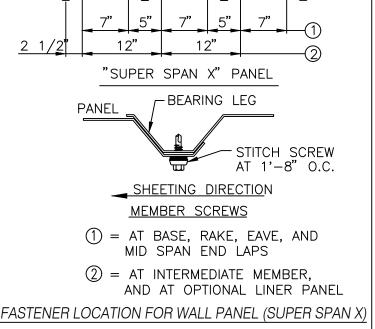
Buildings, Inc., and is not the Engineer of Record for the overall project. The Engineer's responsibility is limited to material designed and manufactured by Whirlwind Steel Buildings, Inc. and excludes part such as doors, windows, foundation design, and erection of the building. BUILDING SECTIONS 65'-0" x 70'-0" x 18'-0"/14'-3" PND PNC CUSTOMER: CUSTOMER LOCATION: HAYDEN, CO 81639 THUNDERSTRUCK / C&B HOLDINGS PROJECT REFERENCE: THUNDERSTRUCK / C&B HOLDINGS JOBSITE LOCATION: JOBSITE COUNTY HAYDEN, CO 81639 ROUTT DWG NO: JOB NO: : CHK: DATE: ENG: JOB NO: DWG NO: PND PNC 08.02.23 KMO 11217-32005 E9

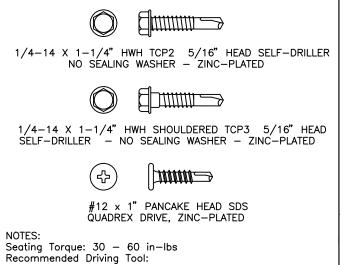








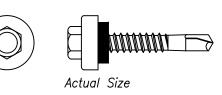




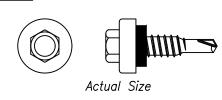
1800 RPM screw gun with depth sensing nosepiece to prevent overdriving and stripout

STANDARD FASTENERS MISCELLANEOUS

Description: 12-14 x 1¹/₄ Hex Head Undercut (#12 x 1¹/₄ Long-#3 Long Pilot Point Self-Drilling Life S.D.S.) Long-Life Zinc Die Cast Head Seating Torque: 30 to 60 in-lbs Recommended Driving Tool: 1800 RPM electric screw gun with depth sensing nosepiece to prevent overdriving and stripout Suggested Pre-Drill: None



Description: 4-14 x 78 Hex Head Undercut (#14 x 78 Long-Life #1 Point Self-Drilling Lap Lap-Tek S.D.S.) Long-Life Zinc Die Cast Head Seating Torque: 30 to 60 in-lbs Recommended Driving Tool: 1800 RPM electric screw gun with depth sensing xnosepiece to prevent overdriving and stripout Suggested Pre-Drill: None



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Erector Installation" can be considered complete. FOR CONSTRUCTION PERMIT:
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Final drawings for construction

METALBUILDING 7651 SHAFFER PARKWAY LITTLETON, CO 8012

ISSUE DATE DESCRIPTION P1 06.19.23 FOR CONSTRUCTION PERMIT P2 07.20.23 REV.FOR CONSTRUCTION PERMIT PND PNC PND PNC 08.02.23 FOR ERECTOR INSTALLATION

SHEET DESCRIPTION: STANDARD DETAIL PAGE 65'-0" x 70'-0" x 18'-0"/14'-3" THUNDERSTRUCK / C&B HOLDINGS PROJECT REFERENCE: THUNDERSTRUCK / C&B HOLDINGS JOBSITE LOCATION: HAYDEN, CO 81639 ROUTT DWG NO: JOB NO: PND PNC 08.02.23 KMO 11217-32005 D1

REVIEWED FOR CODE COMPLIANCE 09/18/2023

FOR APPROVAL:

