

Liquid Unit Location – Twin Enviro Services, Milner, CO

**RCRBD Record
Set T.C.**

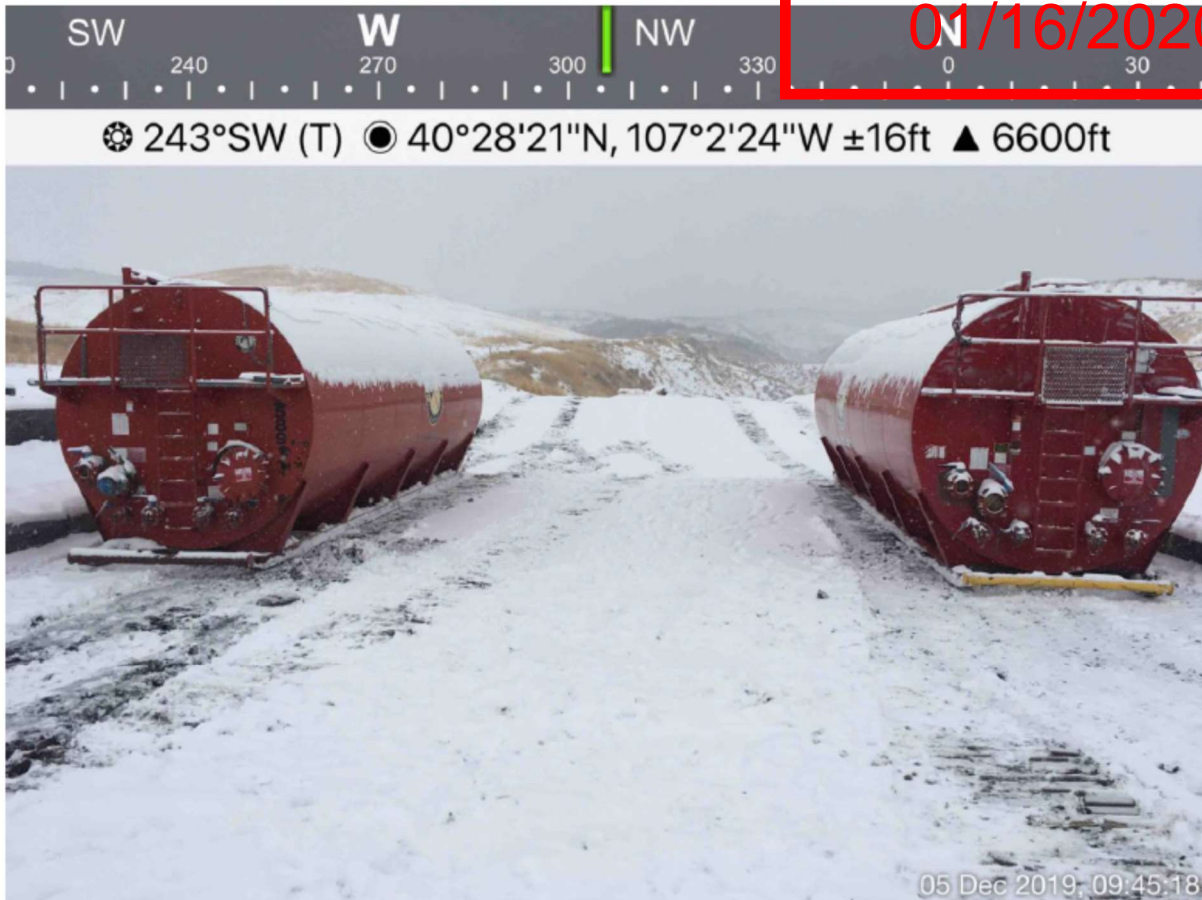
01/16/2020



Installed Tanks Photo


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Load Calculations (excerpts from *Liquid Waste Transfer Unit Design and Operations Plan*, Golder 2019)

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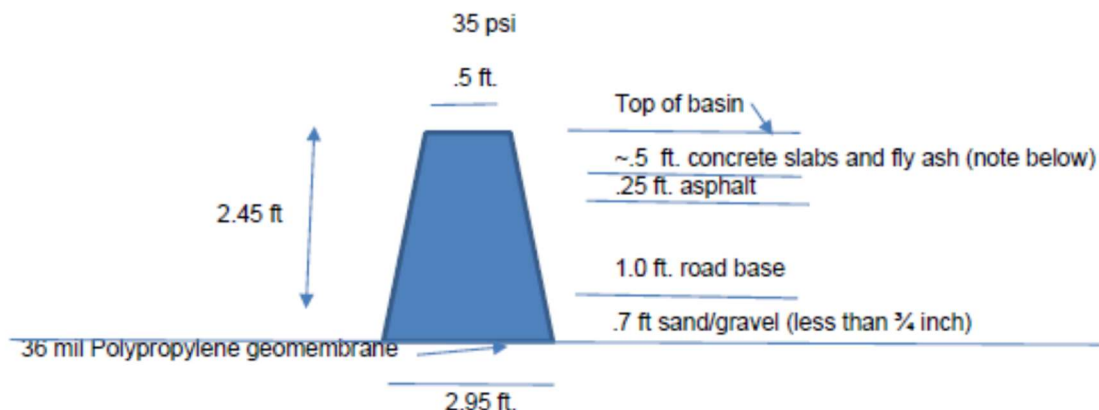
	Subject: Milner Landfill Impacts to Liner in Old Solidification Basin from Addition of Tanks	Made by: MEM	Job No: 1786428 01/16/2020
		Checked by: CDM	Date: 10/22/2019
	Analysis and References	Approved by: MEM	Sheet No: 1 of 2

