

SAC Wireless  
300 Airport Road, Building 1  
Elgin, IL 60123  
(815) 705-4782

REVIEWED  
FOR  
CODE  
COMPLIANCE  
08/07/2024

Kimley » Horn

Kevin Fraleigh, P.E.  
3875 Embassy Pkwy #280  
Akron, OH 44333  
(216) 505-8256

Date: July 20, 2022  
K-H Project #: KHCLE-26656

### Comprehensive Structural Analysis Report

**Carrier Designation:**

Client Project ID: PR-91471  
Site Name: Oak Creek Coal

**Analysis Criteria:**

Code Requirements: TIA-222-H, 2021 IBC, & ASCE 7-16  
Ultimate Wind Speed: 112 mph w/ 0" Ice  
Wind Speed: 50 mph w/ 0.25" Ice

**Site Data:**

29920 County Road 27, Hayden  
CO, 81639, Routt County  
Latitude 40.354108°, Longitude -107.072581°  
80 Foot – Valmont Self-Support

Mr. James Willard,

*Kimley-Horn and Associates, Inc.* is pleased to submit this “Comprehensive Structural Analysis Report” to determine the structural integrity of the above mentioned tower.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

**Existing+Phase 1:**

Proposed Tower Rating:	86.5%	Pass
Proposed Foundation Rating:	57.0%	Pass

**Existing+Phase 1+Phase 2:**

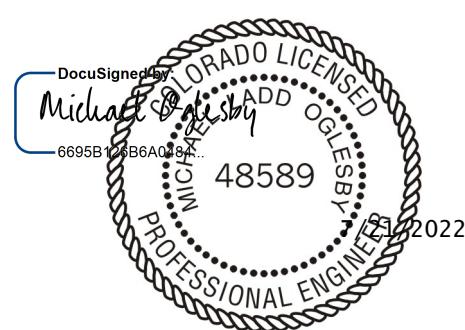
Proposed Tower Rating:	82.1%	Pass
Proposed Foundation Rating:	52.7%	Pass

This analysis has been performed in accordance with the 2021 IBC based upon an ultimate 3-second gust wind speed of 112 mph. Applicable Standard references and design criteria are listed in Page 2 - Analysis Criteria.

Structural analysis prepared by: Elliot Ziebart, E.I.

Respectfully submitted by:

Michael Oglesby, P.E.  
Lic. #PE.0048589, Exp. 10/31/2023  
Kimley-Horn and Associates, Inc.



## ▪ INTRODUCTION

At the request of SAC Wireless, Kimley-Horn and Associates, Inc. performed a structural analysis of the existing tower type structure located in Hayden, CO. The purpose of the analysis is to determine the adequacy of the tower to support the loading configuration outlined in Appendix A (Tower Analysis Summary Form), pursuant to the referenced standards.

## ▪ ANALYSIS CRITERIA

The analysis utilizes tnxTower v. 8.1, an industry-standard finite element analysis program used to create an elastic three-dimensional model considering second-order effects per ANSI/TIA-222 requirements. The program calculates member stresses for various loading cases and selected output from the analysis is included in the appendices.

**The topographic factors and properties listed below were solely determined per directive of Union Wireless for the purpose of this analysis. A more rigorous procedure for determining topographic effects could be considered.**

**The proposed mounts considered in this analysis were chosen per directive by Union Wireless. The tiebacks must be attached to the adjacent tower legs in order for the results of this analysis to be valid.**

**The maximum vertical offset of the proposed equipment is 2'. If the vertical offset of the proposed loading exceeds 2', the results of this analysis are invalid.**

TIA-222 Revision:	TIA-222-H
Risk Category:	III
Ultimate Wind Speed:	112 mph
Exposure Category:	C
Topographic Category:	3
Crest Height:	700 ft
Ice Thickness:	0.25 in
Wind Speed with Ice:	50 mph
Seismic Structure Class:	C
Seismic S <sub>s</sub> :	0.550
Seismic S <sub>1</sub> :	0.099

## SUPPORTING DOCUMENTATION

Information on the current tower geometry, member sizes, foundation dimensions, soil properties, and antenna loading was obtained from the sources listed below. It is assumed that all information provided to Kimley-Horn & Associates, Inc. is accurate. In the absence of information to the contrary, we assume the structure has been properly erected and maintained per the original design drawings and the capacity has not significantly changed from the "as new" condition.

Tower Design	Valmont Drawing #: D-118598, dated 3/23/2004
Foundation Design	Valmont Microflect Drawing #: D-119403, dated 8/5/2004
Geotechnical Report	Not Provided
Previous Analysis	Valmont Analysis Order #: 441507-2, dated 12/30/2020
Tower Loading Data	Union Wireless RFDS, dated 12/28/2021 Union Wireless Loading Sheet, dated 05/23/2022

## ▪ RESULTS

The tables below show a maximum usage summary for each group of components in the structure. The usage of a component is the ratio of force in the member compared to its calculated capacity. A more detailed report of member usages can be found in the appendix at the end of this report. Usages greater than 100% indicate where the force in the member exceeds its capacity. Usages up to 105% are considered acceptable per industry standard practice.

### Phase 1 Structure Usages:

Structure Component	Controlling Usage	Result
Legs	77.5%	Pass
Diagonals	86.5%	Pass
Horizontals/Girts	54.6%	Pass
Redundant/Inner Bracing Members	6.2%	Pass
Bolts	86.5%	Pass
Anchor Rods	38.7%	Pass

### Foundation Usages:

Foundation	Controlling Usage	Result
*Base Foundation	57.0%	Pass

### Phase 2 Structure Usages:

Structure Component	Controlling Usage	Result
Legs	70.7%	Pass
Diagonals	82.1%	Pass
Horizontals/Girts	50.5%	Pass
Redundant/Inner Bracing Members	5.2%	Pass
Bolts	82.1%	Pass
Anchor Rods	35.8%	Pass

### Foundation Usages:

Foundation	Controlling Usage	Result
*Base Foundation	52.7%	Pass

\*Soil information was assumed per TIA-222-H Annex F.

## ▪ CONCLUSIONS AND RECOMMENDATIONS

Per our structural analysis, the structure has been found to pass. The tower and foundation can support the referenced loading in accordance with the structural strength requirements of ANSI/TIA-222-H and 2021 International Building Code.

## ▪ ASSUMPTIONS AND LIMITATIONS

This report is not a condition assessment of the tower and foundation; It is an engineering analysis based upon the theoretical capacity of the structure. Unless told otherwise, we assume the tower and foundation to be in "like new" condition. It is the responsibility of our client and the tower owner to verify that the tower modeled and loading considered is accurate. If these assumptions are not accurate, Kimley-Horn & Associates, Inc. should be notified immediately to perform a revised analysis. This analysis assumes all antenna mounts are adequate to support the existing and proposed loads. It is the carrier's responsibility to ensure antenna mount meets the structural requirements of ANSI/TIA-222. Kimley-Horn & Associates, Inc. did not analyze antenna supporting mounts as part of this structural analysis report.

All services are performed, results obtained, and recommendation made in accordance with generally accepted engineering principles and practices. Kimley-Horn & Associates, Inc. is not responsible for the conclusions, opinions and recommendations made by others based on the information in this report.

Kimley-Horn makes no warranties, expressed or implied in connection with this report and disclaims any liability arising from original design, material, fabrication, and section deficiencies or corrosion of the tower.

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## APPENDIX A

### Tower Analysis Summary Form

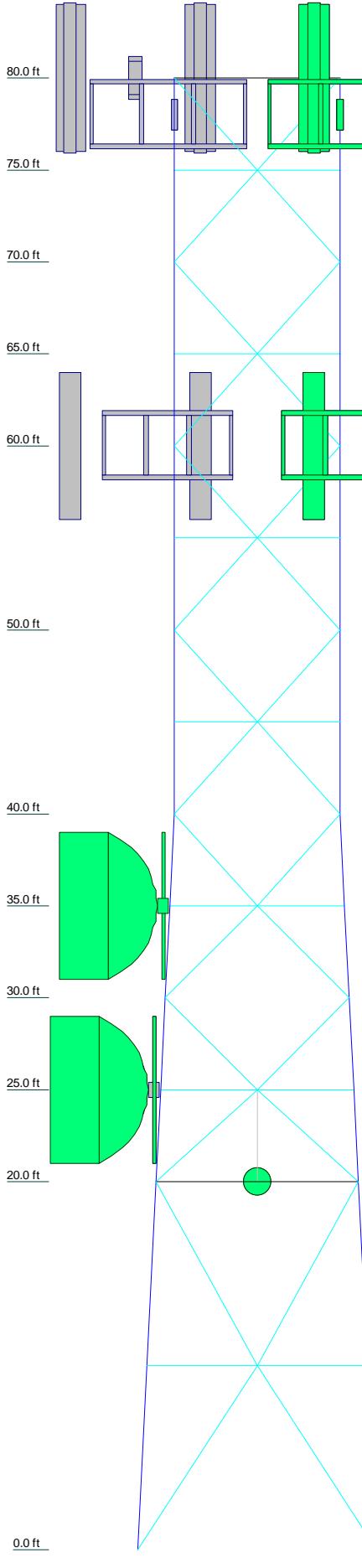


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## APPENDIX B

### tnxTower Output File – Phase 1

### DESIGNED APPURTEANCE LOADING



TYPE	ELEVATION	TYPE	ELEVATION
(2) CWX063X25XM00 w/ MP	78	Site Pro 1 VFA12-WLL	78
(2) CWX063X25XM00 w/ MP	78	Site Pro 1 VFA12-WLL	78
(2) CWX063X25XM00 w/ MP	78	Site Pro 1 VFA12-WLL	78
(2) 12082x w/ MP (Future)	78	(2) NNH4-65C-R6-V3 w/ Mount Pipe	60
(2) 12082x w/ MP (Future)	78	(2) NNH4-65C-R6-V3 w/ Mount Pipe	60
(2) 12082x w/ MP (Future)	78	(2) NNH4-65C-R6-V3 w/ Mount Pipe	60
(3) AHLOA (Future)	78	Nokia 3JR80236AAAA	60
(3) AHLOA (Future)	78	Nokia 3JR80236AAAA	60
(3) AHLOA (Future)	78	Nokia 3JR80236AAAA	60
(2) CMA-UBTULBULBH/6517/17/21/21 w/ MP	78	Nokia 3JR80235AAAA	60
(2) CMA-UBTULBULBH/6517/17/21/21 w/ MP	78	Nokia 3JR80235AAAA	60
AHFIG	78	Rosenberger D218RRUDSM Clamp	60
AHFIG	78	Rosenberger D218RRUDSM Clamp	60
AHFIG	78	DC9-48-60-24-8C-EV	60
AHLOA	78	(2) 8' Pipe Mount (2SCH40)	60
AHLOA	78	(2) 8' Pipe Mount (2SCH40)	60
AHLOA	78	Site Pro 1 VFA10-HD	60
AHCA	78	Site Pro 1 VFA10-HD	60
AHCA	78	8' Pipe Mount (2SCH40)	35
PR-UWPT612	78	(2) WTM4100	35
PR-UWPT612	78	HPX8-65 (Future)	35
PR-UWPT612	78	8' Pipe Mount (2SCH40)	25
FB-L98B-A1041	78	(2) WTM4100	25
FB-L98B-A1041	78	HPX8-65	25
FB-L98B-A1041	78	USX6	25
FB-L98B-A1041	78	B5 - 18" Diameter (Reserved)	20
FB-L98B-A1041	78	B5 - 18" Diameter (Reserved)	20

### SYMBOL LIST

MARK	SIZE	MARK	SIZE
A	2L1 3/4x1 3/4x1/8	B	2L1 3/4x1 3/4x1/8x3/8

### MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A500-46	46 ksi	62 ksi			

### TOWER DESIGN NOTES

1. Tower is located in Routt County, Colorado.
2. Tower designed for Exposure C to the TIA-222-H Standard.
3. Tower designed for a 112 mph basic wind in accordance with the TIA-222-H Standard.
4. Tower is also designed for a 50 mph basic wind with 0.25 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Risk Category III.
7. Topographic Category 3 with Crest Height of 700.00 ft
8. TOWER RATING: 86.5%