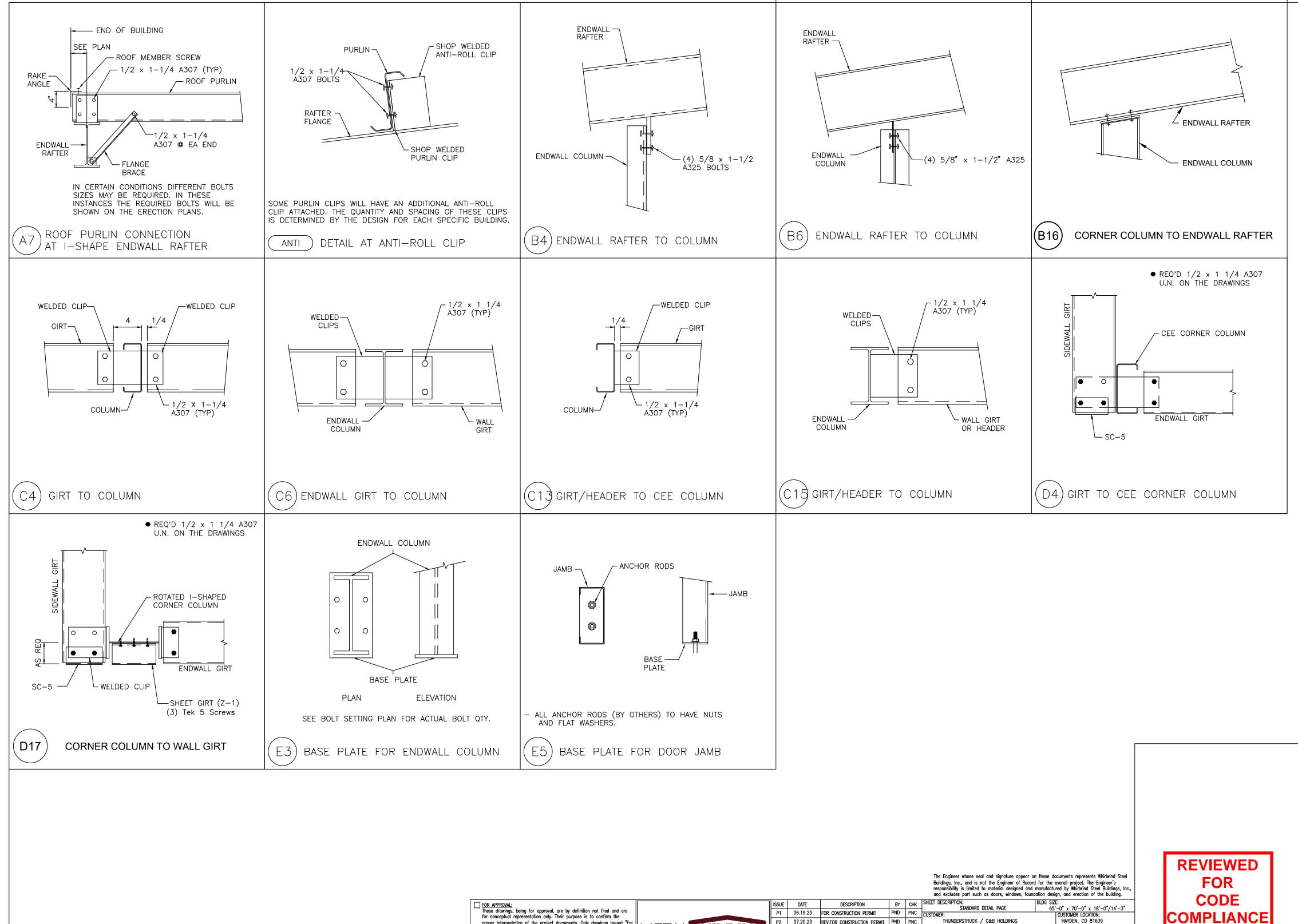
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PND PNC CUSTOMER:

(shape may vary All-thread rod-All-thread rod - Hanger device (shape may vary) 1/3 2/3 maximum off center TRAPEZE HANGER ~ 4" MAX. PIPE HANGER ~ 2-1/2" MAX. PIPE Purlin

All—thread**/** rod - Caddy Caddy clip attached to lip is Connection through the Flange C-Clamp is not an acceptable connection not an acceptable connection flange is not acceptable

> ACCEPTABLE CONNECTIONS FOR ALL COLLATERAL LOADS FOR HANGER ATTACHMENT



FOR APPROVAL:

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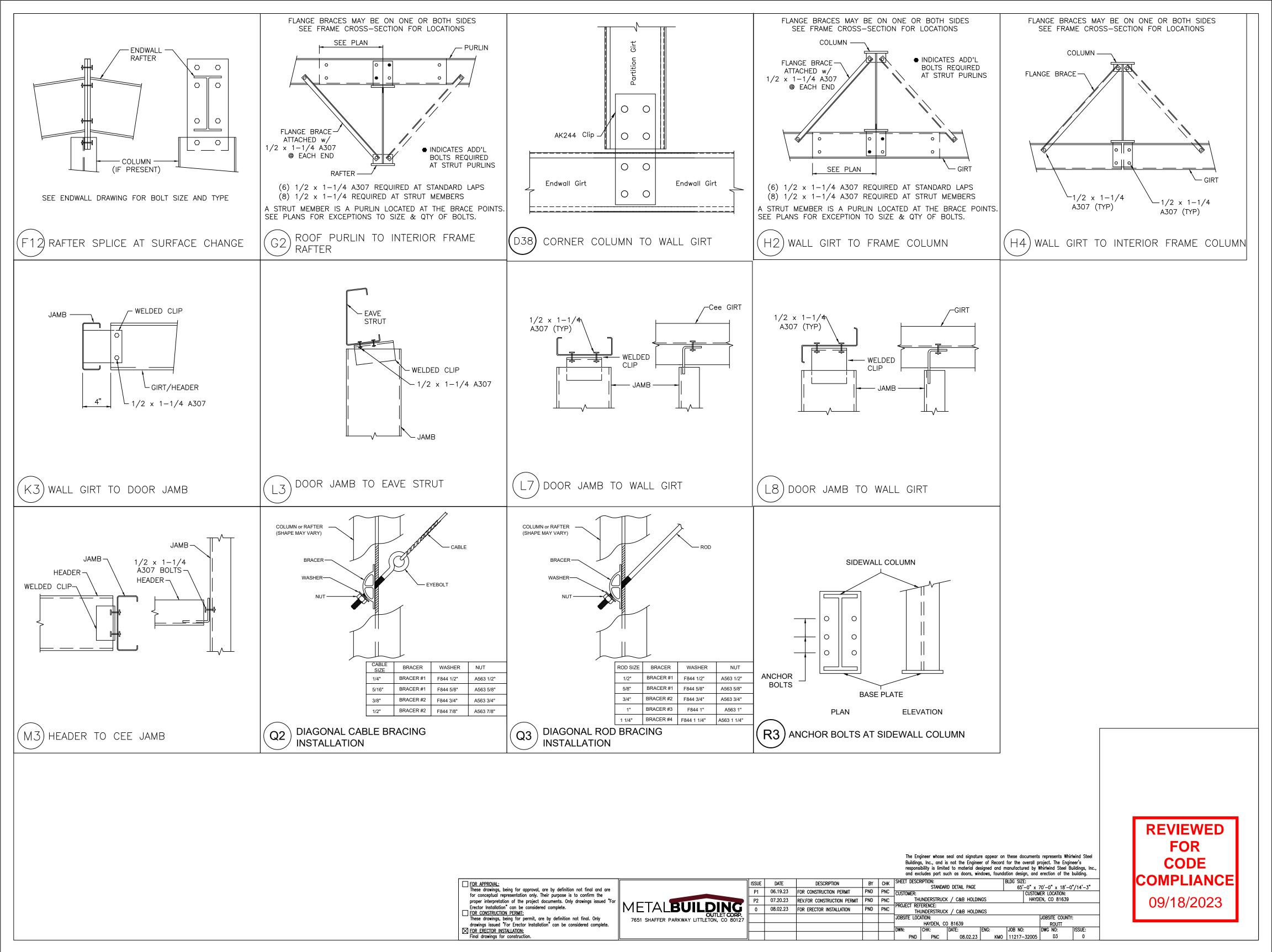
FOR ERECTOR INSTALLATION:
Final drawings for construction. JOBSITE LOCATION:

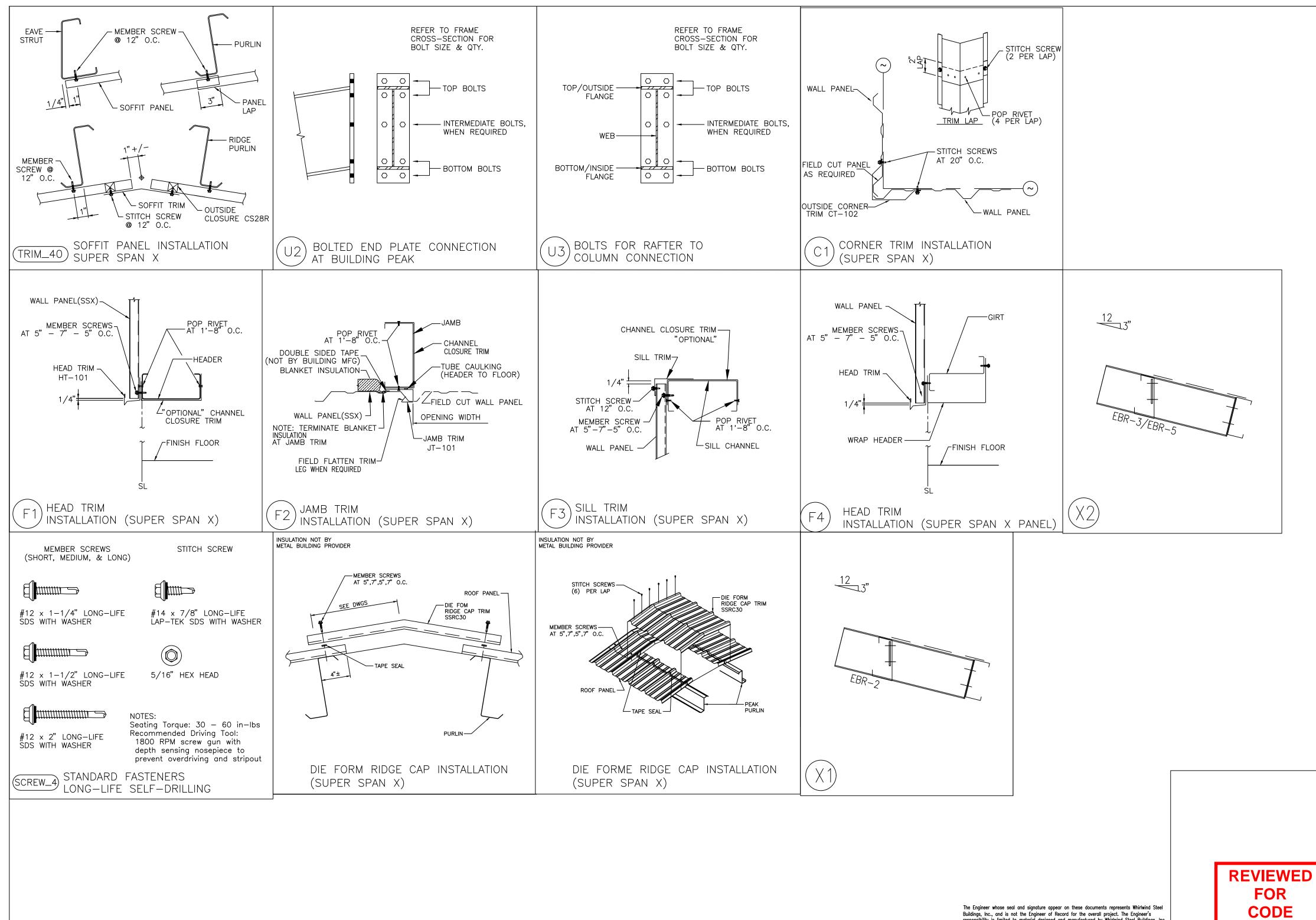
HAYDEN, CO 81639

COMPLIANCE 09/18/2023

JOBSITE COUNTY: ROUTT DWG NO:

| DWN: | CHK: | DATE: | ENG: | JOB NO: | DWG NO: | PND | PNC | 08.02.23 | KMO | 11217-32005 | D2





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65'-0" x 70'-0" x 18'-0"/14'-3" CUSTOMER LOCATION: HAYDEN, CO 81639

> JOBSITE COUNTY: ROUTT DWG NO:

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FOR ERECTOR INSTALLATION:
Final drawings for construction.



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<u>ק</u>	ISSUE	DATE	DESCRIPTION	BY	СНК	SHEET DESCRIPTION: STANDARD DETAIL PAGE BLDG SIZE: 65'-0"					70'–0" x 18	
	P1	06.19.23	FOR CONSTRUCTION PERMIT	PND	PNC	CUSTOMER:	00 0					
	P2	07.20.23	REV.FOR CONSTRUCTION PERMIT	PND	PNC		THUNDERSTRUCK / C&B HOLDINGS HAYDE					
	0	08.02.23	FOR ERECTOR INSTALLATION	PND	PNC	PROJECT REFERENCE: THUNDERSTRUCK / C&B HOLDINGS						
RP. 0127						JOBSITE LOCA	JOBSITE COL					
							ROUTT					
						DWN:	CHK:	DATE:	ENG:	JOB NO:	DWG NO:	
						PND	PNC	08.02.23	кмо	11217-32005	D4	

COMPLIANCE 09/18/2023