OBJECTIVE:

To show that the existing 36-mil reinforced polypropylene liner within old Solidification Basin can withstand potential puncture forces imposed by addition of two 20,000-gallon tanks that will be used for liquids transfer in former solidification basin.

METHOD:

Calculate the stress imposed by the tanks and overburden on the underlying geomembrane. Then evaluate puncture of geomembrane from granular material on top of liner. Use Koerner method of evaluating puncture.




CALCULATIONS:

From Luke Schneider at Milner, two 20,000 tanks, each sits on two steel rails about 35 ft long by 0.5 ft wide. Assume tank is completely full of fluid and stress is transferred to geomembrane at a 1 H to 2 V slope as shown to underlying geomembrane. Each tank weighs ~ 10,000 lbs. empty, so assume that total weight is 10,000 lbs., plus weight of tank full of liquid and that half of the load goes to each rail. Rails are about 7' apart for each rail, so liner will not see stress from both rails or rails supporting adjacent tank (tanks are spaced several feet apart to allow for roll-off box to be placed in-between. (Note: Ignored layers of geotextile and fence on top of geomembrane to simplify analysis. Concrete slabs are ~ 4 inches thick with additional ~ 3 inches of fly ash on top, rounded to 0.5 ft.).

Stress at top of surface of basin = $10,000 \text{ lbs.} + 20,000 \text{ gal.} \times 8.3 \text{ lbs./gal} / (35' \times 0.5')/2 \times 144 \text{ in.}^2 / \text{ft.}^2 = 35 \text{ psi}$

Stress on top of geomembrane from tanks = $35 \text{ psi} / (2.95'/.5') = 6 \text{ psi}$

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Approximate stress on geomembrane from overburden = $130 \text{ lb./ft}^3 \times 2.45 \text{ ft.} \times (1 \text{ ft}^2/144 \text{ in}^2) = 2.2 \text{ psi}$

Total stress on geomembrane = $6 \text{ psi} + 2.2 \text{ psi} = 8.2 \text{ psi}$

Maximum grain-size of sand/gravel on top of geomembrane is $\frac{3}{4}$ inch from Golder CQA report (2016) on repairs

Use Koerner's equation for puncture of a geotextile (page 165 3rd Edition) to estimate required puncture resistance of 36 mil PPE liner

$$F_{reqd} = p' d_a^2 S_1 S_2 S_3$$

Where:

p' = pressure applied to geomembrane = 8.2 psi

d_a = average diameter of puncturing aggregate, assume $\frac{3}{4}$ " which is maximum size

S_1 = protrusion factor h_n/d_a , where h_n is height of protrusion, assume it is equal to d_a , so $S_1 = 1.0$

S_2 = scale factor to adjust puncture test from ASTM D 4833 from 5/16" diameter to actual diameter = $0.31/d_a = 0.31/.75 = 0.41$

S_3 = shape factor $(1 - A_p/A_c)$, where a conservative value of 0.4 for A_p/A_c will be used crushed rock so $S_3 = 0.6$

$$F_{reqd} = 8.2 \times (.75)^2 \times 1.0 \times 0.41 \times 0.6 = 1.13 \text{ lbs.}$$

Typical minimum puncture resistance for 36 mil PPE from Lange Containment Systems using ASTM D 4833 is 85 lbs.

Using a cumulative partial factor of safety of 4.0, the global factor of safety is:

$$FS = F_{allow}/F_{reqd} = 85/(4.0 \times 1.13) = 18.8, \text{ which is acceptable}$$

CONCLUSIONS/RESULTS:

Based on the calculation above, the 36-mil PPE liner will not be at risk from puncture from the addition of the tanks in the basins.

REFERENCES:

Koerner, Robert M. Designing with Geosynthetics, 3rd Edition. Prentice Hall, Englewood Cliffs, NJ. 1994.

Conversation with Luke Schneider at Milner to get information on tanks. September 18, 2019.

Lange Containment Systems Inc. website, Puncture Strength for 36 mi PPE using D 4833.

Golder Associates Inc. CQA Monitoring and Testing Results, Milner Landfill Solidification Repair, April 7, 2015.