**ALL REACTIONS  
ARE FACTORED**

**MAX. CORNER REACTIONS AT BASE:**  
DOWN: 126 K  
SHEAR: 26 K

**UPLIFT: -114 K  
SHEAR: 23 K**

**AXIAL**  
37 K  
SHEAR 9 K      MOMENT 502 kip-ft

**TORQUE 4 kip-ft  
50 mph WIND - 0.2500 in ICE**

**AXIAL**  
28 K  
SHEAR 40 K      MOMENT 2188 kip-ft

**TORQUE 14 kip-ft  
REACTIONS - 112 mph WIND**

# Feed Line Distribution Chart

**0' - 80'**

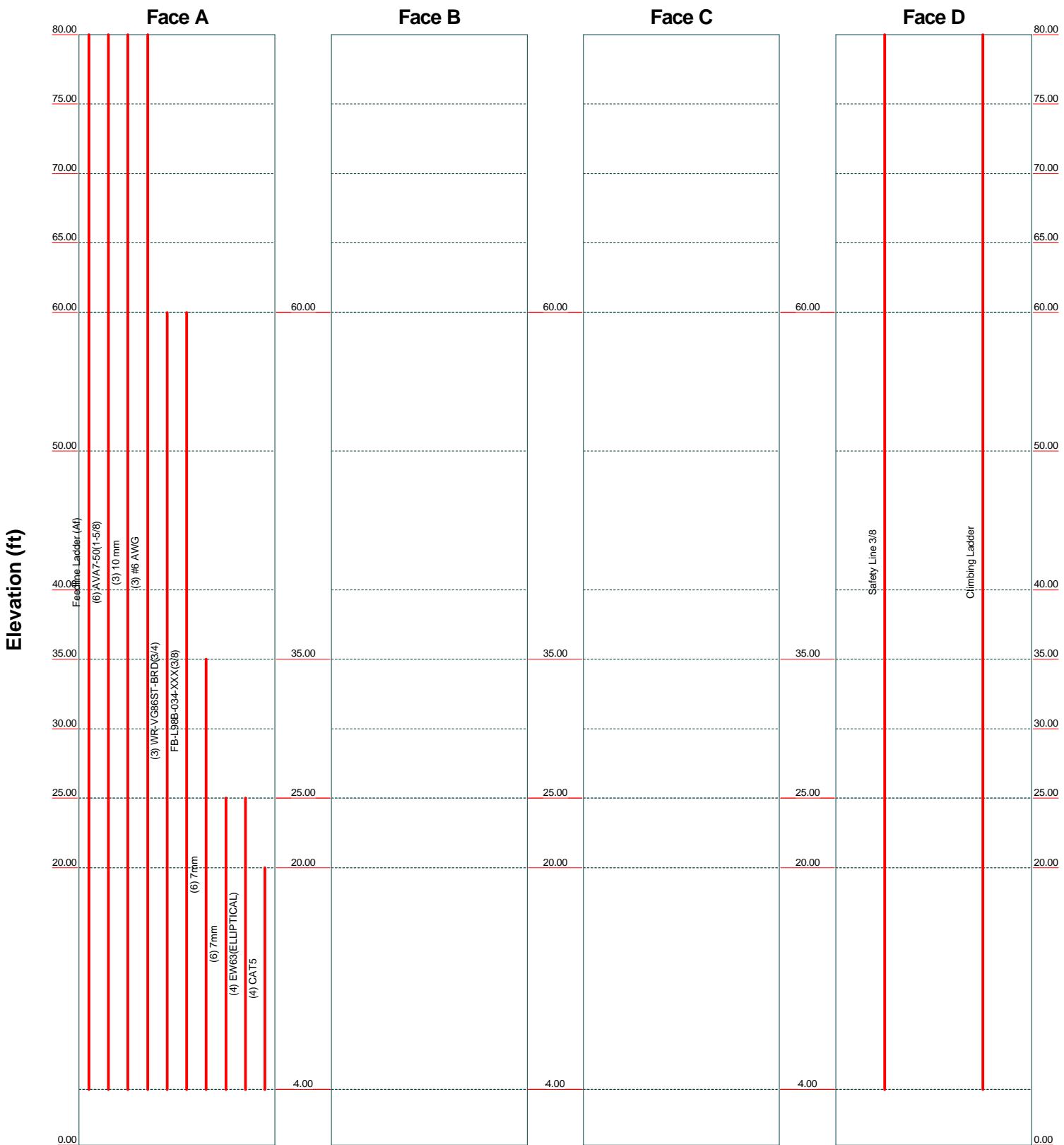
Round

Flat

App In Face

App Out Face

Truss Leg



**Kimley-Horn**

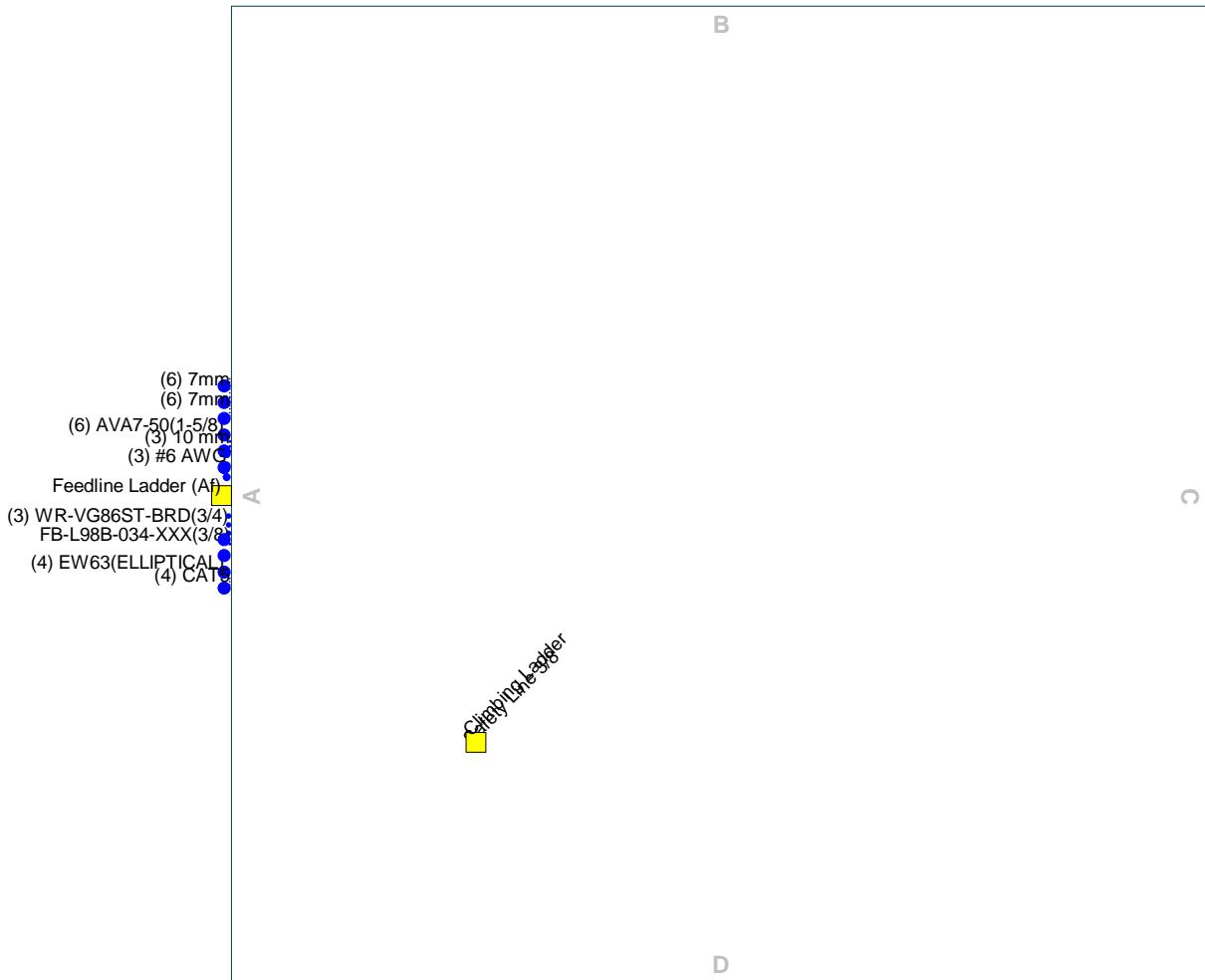
421 Fayetteville St., Suite 600  
Raleigh, NC 27601  
Phone: (919) 677-2000  
FAX: (919) 677-2000

**Oak Creek Coal**

Project:	<b>PR-91471</b>	Drawn by:	Elliot Ziebart	App'd:
Client:	SAC Wireless	Date:	07/20/22	Scale:
Code:	TIA-222-H	Path:	C:\Users\ellie.ziebart\Desktop\Towers\SAC\Union Wireless\Oak Creek Coal Re-Run\Oak Creek Coal -Resources	NTS
				Dwg No: E-7

# Feed Line Plan

Round ————— Flat ————— App In Face ————— App Out Face



<b>tnxTower</b>  <b>Kimley-Horn</b> 421 Fayetteville St., Suite 600 Raleigh, NC 27601 Phone: (919) 677-2000 FAX: (919) 677-2000	<b>Job</b>	Oak Creek Coal	<b>Page</b>
	<b>Project</b>	PR-91471	<b>Date</b> 14:49:46 07/20/22
	<b>Client</b>	SAC Wireless	<b>Designed by</b> Elliot Ziebart

## Tower Input Data

The main tower is a 4x free standing tower with an overall height of 80.00 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 9.00 ft at the top and 13.00 ft at the base.

This tower is designed using the TIA-222-H standard.

The following design criteria apply:

Tower is located in Routt County, Colorado.

Tower base elevation above sea level: 7490.00 ft.

Basic wind speed of 112 mph.

Risk Category III.

Exposure Category C.

Simplified Topographic Factor Procedure for wind speed-up calculations is used.

Topographic Category: 3.

Crest Height: 700.00 ft.

Nominal ice thickness of 0.2500 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

Stress ratio used in tower member design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Exclude From Torque Calculation	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	# Per Row	# Spacing in	Clear Diameter in	Width or Perimeter in	Weight plf
Safety Line 3/8	D	No	No	Ar (CaAa)	80.00 - 4.00 0	-36.000	0.25	1	1	0.3750	0.3750	0.22
Climbing Ladder Feedline Ladder (Af)	D	No	No	Af (CaAa)	80.00 - 4.00 0	-36.000	0.25	1	1	3.0000	3.0000	7.90
AVA7-50(1-5/8)	A	No	No	Af (CaAa)	80.00 - 4.00 0.0000	0	1	1	3.0000	3.0000	8.40	
10 mm #6 AWG	A	No	No	Ar (CaAa)	80.00 - 4.00 0.0000	0.05	3	3	0.3937	0.3937	0.01	
WR-VG86ST-BRD(3/4)	A	No	No	Ar (CaAa)	80.00 - 4.00 0.0000	0.03	3	3	0.5000	1.2720	1.55	
FB-L98B-034-XXX(3/8)	A	No	No	Ar (CaAa)	60.00 - 4.00 0.0000	-0.03	3	3	0.5000	0.7950	0.58	
7mm	A	No	No	Ar (CaAa)	60.00 - 4.00 0.0000	-0.05	1	1	0.3937	0.3937	0.06	
7mm	A	No	No	Ar (CaAa)	35.00 - 4.00 0.0000	0.09	6	6	0.2756	0.2756	0.01	
EW63(ELLITICAL)	A	No	No	Ar (CaAa)	25.00 - 4.00 0.0000	0.11	6	6	0.2756	0.2756	0.01	
CAT5	A	No	No	Ar (CaAa)	20.00 - 4.00 0.0000	-0.07	4	4	0.5000	2.0100	0.51	
						-0.09		4	4	0.2600	0.2600	0.10

<b>tnxTower</b>  <b>Kimley-Horn</b> 421 Fayetteville St., Suite 600 Raleigh, NC 27601 Phone: (919) 677-2000 FAX: (919) 677-2000	Job	Oak Creek Coal					Page	2 of 13
	Project	PR-91471					Date	14:49:46 07/20/22
	Client	SAC Wireless					Designed by	Elliot Ziebart

## Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	CAA		Weight K
						Front	Side	
(2) CWX063X25XM00 w/ MP	A	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	11.81 12.44	10.20 11.64 0.20
(2) CWX063X25XM00 w/ MP	B	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	11.81 12.44	10.20 11.64 0.20
(2) CWX063X25XM00 w/ MP	C	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	11.81 12.44	10.20 11.64 0.20
(2) 12082x w/ MP (Future)	A	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	20.39 21.04	12.59 14.03 0.20
(2) 12082x w/ MP (Future)	B	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	20.39 21.04	12.59 14.03 0.20
(2) 12082x w/ MP (Future)	C	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	20.39 21.04	12.59 14.03 0.20
(3) AHLOA (Future)	A	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	2.23 2.42	1.39 1.55 0.08
(3) AHLOA (Future)	B	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	2.23 2.42	1.39 1.55 0.08
(3) AHLOA (Future)	C	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	2.23 2.42	1.39 1.55 0.08
(2) CMA-UBTULBULBHH/651 7/17/21/21 w/ MP	A	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	22.72 23.39	10.48 11.90 0.15
(2) CMA-UBTULBULBHH/651 7/17/21/21 w/ MP	B	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	22.72 23.39	10.48 11.90 0.15
(2) CMA-UBTULBULBHH/651 7/17/21/21 w/ MP AHFIG	C	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	22.72 23.39	10.48 11.90 0.15
AHFIG	A	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	3.08 3.31	1.40 1.59 0.08
AHFIG	B	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	3.08 3.31	1.40 1.59 0.08
AHFIG	C	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	3.08 3.31	1.40 1.59 0.08
AHLOA	A	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	2.23 2.42	1.39 1.55 0.10
AHLOA	B	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	2.23 2.42	1.39 1.55 0.10
AHLOA	C	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice	2.23 2.42	1.39 1.55 0.10

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	Client SAC Wireless							Designed by Elliot Ziebart

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
AHCA	A	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice 1.29 1.43	0.72 0.83	0.04 0.05
AHCA	B	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice 1.29 1.43	0.72 0.83	0.04 0.05
AHCA	C	From Leg	3.00 0.00 2.00	0.0000	78.00	No Ice 1/2" Ice 1.29 1.43	0.72 0.83	0.04 0.05
PR-UWPT612	A	From Leg	0.00 0.00 0.00	0.0000	78.00	No Ice 1/2" Ice 1.02 1.16	0.67 0.81	0.02 0.03
PR-UWPT612	B	From Leg	0.00 0.00 0.00	0.0000	78.00	No Ice 1/2" Ice 1.02 1.16	0.67 0.81	0.02 0.03
PR-UWPT612	C	From Leg	0.00 0.00 0.00	0.0000	78.00	No Ice 1/2" Ice 1.02 1.16	0.67 0.81	0.02 0.03
FB-L98B-A1041	A	From Leg	0.00 0.00 0.00	0.0000	78.00	No Ice 1/2" Ice 1.02 1.16	0.67 0.81	0.02 0.03
FB-L98B-A1041	B	From Leg	0.00 0.00 0.00	0.0000	78.00	No Ice 1/2" Ice 1.02 1.16	0.67 0.81	0.02 0.03
FB-L98B-A1041	C	From Leg	0.00 0.00 0.00	0.0000	78.00	No Ice 1/2" Ice 1.02 1.16	0.67 0.81	0.02 0.03
Site Pro 1 VFA12-WLL	A	From Leg	0.50 0.00 0.00	0.0000	78.00	No Ice 1/2" Ice 13.20 19.50	9.20 14.60	0.66 0.80
Site Pro 1 VFA12-WLL	B	From Leg	0.50 0.00 0.00	0.0000	78.00	No Ice 1/2" Ice 13.20 19.50	9.20 14.60	0.66 0.80
Site Pro 1 VFA12-WLL	C	From Leg	0.50 0.00 0.00	0.0000	78.00	No Ice 1/2" Ice 13.20 19.50	9.20 14.60	0.66 0.80
(2) NNH4-65C-R6-V3 w/ Mount Pipe	A	From Leg	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 17.31 18.04	10.34 11.86	0.16 0.28
(2) NNH4-65C-R6-V3 w/ Mount Pipe	B	From Leg	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 17.31 18.04	10.34 11.86	0.16 0.28
(2) NNH4-65C-R6-V3 w/ Mount Pipe	C	From Leg	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 17.31 18.04	10.34 11.86	0.16 0.28
Nokia 3JR80236AAAA	A	From Leg	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 2.12 0.00	1.29 0.00	0.05 0.00
Nokia 3JR80236AAAA	B	From Leg	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 2.12 0.00	1.29 0.00	0.05 0.00
Nokia 3JR80236AAAA	C	From Leg	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 2.12 0.00	1.29 0.00	0.05 0.00
Nokia 3JR80235AAAA	A	From Leg	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 2.12 0.00	1.29 0.00	0.05 0.00

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	Project PR-91471							Date 14:49:46 07/20/22
	Client SAC Wireless							Designed by Elliot Ziebart

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front ft <sup>2</sup>	C <sub>AA</sub> Side ft <sup>2</sup>	Weight K
Nokia 3JR80235AAAA	B	From Leg	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 0.00	2.12 0.00 0.00	1.29 0.00 0.00
Nokia 3JR80235AAAA	C	From Leg	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 0.00	2.12 0.00 0.00	1.29 0.00 0.00
Rosenberger D218RRUDSM Clamp	A	From Leg	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 0.00	3.60 0.00 0.00	3.60 0.00 0.00
Rosenberger D218RRUDSM Clamp	B	From Leg	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 0.00	3.60 0.00 0.00	3.60 0.00 0.00
Rosenberger D218RRUDSM Clamp	C	From Leg	3.00 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 0.00	3.60 0.00 0.00	3.60 0.00 0.00
DC9-48-60-24-8C-EV	A	From Leg	0.50 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 0.00	2.74 2.96 5.06	0.03 0.06 0.06
(2) 8' Pipe Mount (2SCH40)	A	From Leg	0.50 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 0.00	1.90 2.73 2.73	0.03 0.04 0.04
(2) 8' Pipe Mount (2SCH40)	B	From Leg	0.50 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 0.00	1.90 2.73 2.73	0.03 0.04 0.04
(2) 8' Pipe Mount (2SCH40)	C	From Leg	0.50 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 0.00	1.90 2.73 2.73	0.03 0.04 0.04
Site Pro 1 VFA10-HD	A	From Leg	0.50 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 0.00	12.10 18.30 14.60	9.20 0.63 0.77
Site Pro 1 VFA10-HD	B	From Leg	0.50 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 0.00	12.10 18.30 14.60	9.20 0.63 0.77
Site Pro 1 VFA10-HD	C	From Leg	0.50 0.00 0.00	0.0000	60.00	No Ice 1/2" Ice 0.00	12.10 18.30 14.60	9.20 0.63 0.77
8' Pipe Mount (2SCH40)	D	From Leg	0.50 0.00 0.00	0.0000	35.00	No Ice 1/2" Ice 0.00	1.90 2.73 2.73	1.90 0.03 0.04
(2) WTM4100	D	From Leg	0.50 0.00 0.00	0.0000	35.00	No Ice 1/2" Ice 0.00	0.38 0.64 0.64	0.38 0.01 0.02
8' Pipe Mount (2SCH40)	D	From Leg	0.50 0.00 0.00	0.0000	25.00	No Ice 1/2" Ice 0.00	1.90 2.73 2.73	1.90 0.03 0.04
8' Pipe Mount (2SCH40)	A	From Leg	0.50 0.00 0.00	0.0000	25.00	No Ice 1/2" Ice 0.00	1.90 2.73 2.73	1.90 0.03 0.04
(2) WTM4100	A	From Leg	0.50 0.00 0.00	0.0000	25.00	No Ice 1/2" Ice 0.00	0.38 0.64 0.64	0.38 0.01 0.02

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## Dishes

Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral Vert ft	Azimuth Adjustment °	3 dB Beam Width °	Elevation ft	Outside Diameter ft	Aperture Area ft²	Weight K
HPX8-65 (Future)	D	Paraboloid w/Shroud (HP)	From Leg	1.00 0.00 0.00	44.7000		35.00	8.00	No Ice 1/2" Ice	50.27 51.32
HPX8-65	D	Paraboloid w/Shroud (HP)	From Leg	1.00 0.00 0.00	44.7000		25.00	8.00	No Ice 1/2" Ice	50.27 51.32
USX6	A	Paraboloid w/Shroud (HP)	From Leg	1.00 0.00 0.00	13.4920		25.00	6.23	No Ice 1/2" Ice	30.48 31.30
B5 - 18" Diameter (Reserved)		Paraboloid w/o Radome	None		0.0000		20.00	1.50	No Ice 1/2" Ice	1.77 0.00
B5 - 18" Diameter (Reserved)		Paraboloid w/o Radome	None		0.0000		20.00	1.50	No Ice 1/2" Ice	1.77 0.00

## Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	80 - 75	1.028	34	0.0925	0.0125
T2	75 - 70	0.928	34	0.0918	0.0118
T3	70 - 65	0.822	34	0.0909	0.0094
T4	65 - 60	0.718	34	0.0884	0.0079
T5	60 - 50	0.619	34	0.0860	0.0065
T6	50 - 40	0.436	34	0.0760	0.0046
T7	40 - 35	0.279	34	0.0611	0.0028
T8	35 - 30	0.211	34	0.0520	0.0018
T9	30 - 25	0.161	34	0.0423	0.0015
T10	25 - 20	0.112	30	0.0326	0.0011
T11	20 - 0	0.080	30	0.0249	0.0009

## Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
78.00	(2) CWX063X25XM00 w/ MP	34	0.988	0.0922	0.0124	49051
60.00	(2) NNH4-65C-R6-V3 w/ Mount Pipe	34	0.619	0.0860	0.0065	55066
35.00	HPX8-65 (Future)	34	0.211	0.0520	0.0018	17313
25.00	HPX8-65	30	0.112	0.0326	0.0011	18418
20.00	B5 - 18" Diameter (Reserved)	30	0.080	0.0249	0.0009	36138

## Maximum Tower Deflections - Design Wind

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Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	80 - 75	3.519	16	0.3159	0.0436
T2	75 - 70	3.177	16	0.3134	0.0411
T3	70 - 65	2.815	16	0.3106	0.0330
T4	65 - 60	2.459	16	0.3022	0.0276
T5	60 - 50	2.118	16	0.2938	0.0227
T6	50 - 40	1.496	9	0.2599	0.0162
T7	40 - 35	0.960	9	0.2089	0.0097
T8	35 - 30	0.729	9	0.1779	0.0061
T9	30 - 25	0.556	9	0.1447	0.0051
T10	25 - 20	0.389	9	0.1115	0.0038
T11	20 - 0	0.276	9	0.0849	0.0031

### Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
78.00	(2) CWX063X25XM00 w/ MP	16	3.384	0.3148	0.0432	14705
60.00	(2) NNH4-65C-R6-V3 w/ Mount Pipe	16	2.118	0.2938	0.0227	16075
35.00	HPX8-65 (Future)	9	0.729	0.1779	0.0061	5055
25.00	HPX8-65	9	0.389	0.1115	0.0038	5393
20.00	B5 - 18" Diameter (Reserved)	9	0.276	0.0849	0.0031	10559

### Bolt Design Data

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load per Bolt K	Ratio Load Allowable	Allowable Ratio	Criteria
T1	80	Diagonal	A325N	0.6250	1	3.34	12.95	0.258 ✓	1	Member Bearing
		Top Girt	A325N	0.6250	1	0.37	13.66	0.027 ✓	1	Member Block Shear
T2	75	Diagonal	A325N	0.6250	1	6.71	12.95	0.518 ✓	1	Member Bearing
		Horizontal	A325N	0.6250	1	2.34	7.75	0.302 ✓	1	Member Block Shear
T3	70	Diagonal	A325N	0.6250	1	6.45	12.95	0.498 ✓	1	Member Bearing
T4	65	Leg	A325N	0.6250	8	1.92	20.34	0.094 ✓	1	Bolt Tension
		Diagonal	A325N	0.6250	1	6.77	12.95	0.523 ✓	1	Member Bearing
		Horizontal	A325N	0.6250	1	0.30	7.75	0.038 ✓	1	Member Block Shear
T5	60	Diagonal	A325N	0.6250	1	9.91	13.81	0.718 ✓	1	Bolt Shear
		Horizontal	A325N	0.6250	1	0.58	7.75	0.075 ✓	1	Member Block Shear
T6	50	Leg	A325N	0.6250	8	6.11	20.34	0.300 ✓	1	Bolt Tension
		Diagonal	A325N	0.6250	1	10.84	13.81	0.785 ✓	1	Bolt Shear
		Horizontal	A325N	0.6250	1	0.84	7.75	0.109 ✓	1	Member Block

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Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load per Bolt K	Ratio Load Allowable	Allowable Ratio	Criteria
T7	40	Diagonal	A325N	0.6250	1	7.90	13.81	0.573 ✓	1	Shear Bolt Shear
T8	35	Diagonal	A325N	0.6250	1	8.21	13.81	0.595 ✓	1	Bolt Shear
		Horizontal	A325N	0.6250	1	1.61	7.75	0.207 ✓	1	Member Block Shear
T9	30	Leg	A325N	0.7500	8	10.18	30.10	0.338 ✓	1	Bolt Tension
		Diagonal	A325N	0.6250	1	7.29	13.81	0.528 ✓	1	Bolt Shear
T10	25	Diagonal	A325N	0.6250	1	8.11	13.81	0.588 ✓	1	Bolt Shear
		Horizontal	A325N	0.6250	1	2.02	9.11	0.221 ✓	1	Member Block Shear
T11	20	Diagonal	A325N	0.6250	2	11.94	13.81	0.865 ✓	1	Bolt Shear
		Horizontal	A325N	0.6250	2	0.68	8.22	0.083 ✓	1	Member Block Shear
		Top Girt	A325N	0.6250	2	4.49	8.22	0.546 ✓	1	Member Block Shear

## Compression Checks

### Leg Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	ϕP <sub>n</sub> K	Ratio P <sub>u</sub> / ϕP <sub>n</sub>
T1	80 - 75	P4.5 x 0.237	5.00	5.00	39.7 K=1.00	3.1741	-8.65	118.16	0.073 <sup>1</sup> ✓
T2	75 - 70	P4.5 x 0.237	5.00	5.00	39.7 K=1.00	3.1741	-8.70	118.16	0.074 <sup>1</sup> ✓
T3	70 - 65	P4.5 x 0.237	5.00	5.00	39.7 K=1.00	3.1741	-19.37	118.16	0.164 <sup>1</sup> ✓
T4	65 - 60	P4.5 x 0.237	5.00	5.00	39.7 K=1.00	3.1741	-19.48	118.16	0.165 <sup>1</sup> ✓
T5	60 - 50	P4.5 x 0.237	10.00	5.00	39.7 K=1.00	3.1741	-38.67	118.16	0.327 <sup>1</sup> ✓
T6	50 - 40	P4.5 x 0.237	10.00	5.00	39.7 K=1.00	3.1741	-56.29	118.16	0.476 <sup>1</sup> ✓
T7	40 - 35	P4.5 x 0.237	5.01	5.01	39.8 K=1.00	3.1741	-72.72	118.09	0.616 <sup>1</sup> ✓
T8	35 - 30	P4.5 x 0.237	5.01	5.01	39.8 K=1.00	3.1741	-72.93	118.09	0.618 <sup>1</sup> ✓
T9	30 - 25	P4.5 x 0.237	5.01	5.01	39.8 K=1.00	3.1741	-91.47	118.09	0.775 <sup>1</sup> ✓
T10	25 - 20	P5.5625 x 0.258	5.01	5.01	32.0 K=1.00	4.2995	-91.93	166.13	0.553 <sup>1</sup> ✓
T11	20 - 0	P5.5625 x 0.258	20.05	10.03	64.1 K=1.00	4.2995	-86.62	135.05	0.641 <sup>1</sup> ✓

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Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio
			ft	ft		in <sup>2</sup>	K	K	$\frac{P_u}{\phi P_n}$

<sup>1</sup> P<sub>u</sub> / ϕP<sub>n</sub> controls

### Diagonal Design Data (Compression)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio
			ft	ft		in <sup>2</sup>	K	K	$\frac{P_u}{\phi P_n}$
T1	80 - 75	P1.5x.145	6.73	6.45	124.3 K=1.00	0.7995	-3.24	11.70	0.277 <sup>1</sup>
T2	75 - 70	P1.5x.145	6.73	6.45	124.3 K=1.00	0.7995	-6.74	11.70	0.576 <sup>1</sup>
T3	70 - 65	P1.5x.145	6.73	6.45	124.3 K=1.00	0.7995	-6.57	11.70	0.562 <sup>1</sup>
T4	65 - 60	P1.5x.145	6.73	6.45	124.3 K=1.00	0.7995	-6.96	11.70	0.595 <sup>1</sup>
T5	60 - 50	P2.5x.203	6.73	6.45	81.7 K=1.00	1.7040	-9.91	45.05	0.220 <sup>1</sup>
T6	50 - 40	P2.5x.203	6.73	6.45	81.7 K=1.00	1.7040	-10.84	45.05	0.241 <sup>1</sup>
T7	40 - 35	P2.5x.203	6.73	6.45	81.7 K=1.00	1.7040	-7.90	45.02	0.176 <sup>1</sup>
T8	35 - 30	P2.5x.203	7.08	6.81	86.3 K=1.00	1.7040	-8.21	42.77	0.192 <sup>1</sup>
T9	30 - 25	P2.5x.203	7.08	6.81	86.3 K=1.00	1.7040	-6.87	42.77	0.161 <sup>1</sup>
T10	25 - 20	P2.5x.203	7.44	7.12	90.2 K=1.00	1.7040	-8.06	40.80	0.198 <sup>1</sup>
T11	20 - 0	P3x.216	11.94	11.51	118.7 K=1.00	2.2285	-23.89	35.71	0.669 <sup>1</sup>

<sup>1</sup> P<sub>u</sub> / ϕP<sub>n</sub> controls

### Horizontal Design Data (Compression)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio
			ft	ft		in <sup>2</sup>	K	K	$\frac{P_u}{\phi P_n}$
T2	75 - 70	2L1 3/4x1 3/4x1/8	9.00	4.19	92.2 K=1.00	0.8438	-2.28	22.26	0.102 <sup>1</sup>
T4	65 - 60	2L1 3/4x1 3/4x1/8	9.00	8.39	138.0 K=1.00	0.8438	-0.29	12.68	0.023 <sup>1</sup>
T5	60 - 50	2L1 3/4x1 3/4x1/8	9.00	6.35	138.0 K=1.00	0.8438	-0.58	12.68	0.046 <sup>1</sup>
T6	50 - 40	2L1 3/4x1 3/4x1/8	9.00	4.19	92.2 K=1.00	0.8438	-0.84	22.26	0.038 <sup>1</sup>
T8	35 - 30	2L1 3/4x1 3/4x1/8	9.50	4.44	97.7	0.8438	-1.58	21.26	0.074 <sup>1</sup>

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Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio $\frac{P_u}{\phi P_n}$
	ft		ft	ft		in <sup>2</sup>	K	K	
T10	25 - 20	2L2x2x1/8	10.50	4.90	K=1.00 K=1.00	93.9	0.9600	-1.95	24.45 0.080 <sup>1</sup>
T11	20 - 0	2L2x2x1/8	12.00	5.57	K=1.00	106.8	0.9600	-1.36	21.82 0.062 <sup>1</sup>

<sup>1</sup> P<sub>u</sub> / ϕP<sub>n</sub> controls

### Top Girt Design Data (Compression)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio $\frac{P_u}{\phi P_n}$
	ft		ft	ft		in <sup>2</sup>	K	K	
T1	80 - 75	2L2x2x3/16x3/8	9.00	8.39	K=1.00	163.1	1.4300	-0.47	15.39 0.031 <sup>1</sup>
T11	20 - 0	2L2x2x1/8x3/8	11.00	5.07	K=1.00	99.1	0.9600	-8.02	20.98 0.382 <sup>1</sup>

2L 'a' > 29.0126 in - 201

<sup>1</sup> P<sub>u</sub> / ϕP<sub>n</sub> controls

### Inner Bracing Design Data (Compression)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio $\frac{P_u}{\phi P_n}$
	ft		ft	ft		in <sup>2</sup>	K	K	
T2	75 - 70	L1 3/4x1 3/4x1/8	6.36	6.36	K=1.00	220.2	0.4219	-0.01	2.49 0.003 <sup>1</sup>
T6	50 - 40	L1 3/4x1 3/4x1/8	6.36	6.36	K=1.00	220.2	0.4219	-0.04	2.49 0.015 <sup>1</sup>
T8	35 - 30	L1 3/4x1 3/4x1/8	6.72	6.72	K=1.00	232.4	0.4219	-0.05	2.24 0.021 <sup>1</sup>
T9	30 - 25	L1 3/4x1 3/4x1/8	7.42	7.42	K=1.00	256.9	0.4219	-0.04	1.83 0.019 <sup>1</sup>
T10	25 - 20	KL/R > 250 (C) - 171 L1 3/4x1 3/4x1/8	7.78	7.78	K=1.00	269.1	0.4219	-0.02	1.67 0.011 <sup>1</sup>
T11	20 - 0	KL/R > 250 (C) - 190 L1 3/4x1 3/4x1/8	12.00	12.00	K=1.00	415.2	0.4219	-0.04	0.70 0.062 <sup>1</sup>

KL/R > 250 (C) - 218

<sup>1</sup> P<sub>u</sub> / ϕP<sub>n</sub> controls

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## Tension Checks

### Leg Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio P <sub>u</sub> / ϕP <sub>n</sub>
	ft		ft	ft		in <sup>2</sup>	K	K	
T1	80 - 75	P4.5 x 0.237	5.00	5.00	39.7	3.1741	4.57	131.41	0.035 <sup>1</sup>
T2	75 - 70	P4.5 x 0.237	5.00	5.00	39.7	3.1741	4.56	131.41	0.035 <sup>1</sup>
T3	70 - 65	P4.5 x 0.237	5.00	5.00	39.7	3.1741	15.39	131.41	0.117 <sup>1</sup>
T4	65 - 60	P4.5 x 0.237	5.00	5.00	39.7	3.1741	15.36	131.41	0.117 <sup>1</sup>
T5	60 - 50	P4.5 x 0.237	10.00	5.00	39.7	3.1741	32.45	131.41	0.247 <sup>1</sup>
T6	50 - 40	P4.5 x 0.237	10.00	5.00	39.7	3.1741	48.90	131.41	0.372 <sup>1</sup>
T7	40 - 35	P4.5 x 0.237	5.01	5.01	39.8	3.1741	64.99	131.41	0.495 <sup>1</sup>
T8	35 - 30	P4.5 x 0.237	5.01	5.01	39.8	3.1741	64.78	131.41	0.493 <sup>1</sup>
T9	30 - 25	P4.5 x 0.237	5.01	5.01	39.8	3.1741	81.41	131.41	0.620 <sup>1</sup>
T10	25 - 20	P5.5625 x 0.258	5.01	5.01	32.0	4.2995	81.24	178.00	0.456 <sup>1</sup>
T11	20 - 0	P5.5625 x 0.258	20.05	10.03	64.1	4.2995	79.39	178.00	0.446 <sup>1</sup>

<sup>1</sup> P<sub>u</sub> / ϕP<sub>n</sub> controls

### Diagonal Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio P <sub>u</sub> / ϕP <sub>n</sub>
	ft		ft	ft		in <sup>2</sup>	K	K	
T1	80 - 75	P1.5x.145	6.73	6.45	124.3	0.7995	3.34	33.10	0.101 <sup>1</sup>
T2	75 - 70	P1.5x.145	6.73	6.45	124.3	0.7995	6.71	33.10	0.203 <sup>1</sup>
T3	70 - 65	P1.5x.145	6.73	6.45	124.3	0.7995	6.45	33.10	0.195 <sup>1</sup>
T4	65 - 60	P1.5x.145	6.73	6.45	124.3	0.7995	6.77	33.10	0.204 <sup>1</sup>
T5	60 - 50	P2.5x.203	6.73	6.45	81.7	1.7040	9.81	70.55	0.139 <sup>1</sup>
T6	50 - 40	P2.5x.203	6.73	6.45	81.7	1.7040	10.47	70.55	0.148 <sup>1</sup>
T7	40 - 35	P2.5x.203	6.73	6.45	81.7	1.7040	7.23	70.55	0.103 <sup>1</sup>

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Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio $\frac{P_u}{\phi P_n}$
	ft		ft	ft		in <sup>2</sup>	K	K	
T8	35 - 30	P2.5x.203	7.08	6.81	86.3	1.7040	7.54	70.55	0.107 <sup>1</sup>
T9	30 - 25	P2.5x.203	7.08	6.81	86.3	1.7040	7.29	70.55	0.103 <sup>1</sup>
T10	25 - 20	P2.5x.203	7.44	7.12	90.2	1.7040	8.11	70.55	0.115 <sup>1</sup>
T11	20 - 0	P3x.216	11.94	11.51	118.7	2.2285	21.14	92.26	0.229 <sup>1</sup>

<sup>1</sup> P<sub>u</sub> / ϕP<sub>n</sub> controls

### Horizontal Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio $\frac{P_u}{\phi P_n}$
	ft		ft	ft		in <sup>2</sup>	K	K	
T2	75 - 70	2L1 3/4x1 3/4x1/8	9.00	4.19	94.8	0.4922	2.34	21.41	0.109 <sup>1</sup>
T4	65 - 60	2L1 3/4x1 3/4x1/8	9.00	8.39	106.4	0.4922	0.30	21.41	0.014 <sup>1</sup>
T5	60 - 50	2L1 3/4x1 3/4x1/8	9.00	6.35	106.4	0.4922	0.58	21.41	0.027 <sup>1</sup>
T6	50 - 40	2L1 3/4x1 3/4x1/8	9.00	4.19	94.8	0.4922	0.84	21.41	0.039 <sup>1</sup>
T8	35 - 30	2L1 3/4x1 3/4x1/8	9.50	4.44	100.3	0.4922	1.61	21.41	0.075 <sup>1</sup>
T10	25 - 20	2L2x2x1/8	10.50	4.90	96.2	0.5794	2.02	25.20	0.080 <sup>1</sup>
T11	20 - 0	2L2x2x1/8	12.00	5.57	110.6	0.5794	1.36	25.20	0.054 <sup>1</sup>

<sup>1</sup> P<sub>u</sub> / ϕP<sub>n</sub> controls

### Top Girt Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio $\frac{P_u}{\phi P_n}$
	ft		ft	ft		in <sup>2</sup>	K	K	
T1	80 - 75	2L2x2x3/16x3/8	9.00	8.39	167.7	0.8616	0.37	37.48	0.010 <sup>1</sup>
T11	20 - 0	2L2x2x1/8x3/8	11.00	5.07	101.0	0.5794	8.98	25.20	0.356 <sup>1</sup>

2L 'a' > 29.0126 in - 199

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<sup>1</sup>  $P_u / \phi P_n$  controls

### Redundant Vertical Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio $\frac{P_u}{\phi P_n}$
	ft		ft	ft		in <sup>2</sup>	K	K	
T10	25 - 20	2L1 3/4x1 3/4x1/8x3/8	5.01	5.01	110.1	0.8438	0.11	27.34	0.004 <sup>1</sup> ✓

2L 'a' > 28.6358 in - 183

<sup>1</sup>  $P_u / \phi P_n$  controls

### Inner Bracing Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio $\frac{P_u}{\phi P_n}$
	ft		ft	ft		in <sup>2</sup>	K	K	
T2	75 - 70	L1 3/4x1 3/4x1/8	6.36	6.36	139.9	0.4219	0.01	13.67	0.000 <sup>1</sup> ✓
T6	50 - 40	L1 3/4x1 3/4x1/8	6.36	6.36	139.9	0.4219	0.04	13.67	0.003 <sup>1</sup> ✓
T8	35 - 30	L1 3/4x1 3/4x1/8	6.72	6.72	147.7	0.4219	0.03	13.67	0.002 <sup>1</sup> ✓
T9	30 - 25	L1 3/4x1 3/4x1/8	7.42	7.42	163.3	0.4219	0.03	13.67	0.002 <sup>1</sup> ✓
T10	25 - 20	L1 3/4x1 3/4x1/8	7.78	7.78	171.0	0.4219	0.02	13.67	0.001 <sup>1</sup> ✓
T11	20 - 0	L1 3/4x1 3/4x1/8	12.00	12.00	263.9	0.4219	0.05	13.67	0.004 <sup>1</sup> ✓

<sup>1</sup>  $P_u / \phi P_n$  controls

### Section Capacity Table

Section No.	Elevation	Component Type	Size	Critical Element	P K	ϕP <sub>allow</sub> K	% Capacity	Pass Fail
	ft							
T1	80 - 75	Leg	P4.5 x 0.237	3	-8.65	118.16	7.3	Pass
T2	75 - 70	Leg	P4.5 x 0.237	23	-8.70	118.16	7.4	Pass
T3	70 - 65	Leg	P4.5 x 0.237	41	-19.37	118.16	16.4	Pass
T4	65 - 60	Leg	P4.5 x 0.237	57	-19.48	118.16	16.5	Pass
T5	60 - 50	Leg	P4.5 x 0.237	69	-38.67	118.16	32.7	Pass
T6	50 - 40	Leg	P4.5 x 0.237	93	-56.29	118.16	47.6	Pass
T7	40 - 35	Leg	P4.5 x 0.237	122	-72.72	118.09	61.6	Pass
T8	35 - 30	Leg	P4.5 x 0.237	138	-72.93	118.09	61.8	Pass
T9	30 - 25	Leg	P4.5 x 0.237	155	-91.47	118.09	77.5	Pass
T10	25 - 20	Leg	P5.5625 x 0.258	176	-91.93	166.13	55.3	Pass
T11	20 - 0	Leg	P5.5625 x 0.258	197	-86.62	135.05	64.1	Pass
T1	80 - 75	Diagonal	P1.5x.145	17	-3.24	11.70	27.7	Pass
T2	75 - 70	Diagonal	P1.5x.145	29	-6.74	11.70	57.6	Pass
T3	70 - 65	Diagonal	P1.5x.145	49	-6.57	11.70	56.2	Pass
T4	65 - 60	Diagonal	P1.5x.145	63	-6.96	11.70	59.5	Pass
T5	60 - 50	Diagonal	P2.5x.203	77	-9.91	45.05	22.0	Pass

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Section No.	Elevation ft	Component Type	Size	Critical Element	P K	$\phi P_{allow}$ K	% Capacity	Pass Fail
T6	50 - 40	Diagonal	P2.5x.203	102	-10.84	45.05	71.8 (b)	24.1 Pass
T7	40 - 35	Diagonal	P2.5x.203	130	-7.90	45.02	78.5 (b)	17.6 Pass
T8	35 - 30	Diagonal	P2.5x.203	144	-8.21	42.77	57.3 (b)	19.2 Pass
T9	30 - 25	Diagonal	P2.5x.203	164	-6.87	42.77	59.5 (b)	16.1 Pass
T10	25 - 20	Diagonal	P2.5x.203	184	-8.06	40.80	52.8 (b)	19.8 Pass
T11	20 - 0	Diagonal	P3x.216	204	-23.89	35.71	58.8 (b)	66.9 Pass
T2	75 - 70	Horizontal	2L1 3/4x1 3/4x1/8	15	2.34	21.41	86.5 (b)	10.9 Pass
T4	65 - 60	Horizontal	2L1 3/4x1 3/4x1/8	48	-0.29	12.68	30.2 (b)	2.3 Pass
T5	60 - 50	Horizontal	2L1 3/4x1 3/4x1/8	76	-0.58	12.68	3.8 (b)	4.6 Pass
T6	50 - 40	Horizontal	2L1 3/4x1 3/4x1/8	100	0.84	21.41	7.5 (b)	3.9 Pass
T8	35 - 30	Horizontal	2L1 3/4x1 3/4x1/8	123	1.61	21.41	10.9 (b)	7.5 Pass
T10	25 - 20	Horizontal	2L2x2x1/8	156	2.02	25.20	20.7 (b)	8.0 Pass
T11	20 - 0	Horizontal	2L2x2x1/8	208	-1.36	21.82	22.1 (b)	6.2 Pass
T1	80 - 75	Top Girt	2L2x2x3/16x3/8	8	-0.47	15.39	8.3 (b)	3.1 Pass
T11	20 - 0	Top Girt	2L2x2x1/8x3/8	201	-8.02	20.98	54.6 (b)	38.2 Pass
T10	25 - 20	Redund Vert Bracing	2L1 3/4x1 3/4x1/8x3/8	183	0.11	27.34	0.4	Pass
T2	75 - 70	Inner Bracing	L1 3/4x1 3/4x1/8	37	-0.00	1.25	0.3	Pass
T6	50 - 40	Inner Bracing	L1 3/4x1 3/4x1/8	107	-0.04	2.49	1.5	Pass
T8	35 - 30	Inner Bracing	L1 3/4x1 3/4x1/8	148	-0.05	2.24	2.1	Pass
T9	30 - 25	Inner Bracing	L1 3/4x1 3/4x1/8	171	-0.04	1.83	1.9	Pass
T10	25 - 20	Inner Bracing	L1 3/4x1 3/4x1/8	190	-0.02	1.67	1.1	Pass
T11	20 - 0	Inner Bracing	L1 3/4x1 3/4x1/8	218	-0.04	0.70	6.2	Pass
						Summary	ELC:	Existing + Phase 1
						Leg (T9)	77.5	Pass
						Diagonal (T11)	86.5	Pass
						Horizontal (T2)	30.2	Pass
						Top Girt (T11)	54.6	Pass
						Redund Vert Bracing (T10)	0.4	Pass
						Inner Bracing (T11)	6.2	Pass
						Bolt Checks Rating =	86.5	Pass
							86.5	Pass

---

## APPENDIX C

### tnxTower Output File – Phase 2



# Feed Line Distribution Chart

**0' - 80'**

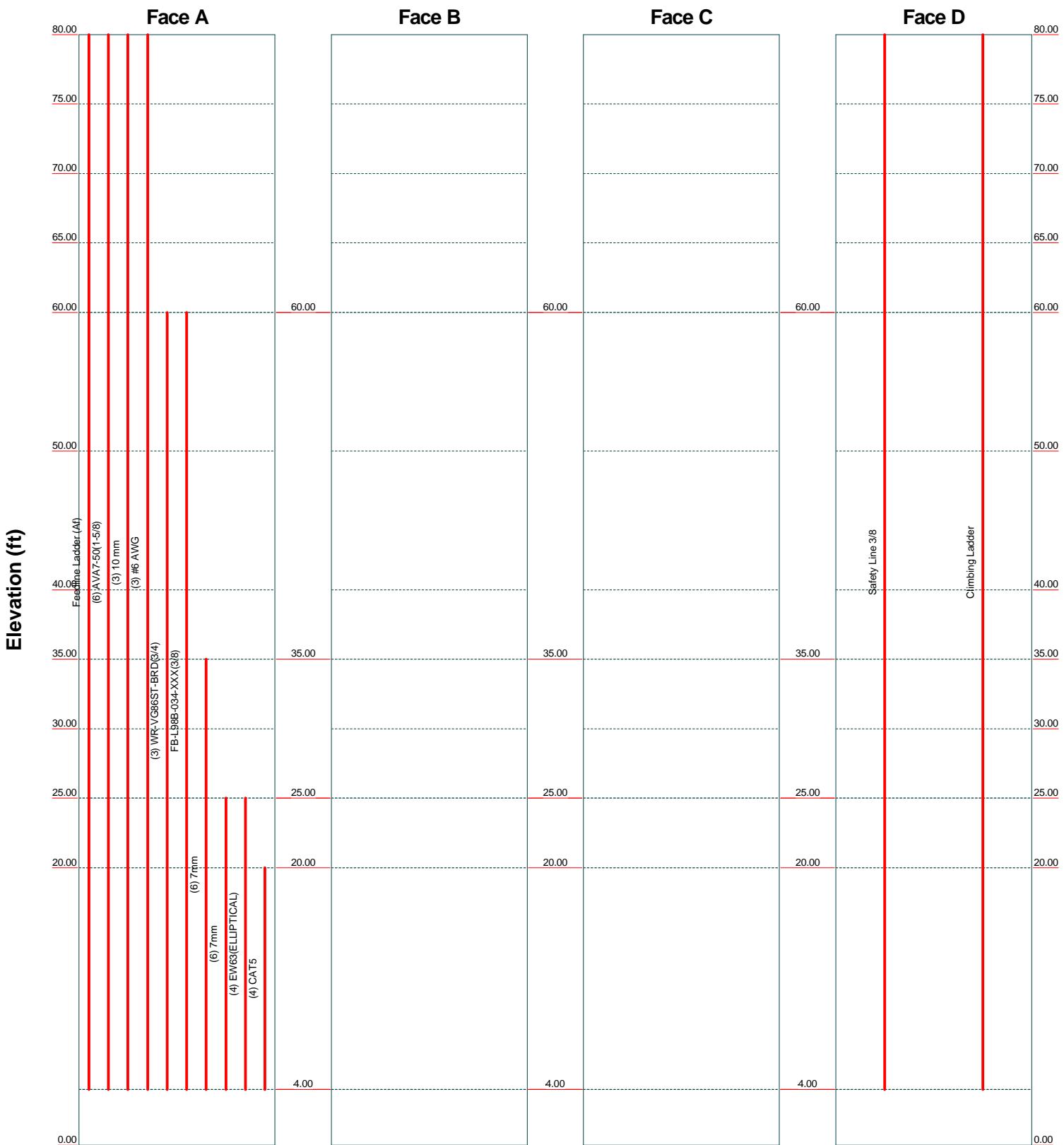
Round

Flat

App In Face

App Out Face

Truss Leg



**Kimley-Horn**

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**Job: Oak Creek Coal**

Project: **PR-91471**

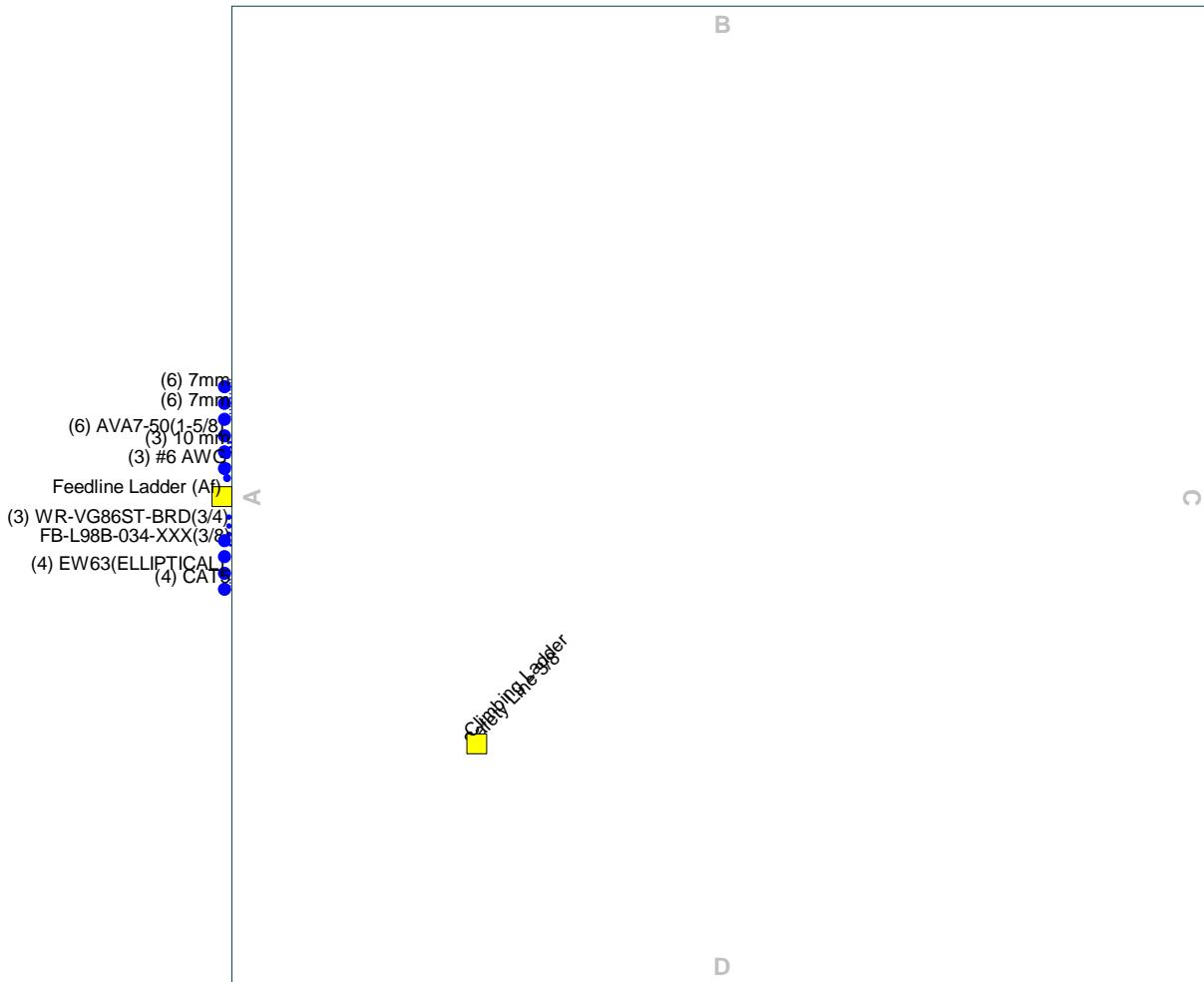
Client: SAC Wireless Drawn by: Elliot Ziebart App'd:

Code: TIA-222-H Date: 07/20/22 Scale: NTS

Path: C:\Users\ellzieb\Desktop\Towers\SAC\Union Wireless\Oak Creek Coal Re-Run\Oak Creek Coal -Resources Dwg No: E-7

# Feed Line Plan

Round ————— Flat ————— App In Face ————— App Out Face















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Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load per Bolt K	Ratio Load Allowable	Allowable Ratio	Criteria
T3	70	Diagonal	A325N	0.6250	1	5.54	12.95	0.428 ✓	1	Shear Member Bearing
T4	65	Leg	A325N	0.6250	8	1.63	20.34	0.080 ✓	1	Bolt Tension
		Diagonal	A325N	0.6250	1	5.83	12.95	0.450 ✓	1	Member Bearing
		Horizontal	A325N	0.6250	1	0.27	7.75	0.035 ✓	1	Member Block Shear
T5	60	Diagonal	A325N	0.6250	1	8.96	13.81	0.649 ✓	1	Bolt Shear
		Horizontal	A325N	0.6250	1	0.52	7.75	0.067 ✓	1	Member Block Shear
T6	50	Leg	A325N	0.6250	8	5.42	20.34	0.266 ✓	1	Bolt Tension
		Diagonal	A325N	0.6250	1	9.87	13.81	0.715 ✓	1	Bolt Shear
		Horizontal	A325N	0.6250	1	0.76	7.75	0.098 ✓	1	Member Block Shear
T7	40	Diagonal	A325N	0.6250	1	7.21	13.81	0.522 ✓	1	Bolt Shear
T8	35	Diagonal	A325N	0.6250	1	7.63	13.81	0.553 ✓	1	Bolt Shear
		Horizontal	A325N	0.6250	1	1.56	7.75	0.201 ✓	1	Member Block Shear
T9	30	Leg	A325N	0.7500	8	9.20	30.10	0.306 ✓	1	Bolt Tension
		Diagonal	A325N	0.6250	1	6.82	13.81	0.494 ✓	1	Bolt Shear
T10	25	Diagonal	A325N	0.6250	1	7.61	13.81	0.551 ✓	1	Bolt Shear
		Horizontal	A325N	0.6250	1	1.95	9.11	0.215 ✓	1	Member Block Shear
T11	20	Diagonal	A325N	0.6250	2	11.33	13.81	0.821 ✓	1	Bolt Shear
		Horizontal	A325N	0.6250	2	0.63	8.22	0.076 ✓	1	Member Block Shear
		Top Girt	A325N	0.6250	2	4.15	8.22	0.505 ✓	1	Member Block Shear

## Compression Checks

## Leg Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	ϕP <sub>n</sub> K	Ratio P <sub>u</sub> / ϕP <sub>n</sub>
T1	80 - 75	P4.5 x 0.237	5.00	5.00	39.7 K=1.00	3.1741	-7.65	118.16	0.065 <sup>1</sup> ✓
T2	75 - 70	P4.5 x 0.237	5.00	5.00	39.7 K=1.00	3.1741	-7.70	118.16	0.065 <sup>1</sup> ✓
T3	70 - 65	P4.5 x 0.237	5.00	5.00	39.7 K=1.00	3.1741	-16.91	118.16	0.143 <sup>1</sup> ✓
T4	65 - 60	P4.5 x 0.237	5.00	5.00	39.7 K=1.00	3.1741	-17.02	118.16	0.144 <sup>1</sup> ✓
T5	60 - 50	P4.5 x 0.237	10.00	5.00	39.7 K=1.00	3.1741	-34.40	118.16	0.291 <sup>1</sup> ✓



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### Horizontal Design Data (Compression)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio P <sub>u</sub> / ϕP <sub>n</sub>
	ft		ft	ft		in <sup>2</sup>	K	K	ϕP <sub>n</sub>
T2	75 - 70	2L1 3/4x1 3/4x1/8	9.00	4.19	92.2 K=1.00	0.8438	-1.92	22.26	0.086 <sup>1</sup>
T4	65 - 60	2L1 3/4x1 3/4x1/8	9.00	8.39	138.0 K=1.00	0.8438	-0.26	12.68	0.020 <sup>1</sup>
T5	60 - 50	2L1 3/4x1 3/4x1/8	9.00	6.35	138.0 K=1.00	0.8438	-0.52	12.68	0.041 <sup>1</sup>
T6	50 - 40	2L1 3/4x1 3/4x1/8	9.00	4.19	92.2 K=1.00	0.8438	-0.76	22.26	0.034 <sup>1</sup>
T8	35 - 30	2L1 3/4x1 3/4x1/8	9.50	4.44	97.7 K=1.00	0.8438	-1.50	21.26	0.071 <sup>1</sup>
T10	25 - 20	2L2x2x1/8	10.50	4.90	93.9 K=1.00	0.9600	-1.85	24.45	0.075 <sup>1</sup>
T11	20 - 0	2L2x2x1/8	12.00	5.57	106.8 K=1.00	0.9600	-1.25	21.82	0.057 <sup>1</sup>

<sup>1</sup> P<sub>u</sub> / ϕP<sub>n</sub> controls

### Top Girt Design Data (Compression)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio P <sub>u</sub> / ϕP <sub>n</sub>
	ft		ft	ft		in <sup>2</sup>	K	K	ϕP <sub>n</sub>
T1	80 - 75	2L2x2x3/16x3/8	9.00	8.39	163.1 K=1.00	1.4300	-0.42	15.39	0.028 <sup>1</sup>
T11	20 - 0	2L2x2x1/8x3/8	11.00	5.07	99.1 K=1.00	0.9600	-7.34	20.98	0.350 <sup>1</sup>

2L 'a' > 29.0126 in - 201

<sup>1</sup> P<sub>u</sub> / ϕP<sub>n</sub> controls

### Inner Bracing Design Data (Compression)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio P <sub>u</sub> / ϕP <sub>n</sub>
	ft		ft	ft		in <sup>2</sup>	K	K	ϕP <sub>n</sub>
T2	75 - 70	L1 3/4x1 3/4x1/8	6.36	6.36	220.2 K=1.00	0.4219	-0.01	2.49	0.003 <sup>1</sup>
T6	50 - 40	L1 3/4x1 3/4x1/8	6.36	6.36	220.2 K=1.00	0.4219	-0.03	2.49	0.011 <sup>1</sup>
T8	35 - 30	L1 3/4x1 3/4x1/8	6.72	6.72	232.4 K=1.00	0.4219	-0.04	2.24	0.018 <sup>1</sup>
T9	30 - 25	L1 3/4x1 3/4x1/8	7.42	7.42	256.9 K=1.00	0.4219	-0.03	1.83	0.016 <sup>1</sup>

KL/R > 250 (C) - 171

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Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio $\frac{P_u}{\phi P_n}$
	ft		ft	ft		in <sup>2</sup>	K	K	
T10	25 - 20	L1 3/4x1 3/4x1/8	7.78	7.78	269.1 K=1.00	0.4219	-0.02	1.67	0.009 <sup>1</sup> ✓
T11	20 - 0	KL/R > 250 (C) - 190 L1 3/4x1 3/4x1/8	12.00	12.00	415.2 K=1.00	0.4219	-0.04	0.70	0.052 <sup>1</sup> ✓
		KL/R > 250 (C) - 218							

<sup>1</sup>  $P_u / \phi P_n$  controls

## Tension Checks

### Leg Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio $\frac{P_u}{\phi P_n}$
	ft		ft	ft		in <sup>2</sup>	K	K	
T1	80 - 75	P4.5 x 0.237	5.00	5.00	39.7	3.1741	3.79	131.41	0.029 <sup>1</sup> ✓
T2	75 - 70	P4.5 x 0.237	5.00	5.00	39.7	3.1741	3.78	131.41	0.029 <sup>1</sup> ✓
T3	70 - 65	P4.5 x 0.237	5.00	5.00	39.7	3.1741	13.11	131.41	0.100 <sup>1</sup> ✓
T4	65 - 60	P4.5 x 0.237	5.00	5.00	39.7	3.1741	13.08	131.41	0.100 <sup>1</sup> ✓
T5	60 - 50	P4.5 x 0.237	10.00	5.00	39.7	3.1741	28.38	131.41	0.216 <sup>1</sup> ✓
T6	50 - 40	P4.5 x 0.237	10.00	5.00	39.7	3.1741	43.40	131.41	0.330 <sup>1</sup> ✓
T7	40 - 35	P4.5 x 0.237	5.01	5.01	39.8	3.1741	58.31	131.41	0.444 <sup>1</sup> ✓
T8	35 - 30	P4.5 x 0.237	5.01	5.01	39.8	3.1741	58.10	131.41	0.442 <sup>1</sup> ✓
T9	30 - 25	P4.5 x 0.237	5.01	5.01	39.8	3.1741	73.64	131.41	0.560 <sup>1</sup> ✓
T10	25 - 20	P5.5625 x 0.258	5.01	5.01	32.0	4.2995	73.47	178.00	0.413 <sup>1</sup> ✓
T11	20 - 0	P5.5625 x 0.258	20.05	10.03	64.1	4.2995	72.76	178.00	0.409 <sup>1</sup> ✓

<sup>1</sup>  $P_u / \phi P_n$  controls

### Diagonal Design Data (Tension)

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Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	ϕP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T1	80 - 75	P1.5x.145	6.73	6.45	124.3	0.7995	2.85	33.10	0.086 <sup>1</sup> ✓
T2	75 - 70	P1.5x.145	6.73	6.45	124.3	0.7995	5.68	33.10	0.172 <sup>1</sup> ✓
T3	70 - 65	P1.5x.145	6.73	6.45	124.3	0.7995	5.54	33.10	0.167 <sup>1</sup> ✓
T4	65 - 60	P1.5x.145	6.73	6.45	124.3	0.7995	5.83	33.10	0.176 <sup>1</sup> ✓
T5	60 - 50	P2.5x.203	6.73	6.45	81.7	1.7040	8.86	70.55	0.126 <sup>1</sup> ✓
T6	50 - 40	P2.5x.203	6.73	6.45	81.7	1.7040	9.51	70.55	0.135 <sup>1</sup> ✓
T7	40 - 35	P2.5x.203	6.73	6.45	81.7	1.7040	6.56	70.55	0.093 <sup>1</sup> ✓
T8	35 - 30	P2.5x.203	7.08	6.81	86.3	1.7040	6.90	70.55	0.098 <sup>1</sup> ✓
T9	30 - 25	P2.5x.203	7.08	6.81	86.3	1.7040	6.82	70.55	0.097 <sup>1</sup> ✓
T10	25 - 20	P2.5x.203	7.44	7.12	90.2	1.7040	7.61	70.55	0.108 <sup>1</sup> ✓
T11	20 - 0	P3x.216	11.94	11.51	118.7	2.2285	19.92	92.26	0.216 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / ϕP<sub>n</sub> controls

### Horizontal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L <sub>u</sub> ft	Kl/r	A in <sup>2</sup>	P <sub>u</sub> K	ϕP <sub>n</sub> K	Ratio $\frac{P_u}{\phi P_n}$
T2	75 - 70	2L1 3/4x1 3/4x1/8	9.00	4.19	94.8	0.4922	1.97	21.41	0.092 <sup>1</sup> ✓
T4	65 - 60	2L1 3/4x1 3/4x1/8	9.00	8.39	106.4	0.4922	0.27	21.41	0.013 <sup>1</sup> ✓
T5	60 - 50	2L1 3/4x1 3/4x1/8	9.00	6.35	106.4	0.4922	0.52	21.41	0.024 <sup>1</sup> ✓
T6	50 - 40	2L1 3/4x1 3/4x1/8	9.00	4.19	94.8	0.4922	0.76	21.41	0.035 <sup>1</sup> ✓
T8	35 - 30	2L1 3/4x1 3/4x1/8	9.50	4.44	100.3	0.4922	1.56	21.41	0.073 <sup>1</sup> ✓
T10	25 - 20	2L2x2x1/8	10.50	4.90	96.2	0.5794	1.95	25.20	0.078 <sup>1</sup> ✓
T11	20 - 0	2L2x2x1/8	12.00	5.57	110.6	0.5794	1.25	25.20	0.050 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / ϕP<sub>n</sub> controls

<b>tnxTower</b>  <b>Kimley-Horn</b> 421 Fayetteville St., Suite 600 Raleigh, NC 27601 Phone: (919) 677-2000 FAX: (919) 677-2000	Job	Oak Creek Coal	Page
	Project	PR-91471	Date 15:07:29 07/20/22
	Client	SAC Wireless	Designed by Elliot Ziebart

### Top Girt Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio $\frac{P_u}{\phi P_n}$
	ft		ft	ft		in <sup>2</sup>	K	K	
T1	80 - 75	2L2x2x3/16x3/8	9.00	8.39	167.7	0.8616	0.33	37.48	0.009 <sup>1</sup> ✓
T11	20 - 0	2L2x2x1/8x3/8	11.00	5.07	101.0	0.5794	8.30	25.20	0.330 <sup>1</sup> ✓
2L 'a' > 29.0126 in - 199									

<sup>1</sup> P<sub>u</sub> / ϕP<sub>n</sub> controls

### Redundant Vertical Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio $\frac{P_u}{\phi P_n}$
	ft		ft	ft		in <sup>2</sup>	K	K	
T10	25 - 20	2L1 3/4x1 3/4x1/8x3/8	5.01	5.01	110.1	0.8438	0.11	27.34	0.004 <sup>1</sup> ✓
2L 'a' > 28.6358 in - 183									

<sup>1</sup> P<sub>u</sub> / ϕP<sub>n</sub> controls

### Inner Bracing Design Data (Tension)

Section No.	Elevation	Size	L	L <sub>u</sub>	Kl/r	A	P <sub>u</sub>	ϕP <sub>n</sub>	Ratio $\frac{P_u}{\phi P_n}$
	ft		ft	ft		in <sup>2</sup>	K	K	
T2	75 - 70	L1 3/4x1 3/4x1/8	6.36	6.36	139.9	0.4219	0.01	13.67	0.000 <sup>1</sup> ✓
T6	50 - 40	L1 3/4x1 3/4x1/8	6.36	6.36	139.9	0.4219	0.03	13.67	0.002 <sup>1</sup> ✓
T8	35 - 30	L1 3/4x1 3/4x1/8	6.72	6.72	147.7	0.4219	0.02	13.67	0.002 <sup>1</sup> ✓
T9	30 - 25	L1 3/4x1 3/4x1/8	7.42	7.42	163.3	0.4219	0.02	13.67	0.002 <sup>1</sup> ✓
T10	25 - 20	L1 3/4x1 3/4x1/8	7.78	7.78	171.0	0.4219	0.01	13.67	0.001 <sup>1</sup> ✓
T11	20 - 0	L1 3/4x1 3/4x1/8	12.00	12.00	263.9	0.4219	0.04	13.67	0.003 <sup>1</sup> ✓

<sup>1</sup> P<sub>u</sub> / ϕP<sub>n</sub> controls

### Section Capacity Table



<b><i>tnxTower</i></b>  <b>Kimley-Horn</b> 421 Fayetteville St., Suite 600 Raleigh, NC 27601 Phone: (919) 677-2000 FAX: (919) 677-2000	<b>Job</b>	Oak Creek Coal	<b>Page</b>
	<b>Project</b>	PR-91471	<b>Date</b> 15:07:29 07/20/22
	<b>Client</b>	SAC Wireless	<b>Designed by</b> Elliot Ziebart

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	$\phi P_{allow}$ K	% Capacity	Pass Fail
				(T2)				
				Top Girt (T11)		50.5	Pass	
				Redund Vert Bracing (T10)	0.4		Pass	
				Inner Bracing (T11)		5.2	Pass	
				Bolt Checks Rating =	82.1		Pass	
						82.1	Pass	

---

## APPENDIX D

### Base Plate & Anchor Rod Calculations

## Self Support Anchor Rod Capacity - Phase 1

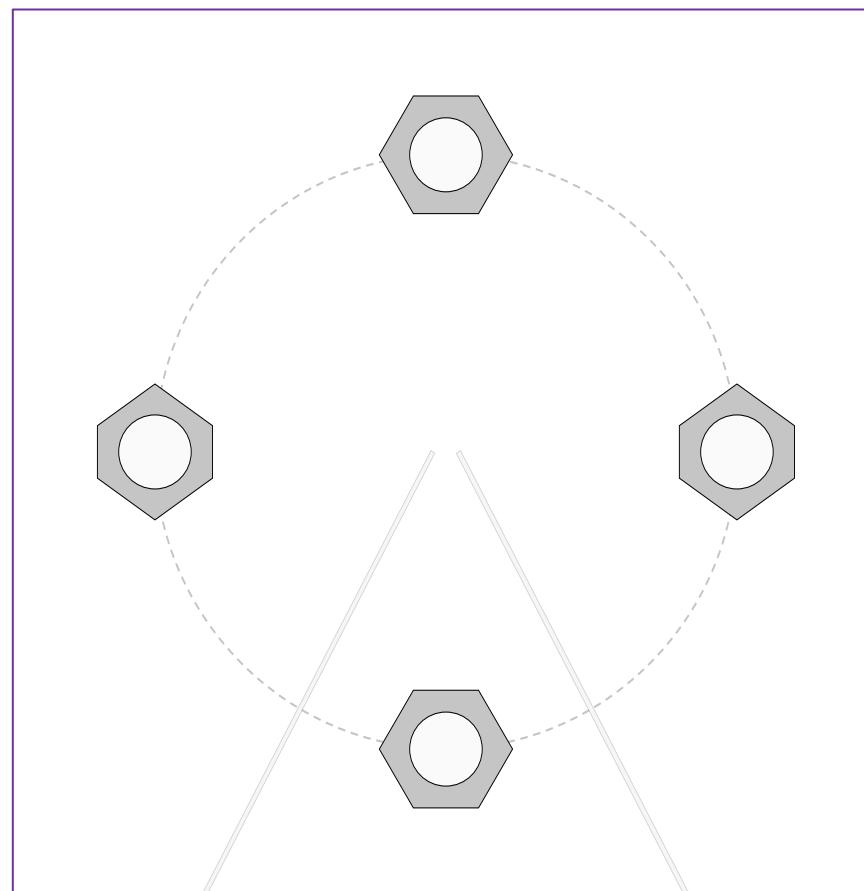
Site Info	
Client Project ID	PR-91471
Site Name	Oak Creek Coal
Order #	KHCLE-26656

Analysis Considerations	
TIA-222 Revision	H
Grout Considered:	0
$l_{ar}$ (in)	0

Applied Loads		
	Comp.	Uplift
Axial Force (kips)	126.00	114.00
Shear Force (kips)	26.00	23.00

Considered Eccentricity	
Leg Mod Eccentricity (in)	0.000
Anchor Rod N.A Shift (in)	0.000
Total Eccentricity (in)	0.000

\*Anchor Rod Eccentricity Applied



### Connection Properties

#### Anchor Rod Data

(4) 1-1/2" ø bolts (F1554-55 N; Fy=55 ksi, Fu=75 ksi)  
 $l_{ar}$  (in): 0

### Analysis Results

#### Anchor Rod Summary

$P_u_c = 31.5$	#DIV/0!	<b>Stress Rating</b>
$V_u = 6.5$	$\phi V_n = 39.36$	<b>38.7%</b>
$M_u = n/a$	$\phi M_n = n/a$	<b>Pass</b>

(units of kips, kip-in)

## Self Support Anchor Rod Capacity - Phase 2

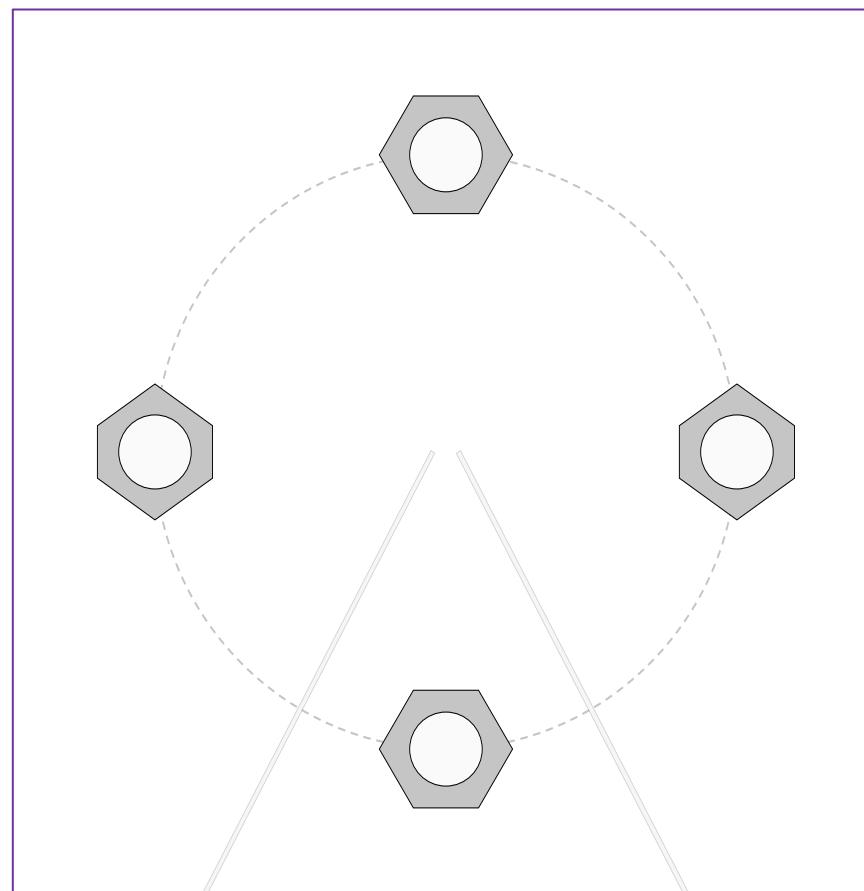
Site Info	
Client Project ID	PR-91471
Site Name	Oak Creek Coal
Order #	KHCLE-26656

Analysis Considerations	
TIA-222 Revision	H
Grout Considered:	0
$l_{ar}$ (in)	0

Applied Loads		
	Comp.	Uplift
Axial Force (kips)	117.00	105.00
Shear Force (kips)	24.00	22.00

Considered Eccentricity	
Leg Mod Eccentricity (in)	0.000
Anchor Rod N.A Shift (in)	0.000
Total Eccentricity (in)	0.000

\*Anchor Rod Eccentricity Applied



### Connection Properties

#### Anchor Rod Data

(4) 1-1/2" ø bolts (F1554-55 N; Fy=55 ksi, Fu=75 ksi)  
 $l_{ar}$  (in): 0

### Analysis Results

#### Anchor Rod Summary

$P_u_c = 29.25$	#DIV/0!	<b>Stress Rating</b>
$V_u = 6$	$\phi V_n = 39.36$	<b>35.8%</b>
$M_u = n/a$	$\phi M_n = n/a$	<b>Pass</b>

(units of kips, kip-in)

---

## APPENDIX E

### Foundation Calculations

# SST Unit Base Foundation - Phase 1

<b>Client Project ID:</b>	PR-91471
<b>Site Name:</b>	Oak Creek Coal
<b>JIRA #:</b>	KHCLE-26656

TIA-222 Revision: H

Top & Bot. Pad Rein. Different?:	<input checked="" type="checkbox"/>
Tower Centroid Offset?:	<input type="checkbox"/>
Block Foundation?:	<input checked="" type="checkbox"/>
Rectangular Pad?:	<input type="checkbox"/>

Superstructure Analysis Reactions		
Global Moment, M:	2188	ft-kips
Global Axial, P:	28	kips
Global Shear, V:	40	kips
Leg Compression, P <sub>comp</sub> :	126	kips
Leg Comp. Shear, V <sub>u_comp</sub> :	26	kips
Leg Uplift, P <sub>uplift</sub> :	114	kips
Leg Uplift. Shear, V <sub>u_uplift</sub> :	23	kips
Tower Height, H:	80	ft
Base Face Width, BW:	13	ft
BP Dist. Above Fdn, bp <sub>dist</sub> :	3	in
Anchor Bolt Circle, BC:	12	in

Foundation Analysis Checks				
	Capacity	Demand	Rating	Check
Lateral (Sliding) (kips)	105.38	40.00	38.0%	Pass
Bearing Pressure (ksf)	3.29	1.33	40.5%	Pass
Overturning (kip*ft)	4139.80	2358.00	57.0%	Pass
Pad Flexure (kip*ft)	2236.48	688.51	30.8%	Pass
Pad Shear - 1-way (kips)	1124.67	95.12	8.5%	Pass
Pad Shear - Comp 2-way (ksi)	0.164	0.013	7.9%	Pass
Flexural 2-way (Comp) (kip*ft)	1014.64	0.00	0.0%	Pass
Pad Shear - Tension 2-way (ksi)	0.164	0.012	7.1%	Pass
Flexural 2-way (Tension) (kip*ft)	1014.64	0.00	0.0%	Pass

Structural Rating:	<b>30.8%</b>
Soil Rating:	<b>57.0%</b>

Pad Properties		
Depth, D:	3.50	ft
Pad Width, W <sub>1</sub> :	26.00	ft
Pad Thickness, T:	4.00	ft
Pad Rebar Size (Top dir.2), Sp <sub>top2</sub> :	6	
Pad Rebar Quantity (Top dir. 2), mp <sub>top2</sub> :	21	
Pad Rebar Size (Bottom dir. 2), Sp <sub>2</sub> :	6	
Pad Rebar Quantity (Bottom dir. 2), mp <sub>2</sub> :	26	
Pad Clear Cover, cc <sub>pad</sub> :	3	in

Material Properties		
Rebar Grade, Fy:	60	ksi
Concrete Compressive Strength, F'c:	3	ksi
Dry Concrete Density, δc:	150	pcf

Soil Properties		
Total Soil Unit Weight, γ:	110	pcf
Ultimate Net Bearing, Qnet:	4.000	ksf
Cohesion, Cu:		ksf
Friction Angle, φ:	30	degrees
SPT Blow Count, N <sub>blows</sub> :	10	
Base Friction, μ:		
Neglected Depth, N:	4.0	ft
Foundation Bearing on Rock?	No	
Groundwater Depth, gw:	N/A	ft

-- Toggle between Gross and Net

## SST Unit Base Foundation - Phase 2

<b>Client Project ID:</b>	PR-91471
<b>Site Name:</b>	Oak Creek Coal
<b>JIRA #:</b>	KHCLE-26656

TIA-222 Revision: H

Top & Bot. Pad Rein. Different?:	<input checked="" type="checkbox"/>
Tower Centroid Offset?:	<input type="checkbox"/>
Block Foundation?:	<input checked="" type="checkbox"/>
Rectangular Pad?:	<input type="checkbox"/>

Superstructure Analysis Reactions		
Global Moment, M:	2021	ft-kips
Global Axial, P:	28	kips
Global Shear, V:	38	kips
Leg Compression, P <sub>comp</sub> :	117	kips
Leg Comp. Shear, V <sub>u_comp</sub> :	24	kips
Leg Uplift, P <sub>uplift</sub> :	105	kips
Leg Uplift. Shear, V <sub>u_uplift</sub> :	22	kips
Tower Height, H:	80	ft
Base Face Width, BW:	13	ft
BP Dist. Above Fdn, bp <sub>dist</sub> :	3	in
Anchor Bolt Circle, BC:	12	in

Foundation Analysis Checks				
	Capacity	Demand	Rating	Check
Lateral (Sliding) (kips)	105.38	38.00	36.1%	Pass
Bearing Pressure (ksf)	3.29	1.29	39.2%	Pass
Overturning (kip*ft)	4139.80	2182.50	52.7%	Pass
Pad Flexure (kip*ft)	2236.48	624.39	27.9%	Pass
Pad Shear - 1-way (kips)	1124.67	86.17	7.7%	Pass
Pad Shear - Comp 2-way (ksi)	0.164	0.012	7.3%	Pass
Flexural 2-way (Comp) (kip*ft)	1014.64	0.00	0.0%	Pass
Pad Shear - Tension 2-way (ksi)	0.164	0.011	6.6%	Pass
Flexural 2-way (Tension) (kip*ft)	1014.64	0.00	0.0%	Pass

Structural Rating:	<b>27.9%</b>
Soil Rating:	<b>52.7%</b>

Pad Properties		
Depth, D:	3.50	ft
Pad Width, W <sub>1</sub> :	26.00	ft
Pad Thickness, T:	4.00	ft
Pad Rebar Size (Top dir.2), Sp <sub>top2</sub> :	6	
Pad Rebar Quantity (Top dir. 2), mp <sub>top2</sub> :	21	
Pad Rebar Size (Bottom dir. 2), Sp <sub>2</sub> :	6	
Pad Rebar Quantity (Bottom dir. 2), mp <sub>2</sub> :	26	
Pad Clear Cover, cc <sub>pad</sub> :	3	in

Material Properties		
Rebar Grade, Fy:	60	ksi
Concrete Compressive Strength, F'c:	3	ksi
Dry Concrete Density, δc:	150	pcf

Soil Properties		
Total Soil Unit Weight, γ:	110	pcf
Ultimate Net Bearing, Qnet:	4.000	ksf
Cohesion, Cu:		ksf
Friction Angle, φ:	30	degrees
SPT Blow Count, N <sub>blows</sub> :	10	
Base Friction, μ:		
Neglected Depth, N:	4.0	ft
Foundation Bearing on Rock?	No	
Groundwater Depth, gw:	N/A	ft

-- Toggle between Gross and Net

## APPENDIX F

### RFDS>Loading Sheet



Collo 1	RRH	60	Nokia	3JR80235AAAA	40	1	Existing	A Sector
Collo 1	Sector Frame	60	Valmont	VFA10-HD FRAMES	135	1	Existing	NA
Collo 1	Panel Antenna	60	CommScope	NNH4-65C-R6-V3	135	1	Existing	B Sector
Collo 1	Panel Antenna	60	CommScope	NNH4-65C-R6-V3	135	1	FUTURE	B Sector
Collo 1	DUAL CLAMP MOUNT	60	Rosenberger	D218RRUDSM	135	1	Existing	B Sector
Collo 1	RRH	60	Nokia	3JR80236AAAA	135	1	Existing	B Sector
Collo 1	RRH	60	Nokia	3JR80235AAAA	135	1	Existing	B Sector
Collo 1	Sector Frame	60	Valmont	VFA10-HD FRAMES	300	1	Existing	NA
Collo 1	Panel Antenna	60	CommScope	NNH4-65C-R6-V3	300	1	Existing	G Sector
Collo 1	Panel Antenna	60	CommScope	NNH4-65C-R6-V3	300	1	FUTURE	G Sector
Collo 1	DUAL CLAMP MOUNT	60	Rosenberger	D218RRUDSM	300	1	Existing	G Sector
Collo 1	RRH	60	Nokia	3JR80236AAAA	300	1	Existing	G Sector
Collo 1	RRH	60	Nokia	3JR80235AAAA	300	1	Existing	G Sector
Collo 1	Power Trunk	0-60	Rosenberger	WR-VG865T-BRD	NA	3	Existing	All Sectors
Collo 1	Fiber Feed	0-60	Rosenberger	FB-L98B-235-75000	NA	1	Existing	All Sectors
Collo 1	Dist. Box	60	Raycap	DC9-48-60-24-8C-EV	NA	1	Existing	All Sectors
Collo 2	Dish	20	Mimosa	B5 - 18" Diameter	74	1	LEASED	Colocator
Collo 2	Waveguide	0-20	Unknown	CAT5 - .25" Diameter	NA	2	LEASED	Colocator
Collo 2	Dish	20	Mimosa	B5 - 18" Diameter	102	1	LEASED	Colocator
Collo 2	Waveguide	0-20	Unknown	CAT5 - .25" Diameter	NA	2	LEASED	Colocator









